## SCHOOL OF CIVIL AND ENVIROMENTAL ENGINEERING

## Surveying II CENG 2092

## Chapter 3 Curves



## Engineering Surveying -- Def

The ASCE defines engineering surveying as those activities involved in the planning and execution of surveys for the location, design, construction, operation, and maintenance of civil and other engineered projects. Such activities include:

- The preparation of survey and related mapping specifications;
- Execution of photogrammetric and field surveys for the collection of required data
- Calculation, reduction and plotting of survey data for use in engineering design including use for geographic information systems (GIS);
- Design and provision of horizontal and vertical control survey networks;
- Monitoring of ground and structural stability, including alignment observations, settlement levels, and related reports and certifications; and
- Analysis of errors and tolerances associated with the measurement, field layout and mapping.


## Engineering surveying

- Curve setting out
- Earth work computation
- Staking of structures like building, bridge, culvert and tunnel
- Monitoring of ground and structural stability
- Route surveying


## Measurement and setting out

- Accurate large-scale plan $\rightarrow$ planning and design of a construction project
- The plan $\rightarrow$ set out on the ground in the correct absolute and relative position and to its correct dimensions


## Curve

- The center line of a road consists of series of straight lines interconnected by curves that are used to change the alignment, direction, or slope of the road.
- Those curves that change the alignment or direction are known as horizontal curves, and
- Those that change the slope are vertical curves.


## Curve Setting out

- Horizontal Curve
- Circular Curve
- Compound Curve
- Reverse Curve
- Transition Curve
- Vertical Curve
- Parabolic curve


## Simple circular and Compound



## Reverse Curve and Transition

## curve



## Vertical Curves



## Horizontal Curves

- The principal consideration in the design of a curve is the selection of the length of the radius or the degree of curvature
- This selection is based on such considerations as the design speed of the highway and the sight distance as limited by headlights or obstructions



## Elements of Horizontal Curves

- I - Point of intersection
- T1 - Point of commencement
- T2 - Point of tangency
- E-External distance
- T1T2 - Length of the curve
- T11 = IT2 = tangent length
- AI - Back Tangent
- BI - Forward Tangent
- T1T2 - Chord length
- $\Delta$ - Deflection angle
- R - Radius of the curve
- $\phi$ - Angle of intersection
- M - Mid-ordinate



## Formula to calculate the various elements of a circular curve for use in design and setting out

$$
\begin{aligned}
\text { Tangent length }(T) & =R \tan \frac{\Delta}{2} \\
\text { Length of curve }(l) & =\frac{\pi R \Delta}{180} \\
\text { Long chord }(L) & =2 R \sin \frac{\Delta}{2} \\
\text { External distance }(E) & =R\left(\sec \frac{\Delta}{2}-1\right) \\
\text { Mid-ordinate }(M) & =R\left(1-\cos \frac{\Delta}{2}\right) \\
\text { Chainage of } T_{1} & =\text { Chainage of P.I. }-T \\
\text { Chainage of } T_{2} & =\text { Chainage of } T_{1}+l .
\end{aligned}
$$

## Setting out of circular curves

Offset from long chord


## - Offset from tangent



$$
\begin{align*}
y & =R-\sqrt{\left(R^{2}-x^{2}\right)} & & (\text { exact })  \tag{exact}\\
& =\frac{x^{2}}{2 R} & & \text { (approximate) }
\end{align*}
$$

## - Setting out using one theodolite and tape



Tangential angle $\delta_{n}=1718.9 \frac{c_{n}}{R}$ minutes

## - Setting out using two theodolite



## - Setting out using Coordinates



- Coordinates of T1 and I known form design
- $\delta$ known from deflection angle method
- Bearing of T1I is computed
- Using $\delta$ s and bearing of T1I bearings of T1A, T1B ..
- Distance T1A, T1B .. can be computed as $2 \mathrm{R} \sin (\delta 1) \ldots$
- using the bearing and distances coordinates of $\mathrm{A}, \mathrm{B}, \mathrm{C}$.. are obtained
- These points can now be set out from the nearest control points by polar or intersection methods
- By computing bearing and distance


## - Setting out with inaccessible intersection point

Project the straights forward as far as possible and establish two points $A$ and $B$ on them. Measure distance $A B$ and angles $B A C$ and $D B A$ then:
angle $I A B=180^{\circ}-\hat{A A C}$ and angle $I B A=180^{\circ}-D \hat{B A} A$, from which angle $B I A$ is deduced and angle $\triangle$. The triangle AIB can now be solved for lengths $I A$ and $I B$. These lengths, when subtracted from the computed tangent lengths $(R \tan \Delta 2)$, give $A T_{1}$ and $B T_{2}$, which are set off along the straight to give positions $T_{1}$ and $T_{2}$ respectively.


