DETAILING FOR ACOUSTICS

Peter Lord and Duncan Templeton with graphics by Aidan Potter

Second edition

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We are particularly grateful to the following:

Richard Cowell, Dr Judith Lang, Nils Jordan, Hadyn Bodycombe, and colleagues at BDP and University of Salford, Department of Applied Acoustics.

Material from CIRIA Report 1988, 'Sound Insulation of House Separating and External Walls (with lightweight masonry for thermal insulation)' is reproduced by permission of the Director of CIRIA.

ACKNOWLEDGEMENTS

Effective acoustic design—unfortunately still a Cinderella element of our architecture—depends heavily on detail. There are many references for guidance on the principles of good acoustic design, not enough tackling the details.

Here is a book which emphasizes details, and the authors set out to make it useful. Details, whether for sound separation, absorbent linings or impact isolation need to take due account of non-acoustic influences, and favourite solutions differ widely. Whether taken from product technical literature or prised from private collections these details represent a useful reference for all those involved with building.

I expect to refer to them often and hope they will help stimulate debate and development in a field where they are badly needed.

Richard Cowell Arup Acoustics

FOREWORD

There is paucity of practical material relating to architectural acoustics, compared with academic material dealing with the mathematics and physics of sound. This book is composed largely of guidance details intended for reference by architects, students, structural and services engineers and interior designers. Some knowledge of the theory of sound is assumed. Exhaustive coverage is not claimed, nor does the content replace the need for specialist aid. Component assembly and choice of materials are 'moving targets' and sheets could be added ad infinitum to this selection of standard and built examples.

Sources

Wherever possible laboratory test results have been obtained for the standard assemblies of materials: often the basic 'favourites' could be traced to a number of sources, with minor variations on a theme. Inevitably, for light partitions and ceilings in particular, manufacturers' information has been an important source of data. Such data should be treated with some caution as results may be given in the best light. The material presented has been checked as far as possible. Exact trade name specifications and references are given only where critical, as some products are subject to frequent change and development.

Format

The material comprises details of standard elements of building construction, assemblies of elements from projects and diagrams for assessing basics. Standard elements consider both sound insulation and sound absorption aspects. In the case of the former, a single value is normally given; for sound reduction, values are in the range 100 – 3150 Hz (with values listed for octaves, ie 125, 250, 500, 1000, 2000, and 4000 Hz). The scale of details as originally drawn is generally 1:5 unless noted otherwise, but all drawings are reproduced at reduced scale—use the drawn scale on each sheet for reference. Details of specialist components—eg suspended discs—illustrate specific usage and are not for copying on another project: we want to encourage dialogue with acoustic consultants, not replace it.

Content

The stated performance of the sound insulation of component assemblies is not intended to assign each a definite value. A particular assembly does not have a 'magic number' because its performance will depend on the context of use. Taking a partition type as an example, the sound insulation performance depends not only on its sectional constituents but on its size, degree of restraint at all sides, flanking effects and receiving room absorption. The values stated are only an average and two elements with the same average may have widely varying sound transmission at a particular frequency. For this reason, some important examples have their performance illustrated throughout the frequency range.

The single-figure values are to be used to provide a choice of comparable elements of construction. consistent in acoustical terms. A 'kit of parts' of elements can be put together where no part of the whole assembly is significantly weaker than the rest in performance. Doors and windows are problematic in that they are inherently lighter and gap-prone, but all is not lost when doors and windows are not up to the performance of the surrounding walls, floors and ceiling, and composite performance of assemblies can be assessed. A philosophy that the whole is only as good as the weakest link is analogous to components in a sound-reproduction system. Care in detailing junctions is particularly important where discontinuous construction details are used to achieve good sound isolation. Cost-cutting exercises through the design stage should not allow part of the 'kit' to be downrated to meet budget.

In the case of sound-absorption values, the figures should be used together with the tabulated values to sum the total effect of absorption in a particular space. In a large-area space, for example, an open-plan office, the characteristics of the ceiling and floor will be of particular concern.

Information can only reflect the current 'state of the art'. There are exciting developments in materials technology, for instance in the development of thin but very effective isolating membranes. In a future of



lighter buildings and higher external noise levels, such materials could be a valuable asset to the designer.

Notes on 2nd edition

The second edition of this collection of details gives us the opportunity to add, update, or correct material. In particular the new UK Building Regulations made our guidance on the old Part G obsolete and mark a change in emphasis. The old Regulations needed diagrams just to explain the meaning of the many subparagraphs and were a confusing mixture of deemed-to-satisfy provisions, not necessarily meeting the performance figures also meant to apply. The new Regulations are commendably practical and clearly set out.

We have, therefore, included test results of walls and floors illustrating some of the favoured permutations of materials. As a matter of common sense, it may be observed that not all combinations are advisable, for example, certain substantial floors should not be used with certain lightweight walls.