## Example 1

- A circular curve of 500 m radius to be set out joining the two straights with deflection angle of $38^{\circ}$. Calculate the necessary data for setting out the curve by the method of
- Offset from long chord
- Offset from tangent
- Deflection angle method

Take peg interval of 30 m length and the chainage of I ( 60 $+13.385)$

## Solution

## Calculations of elements of the Curve

- Tangent length $=\operatorname{Rtan}(\Delta / 2)=500 \tan 19^{\circ}=172.164 \mathrm{~m}$
- Length of the curve $(1)=(\pi \mathrm{R} \Delta / 180)=331.613 \mathrm{~m}$
- Chainage of $\mathrm{T} 1=$ Chainage of $\mathrm{I}-\mathrm{T} 1 \mathrm{I}=60 \times 30+13.385-172.164$

$$
=1641.221=54+21.22
$$

- Chainage of $\mathrm{T} 2=$ Chainage of $\mathrm{I}+\mathrm{l}=1641.221+331.613$

$$
=1972.834=65+22.83
$$

- Long chord $(\mathrm{L})=2 \mathrm{R} \sin (\Delta / 2)=325.57 \mathrm{~m}$
- $\mathrm{L} / 2=162.785 \mathrm{~m}$
- To locate the points on the curve, for distances
- $X=0,30,60,90,120,150,162.785 \mathrm{~m}$

The offset from long chord is calculated as:

$$
\begin{aligned}
y & =\sqrt{\left(R^{2}-x^{2}\right)}-\sqrt{\left(R^{2}-\frac{L}{4}\right)^{2}} \\
& =\sqrt{\left(500^{2}-x^{2}\right)}-472.759
\end{aligned}
$$

The calculated value of $y$,

| Distance $x(\mathrm{~m})$ | 0 | 30 | 60 | 90 | 120 | 150 | 162.79 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Offset $y(\mathrm{~m})$ | 27.24 | 26.34 | 23.63 | 19.07 | 12.63 | 4.21 | 0.00 |

Offset from tangent

$$
y=R-\sqrt{\left(R^{2}-x^{2}\right)}
$$

| $\mathbf{x}$ | $\mathbf{0}$ (T1) | $\mathbf{3 0}$ | $\mathbf{6 0}$ | $\mathbf{9 0}$ | $\mathbf{1 2 0}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 2 . 1 6 4 ( \mathbf { I } )}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| y | 0 | 0.901 | 3.613 | 8.167 | 14.614 | 23.030 | 30.575 |

## Deflection angle method

Length of first sub-chord $=(54+30)-(54+21.22)=8.78 \mathrm{~m}$ Length of last sub-chord $=(65+22.83)-(65+0)=22.83 \mathrm{~m}$ Number of normal chords $N=65-55=10$
Total number of chords $n=10+2=12$
Tangential angle $\delta_{n}=1718.9 \frac{c_{n}}{R}$ minutes
Tangential angle for the first chord $=1718.9 * 8.78 / 500=30.184 \mathrm{~min}$ Tangential angle for the normal chord $=1718.9 * 30 / 500=103.184 \mathrm{~min}$ Tangential angle for the last chord $=1718.9 * 22.83 / 500=78.485 \mathrm{~min}$

| Point | Chainage | Chord <br> Length (m) | Tangential angle (') | Deflection Angle (') | Angle set on 1" |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $0\left(\mathrm{~T}_{1}\right)$ | $54+21.22$ | - | 0.0 | 0.0 |  |
| 1 | $55+00$ | 8.78 | 30.184 | 30.184 | 00 ${ }^{\circ} 3{ }^{\prime} 11{ }^{\prime \prime}$ |
| 2 | $56+00$ | 30 | 103.134 | 133.318 | 02 ${ }^{\circ} 13$ '19" |
| 3 | $57+00$ | 30 | 103.134 | 236.452 | $03^{\circ} 56,2{ }^{\prime \prime}$ |
| 4 | $58+00$ | 30 | 103.134 | 339.586 | 05'39'35' |
| 5 | $59+00$ | 30 | 103.134 | 442.720 | 07 ${ }^{\circ} 2^{\prime} 43^{\prime \prime}$ |
| 6 | $60+00$ | 30 | 103.134 | 546.104 | 09 ${ }^{\circ} 06$ '06" |
| 7 | $61+00$ | 30 | 103.134 | 648.988 | 10 ${ }^{\circ} 4{ }^{\prime} 59$ " |
| 8 | $62+00$ | 30 | 103.134 | 752.122 | 12 ${ }^{\circ} 3^{\prime}$, $7^{\prime \prime}$ |
| 9 | $63+00$ | 30 | 103.134 | 855.256 | $14^{\circ} 15^{\prime} 15$ " |
| 10 | $64+00$ | 30 | 103.134 | 958.839 | 15 ${ }^{\circ} 58$ '50" |
| 11 | $65+00$ | 30 | 103.134 | 1061.524 | 17${ }^{\circ} 41$ '31" |
| 12( $\mathrm{T}_{2}$ ) | $65+22.83$ | 22.83 | 78.485 | 1140.009 | $19^{\circ} 00^{\prime} 01 "$ |

## Transition curves

- The transition curve is a curve of constantly changing radius


Some of the important properties of the spirals are given below:
$\cdot L=2 R \theta$

- $\theta=\left(L / L_{s}\right)^{2} \theta_{s}$
$\cdot \theta_{\mathrm{s}}=\mathrm{L}_{\mathrm{s}} / 2 R_{\mathrm{c}}$ (in radians) $=28.65 \mathrm{~L}_{\mathrm{s}} / \mathrm{R}_{\mathrm{c}}$ (in degrees)
$\cdot \mathrm{T}_{\mathrm{s}}=\mathrm{L}_{\mathrm{s}} / 2+\left(\mathrm{R}_{\mathrm{c}}+\mathrm{S}\right)^{*} \tan (\Delta / 2)$
- $\mathrm{S}=\mathrm{L}_{\mathrm{s}}{ }^{2} / 24 \mathrm{R}_{\mathrm{c}}$
- $\mathrm{E}_{\mathrm{s}}=\left(\mathrm{R}_{\mathrm{c}}+\mathrm{S}\right)^{*} \sec (\Delta / 2)-R_{\mathrm{c}}$


## Transition curves



Note:
$\theta_{\mathrm{s}}=$ spiral angle
$\Delta=$ total central angle
$\Delta_{\mathrm{c}}=$ central angle of the circular arc extending fro BC to $\mathrm{EC}=\Delta-2$
$\theta_{\text {s }}$
$\mathrm{R}_{\mathrm{c}}=$ radius of circular curve
$\mathrm{L}=$ length of spiral from starting point to any point
$\mathrm{R}=$ radius of curvature of the spiral at a point L distant from starting point.
$\mathrm{T}_{\mathrm{s}}=$ tangent distance
$\mathrm{E}_{\mathrm{s}}=$ external distance
$\mathrm{S}=$ shift
HIP = horizontal intersection point
$\mathrm{BS}=$ beginning of spiral
$\mathrm{BC}=$ beginning of circular curve
$\mathrm{EC}=$ end of circular curve
$\mathrm{ES}=$ end of spiral curve

## Shift, S

- Where transition curves are introduced between the tangents and a circular curve of radius $R$, the circular curve is "shifted" inwards from its original position by an amount $\mathrm{BP}=\mathrm{S}$ so that the curves can meet tangentially.