The new Regulations endorse the use of built-up layers of plasterboard within partitions, floor deck linings, and ceilings. The authors can vouch for the excellent performance possible from wide-spaced double or triple plasterboard layers with a bit of absorption in the cavity. The practical advantages of plasterboard are its density (750 kg/m³), fire resistance, ready availability, low cost, ease of fixing, and its sealability by skimming, overlap of successive panel layers, and caulk.

Design process

For basic knowledge, use a primer text: eg the classic 'Acoustics Noise and Buildings', 4th Edition, Parkin, Humphreys and Cowell. The details we give here are intended to help at the practical rather than the crucial concept end of the acoustical design process. Stages of acoustical design input are summarized to show the total picture through a project. Acoustic consultants should be approached where a close check of characteristics is required.

1 Briefing

The client may state required standards in the finished

building or, more likely, the functions stated dictate the fabric performance. Target criteria should be set at this stage.

2 Site selection

If a choice of sites is available noise sources may be included with other environmental criteria in a scoring matrix to determine the most suitable.

3 Noise survey

Background noise levels may be taken to assist brief-making studies or to determine the best position of a building on site. Quantification of adjacent noise sources may influence the design of the external envelope, in order to avoid noise intrusion.

4 Outline design

The form of the building may allow 'buffer' screening of sensitive spaces, and the arrangement of rooms may allow those requiring quiet conditions to be remote from noisy rooms, with fenestration limited and not facing any external noise source.

5 Detail design

In order that rooms can be sized to suit function and good aural reception, proportion, volume/occupant. reverberation time and surface geometry may be considered and adjusted. The quantity, shape and specification of finishes may be made optimal to required sound reflection, diffusion or absorption properties. The required separation between rooms or to outside noise is designed-in by each element having adequate sound insulating properties. Noise-control standards for services should be compatible with fabric-design standards: air-conditioning systems, plumbing, lighting, generators and switchgear plant are frequent noise culprits in large buildings. Design of specialist sound systems to suit the acoustics of the spaces is finalized at this stage.