Referring the figure below $\angle \mathrm{NMO}=\angle \mathrm{RTO}=90^{\circ}$
$\mathrm{BM}=\mathrm{NT}_{1}=$ Maximum offset on transition curve

$$
\begin{aligned}
& \text { Also shift }=\mathrm{S}=B P=B M-M O=N T_{1}-(P O-M O) \\
& \begin{aligned}
=\frac{L^{3}}{6 L R}-\left(R-R \cos \phi_{1}\right) & =\frac{L^{3}}{6 L R}-\left\{R-R\left(1-\frac{\phi_{1}^{2}}{2!}+\frac{\phi_{1}^{4}}{4!}-\ldots\right)\right\}=\frac{L^{3}}{6 L R}-R \frac{\phi_{1}^{2}}{2} \\
& =\frac{L^{3}}{6 L R}-\frac{R}{2}\left(\frac{L^{2}}{2 L R}\right)^{2} \\
& =\frac{L^{2}}{24 R}
\end{aligned} \\
& \text { Also } \mathrm{Q}_{1} \mathrm{~T}_{1} \approx \mathrm{PT}_{1} \approx \mathrm{R} \phi_{1}=\frac{R L^{2}}{2 L R}=\frac{L}{2}
\end{aligned}
$$


b)

## Setting out of transition curve

## Step 1

Calculate the shift S from the expression $S=\frac{L^{2}}{24 R}$
Step 2
Calculate $\mathrm{IB}=(R+S) \tan \frac{\theta}{2}$
Step 3
$\mathrm{BT}=\mathrm{L} / 2$ Then $\mathrm{IT}=(R+S) \tan \frac{\theta}{2}+\frac{L}{2}$

## Step 4

Either calculate offset from

$$
x=\frac{l^{3}}{6 K} \text { or } x=\frac{y^{3}}{6 K}
$$

OR
Calculate the deflection angles $\delta$ from particular distances 1 from T using the fact that

$$
\begin{aligned}
\delta & =\phi / 3=\frac{l^{2}}{6 R L} \mathrm{rad} \\
& =\frac{1800}{\pi} \frac{l^{2}}{R L} \min \delta_{\max }=L / 6 R \mathrm{rad} \text { OR }=\frac{1800 L}{\pi R}
\end{aligned}
$$

## Step 5

Setting out the circular curve
Calculate the deflection angles for the circular curve from
$\delta_{\text {Ciralur }}=1718.9 \frac{\mathrm{C}}{\mathrm{R}} \mathrm{min}$
Where c is the chord length for the circular arc
The angle subtended by the circular arc $\mathrm{T}_{1} \mathrm{~T}_{2}$ at the center of that arc is $\left(\theta-2 \phi_{1}\right)$
Length of the arc $\mathrm{T}_{1} \mathrm{~T}_{2}=R\left(\theta-2 \phi_{1}\right) \frac{\pi}{180}$
Step 6
Set up the theodolite at $T_{1}$ and sight back on $T$; then, transit the telescope and locate $T_{1} T_{3}$ by setting off an angle $2 / 3 \phi_{1}$. Set out the circular curve by the deflection angle method, from this tangent.


## Example 2

- Two straights $A B$ and $B C$ intersect at chainage 1530.685 m , the total deflection angle being $33^{\circ} 08^{\prime}$. It is proposed to insert a circular curve of 1000 m radius and the transition curves for a rate of change of radial acceleration of $0.3 \mathrm{~m} / \mathrm{s} 3$, and a velocity of 108 $\mathrm{km} / \mathrm{h}$. Determine setting out data using theodolite and tape for the transition curve at 20 m intervals and the circular curve at 50 m intervals.


## Solution

- $\alpha=0.3 \mathrm{~m} / \mathrm{cub} \mathrm{sec}$
- $\mathrm{V}=108 \mathrm{~km} / \mathrm{hr}=30 \mathrm{~m} / \mathrm{s}$
- $\Delta=33^{\circ} 08^{\prime} \rightarrow \Delta / 2=16^{\circ} 34^{\prime}$
- Radius of circular curve $=1000 \mathrm{~m}$
- Chainage of $\mathrm{I}=1530.686 \mathrm{~m}$
- Peg interval for transition curve $=20 \mathrm{~m}$
- Peg interval for circular curve $=50 \mathrm{~m}$

$$
\begin{aligned}
& \alpha=\frac{V^{3}}{L R} \rightarrow L=\frac{V^{3}}{\alpha R}=\frac{30^{3}}{0.3 \times 1000}=90.0 \mathrm{~m} \\
& \text { Shift }, S=\frac{L^{2}}{24 R}=\frac{90^{2}}{24 \times 1000}=0.338 \mathrm{~m}
\end{aligned}
$$

Tangent length $\mathrm{IT}=(\mathrm{R}+\mathrm{S}) \tan (\Delta / 2)+(\mathrm{L} / 2)$

$$
=342.580
$$

- $\phi 1=\mathrm{L} / 2 \mathrm{R} \mathrm{rad}=90 /(2 \mathrm{x} 1000) \mathrm{x}(180 / \pi)=2^{\circ} 34^{\prime} 42^{\prime \prime}$
- Angle subtended by T1- T2 $=\theta=\Delta-2 \phi 1=27^{\circ} 58^{\prime} 36^{\prime}$
- Length of the curve, $1=(\pi R \theta / 180)=488.285 \mathrm{~m}$
- Chainage of $\mathrm{T}=$ Chainage of $\mathrm{I}-\mathrm{IT}=1188.105 \mathrm{~m}$
- $\quad=59+8.105$ chains for peg interval 20 m
- Chainage of $\mathrm{T} 1=$ Chainage of $\mathrm{T}+\mathrm{L}=1278,105 \mathrm{~m}$
- $\quad=25+28.105$ chains for peg interval 50 m
- Chainage of $\mathrm{T} 2=$ Chainage of $\mathrm{T} 1+1=1766.390 \mathrm{~m}$
- $\quad=35+16.390$ chains for peg interval 50 m
- $\quad=88+6.390$ chains for peg interval 20 m
- Chainage of $\mathrm{U}=$ Chainage of $\mathrm{T} 2+\mathrm{L}=1856.390 \mathrm{~m}$
- $\quad=92+16.390$ chains for peg interval 20 m
- Length of the first sub chord for transition

$$
(59+20)-(59+8.105)=11.895 \mathrm{~m}
$$

- Length of first sub chord for circular curve
- $(25+50)-(25+28.105)=21.895 \mathrm{~m}$
- Length of last sub chord for circular curve
- $(35+16.390)-(35+0)=16.390 \mathrm{~m}$

Deflection angle for transition curve

$$
\delta=\frac{1800 l^{2}}{\pi R L}=0.006366 l^{2} \mathrm{~min}
$$

- Deflection angle for circular curve

$$
\delta=1718.9 \frac{c}{R} \min
$$

## Setting out data for $1^{\text {st }}$ transition curve

| Point | Chainage <br> $(\mathrm{m})$ | Chord length <br> $(\mathrm{m})$ | $l$ <br> $(\mathrm{~m})$ | Deflection angle <br> $(\delta)$ |
| :---: | :---: | :---: | :---: | :---: |
| $0(\mathbf{T})$ | 1188.105 | 0.0 | 0.0 | 0.0 |
| 1 | 1200.000 | 11.895 | 11.895 | $0^{\circ} 00^{\prime} 54^{\prime \prime}$ |
| 2 | 1220.000 | 20 | 31.895 | $0^{\circ} 06^{\prime} 29^{\prime \prime}$ |
| 3 | 1240.000 | 20 | 51.895 | $0^{\circ} 17^{\prime} 09^{\prime \prime}$ |
| 4 | 1260.000 | 20 | 71.895 | $0^{\circ} 32^{\prime} 54^{\prime \prime}$ |
| $5(\mathbf{T 1})$ | 1278.105 | 18.105 | 90.000 | $0^{\circ} 51^{\prime} 34^{\prime \prime}$ |

## Setting out data for circular curve

| Point | Chainage <br> $(\mathrm{m})$ | Chord <br> length $(\mathrm{m})$ | Tangential <br> angle $(\delta)$ | Deflection <br> angle $(\Delta)$ |
| :---: | :---: | :---: | :---: | :---: |
| $5 \mathbf{T 1}$ | 1278.105 | 0.0 | 0.0 | 0.0 |
| 6 | 1300.000 | 21.895 | $0^{\circ} 37^{\prime} 38.1^{\prime \prime}$ | $0^{\circ} 37^{\prime} 38^{\prime \prime}$ |
| 7 | 1350.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $2^{\circ} 03^{\prime} 35^{\prime \prime}$ |
| 8 | 1400.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $3^{\circ} 29^{\prime} 32^{\prime \prime}$ |
| 9 | 1450.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $4^{\circ} 55^{\prime} 28^{\prime \prime}$ |
| 10 | 1500.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $6^{\circ} 21^{\prime} 25^{\prime \prime}$ |
| 11 | 1550.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $7^{\circ} 47^{\prime} 22^{\prime \prime}$ |
| 12 | 1600.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $9^{\circ} 13^{\prime} 18^{\prime \prime}$ |
| 13 | 1650.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $10^{\circ} 39^{\prime} 15^{\prime \prime}$ |
| 14 | 1700.000 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $12^{\circ} 05^{\prime} 12^{\prime \prime}$ |
| 15 | 1750.766 | 50 | $1^{\circ} 25^{\prime} 56.7^{\prime \prime}$ | $13^{\circ} 31^{\prime} 08^{\prime \prime}$ |
| $16 \mathbf{T 2}$ | 1766.390 | 16.390 | $0^{\circ} 28^{\prime} 10.4^{\prime \prime}$ | $13^{\circ} 59^{\prime} 19^{\prime \prime}$ |

## Setting out data for 2 nd Transition curve

| Point | Chainage <br> $(\mathrm{m})$ | Chord <br> length $(\mathrm{m})$ | $l$ <br> $(\mathrm{~m})$ | Deflection <br> angle $(\delta)$ |
| :---: | :---: | :---: | :---: | :---: |
| $16 \mathbf{T 2}$ | 1766.390 | 13.610 | 90.000 | $0^{\circ} 51^{\prime} 34^{\prime \prime}$ |
| 17 | 1780.000 | 20.000 | 76.390 | $0^{\circ} 37^{\prime} 09^{\prime \prime}$ |
| 18 | 1800.000 | 20.000 | 56.390 | $0^{\circ} 20^{\prime} 15^{\prime \prime}$ |
| 19 | 1820.000 | 20.000 | 36.390 | $0^{\circ} 08^{\prime} 26^{\prime \prime}$ |
| 20 | 1840.000 | 16.390 | 16.390 | $0^{\circ} 01^{\prime} 43^{\prime \prime}$ |
| $21 \mathbf{U}$ | 1856.390 | 0.0 | 0.0 | 0.0 |

## Vertical Curve



Vertical curves (VC) are used to connect intersecting gradients in the vertical plane.

They should be of sufficiently large curvature to provide comfort to the driver, that is, they should have a low 'rate of change of grade'.

## Vertical curve formula

$$
r=\frac{g_{2}-g_{1}}{L} \quad y=\frac{\mathrm{rx}^{2}}{2}+g_{1 x}+\text { elevation of BVC }
$$

Where
$r \quad=$ rate of change of grade per section (\%)
g1 $=$ starting grade (\%)
g2 $=$ ending grade (\%)
$\mathrm{L}=$ length of curve (horizontal distance m )
$\mathrm{y} \quad=$ elevation of a point on the curve
$\mathrm{x}=$ distance in stations from the BVC (meters/100)
$\mathrm{BVC}=$ beginning of the vertical curve
$\mathrm{EVC}=$ end of the vertical curve

## Properties of a Vertical Curve

$>$ The difference in elevation between the BVC and a point on the $g_{1}$ grade line at a distance $X$ units (feet or meters) is $g_{1} X$ ( $g_{1}$ is expressed as a decimal).
The tangent offset between the grade line and the curve is given by $\mathrm{ax}^{2}$, where x is the horizontal distance from the BVC; (that is, tangent offsets are proportional to the squares of the horizontal distances).
The elevation of the curve at distance $X$ from the BVC is given (on a crest curve) by:

$$
B V C+g_{1} x-a x^{2}
$$

(the signs would be reversed in a sag curve).
The grade lines ( g 1 and g 2 ) intersect midway between the BVC and the EVC. That is, BVC to V $=1 / 2 L=V$ to EVC.
$>$ Offsets from the two grade lines are symmetrical with respect to the PVI.
> The curve lies midway between the PVI and the midpoint of the chord; that is, $\mathrm{Cm}=\mathrm{mV}$.

## Computation of Low or High Point on Curve

The locations of curve high and low points are important for drainage and bridge considerations. For example, on curbed streets catch basins must be installed precisely at the drainage low point.

It was noted earlier that the slope was given by the
expression

$$
\text { Slope }=2 a x+g 1
$$

The figure above shows a sag vertical curve with a tangent drawn through the low point; it is obvious that the tangent line is horizontal with a slope of zero; that is,

$$
\begin{gathered}
2 a x+g 1=0 \\
\text { Since } 2 a=A / L \\
x=-g 1 L / A
\end{gathered}
$$

where x is the distance from the BVC to the high or low point.

## Procedure for Computing a Vertical Curve

1. Compute the algebraic difference in grades: A
2. Compute the chainage of the BVC and EVC. If the chainage of the PVI is known,
$1 / 2 \mathrm{~L}$ is simply subtracted and added to the PVI chainage.
3. Compute the distance from the BVC to the high or low point (if applicable):

$$
x=-g 1 L / A
$$

and determine the station of the high/low point.
4. Compute the tangent grade line elevation of the BVC and the EVC.
5. Compute the tangent grade line elevation for each required station.
6. Compute the midpoint of chord elevation
\{elevation of BVC + elevation of EVC\}/2

## Procedure for Computing a Vertical Curve

7. Compute the tangent offset (d) at the PVI (i.e., distance Vm):
$d=\{$ elevation of PVI - elevation of midpoint of chord $\} / 2$
8. Compute the tangent offset for each individual station.

Tangent offset $=\{x /(L / 2)\}^{2} d$
where x is the distance from the BVC or EVC (whichever is closer) to the required station.
9. Compute the elevation on the curve at each required station by combining the tangent offsets with the appropriate tangent grade line elevations. Add for sag curves and subtract for crest curves.

## Example 3

- A vertical curve $\mathbf{1 2 0} \mathbf{~ m}$ long of the parabola type is to join a falling gradient of $\mathbf{1}$ in 200 to a rising gradient of $1 \mathbf{i n} \mathbf{3 0 0}$. If the level of the intersection of the two gradients is $\mathbf{3 0 . 3 6} \mathbf{~ m}$. Compute the levels at $\mathbf{1 5} \mathbf{- m}$ intervals along the curve.



## Solution

Chainage of $A=$ Chainage of $B-L / 2$

$$
=2000-60=1940 \mathrm{~m}
$$

Chainage of $C=$ Chainage of $B+L / 2$

$$
=2000+60=2060 \mathrm{~m}
$$

Elevation of A = Elev. $\mathrm{B}+(\mathrm{pL} / 200)$

$$
=30.36+(0.5 * 120 / 200)=30.660
$$

Elevation of $\mathrm{C}=$ Elev. $\mathrm{B}+(\mathrm{qL} / 200)$

$$
=30.36+(0.33 * 120 / 200)=30.56 \mathrm{~m}
$$

$$
\mathrm{r}=\frac{\mathrm{g}_{2}-\mathrm{g}_{1}}{\mathrm{~L}} \quad \mathrm{y}=\frac{\mathrm{rx}^{2}}{2}+\mathrm{g}_{1} \mathrm{x}+\text { elevation of } \mathrm{BVC}
$$

| Station | Chainage (m) | $\mathbf{x}(\mathbf{m})$ | $\mathbf{y}_{\mathbf{i}}$ |
| :---: | :---: | :---: | :--- |
| A (BVC) | 1940 | 0 | 30.660 |
| 1 | 1955 | 15 | 30.593 |
| 2 | 1970 | 30 | 30.541 |
| 3 | 1985 | 45 | 30.505 |
| 4 (above B) | 2000 | 60 | 30.485 |
| 5 | 2015 | 75 | 30.479 |
| 6 | 2030 | 90 | 30.490 |
| 7 | 2045 | 105 | 30.516 |
| C (EVC) | 2060 | 120 | $30.558 \approx 30.56$ |

## Example 4

Given that $\mathrm{L}=300 \mathrm{~m}, \mathrm{~g}_{1}=-3.2 \%, \mathrm{~g}_{2}=+1.8 \%$, PVI at $30+030$, and elevation $=465.92$. Determine the location and elevation of the low point and elevations on the curve at 50 m interval starting from BVC. 1 st $=100$