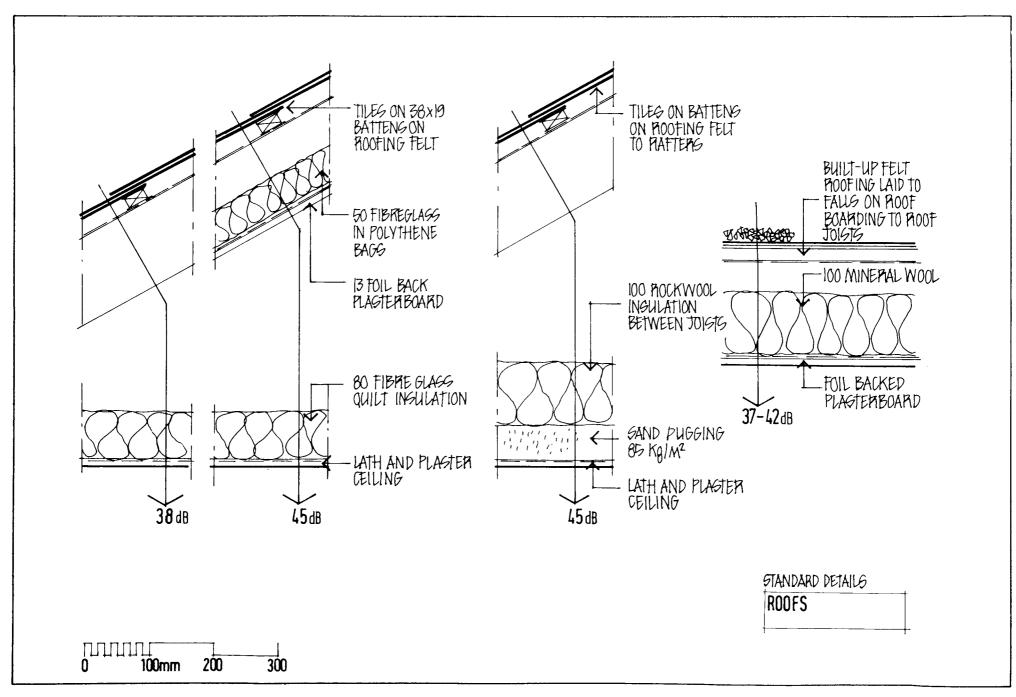
6 Supervision

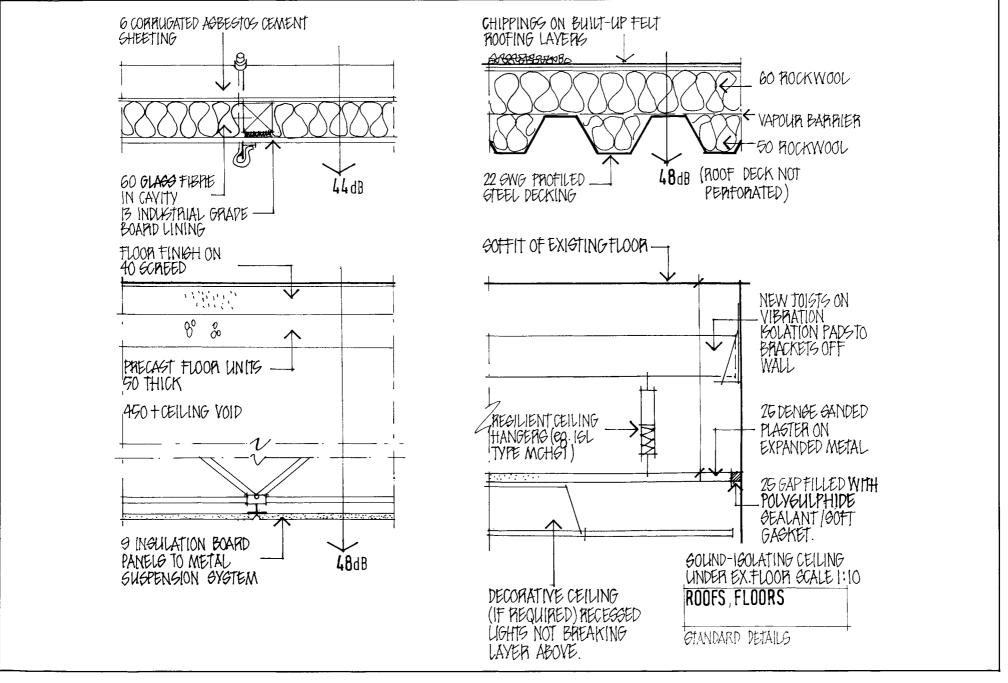
Care must be taken in getting many of the assemblies shown built properly, as some principles go against the grain of normal building practice—discontinuous construction at junctions and cavity walls with no ties will tempt the average contractor used to tying the whole lot together for stability.

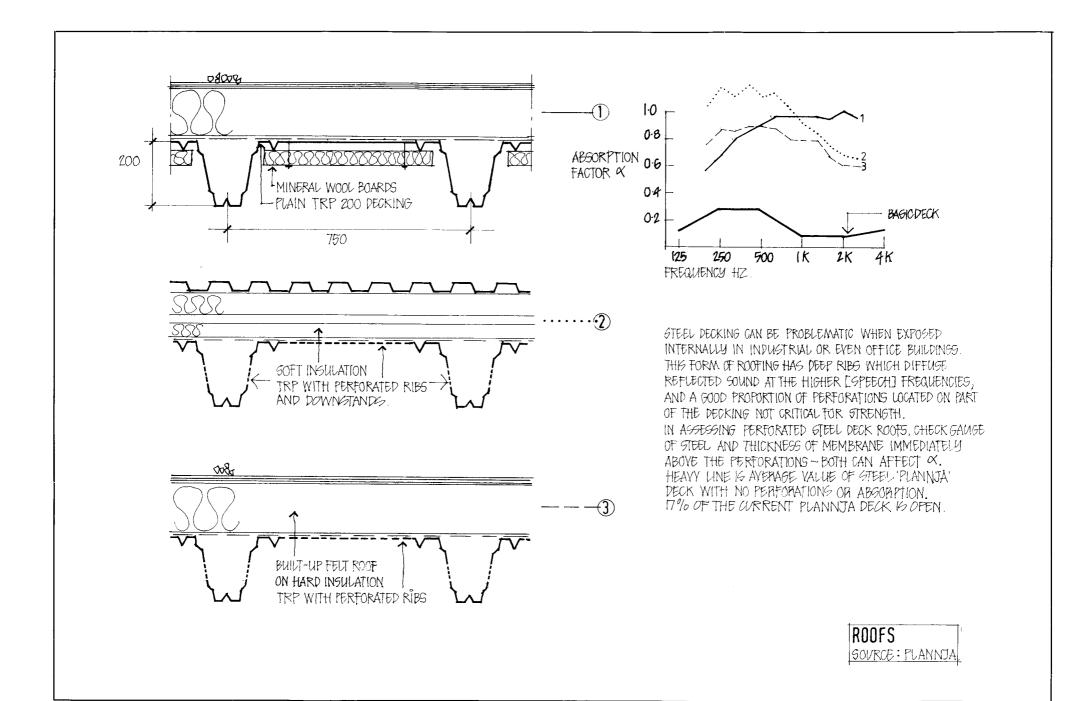
7 Commissioning

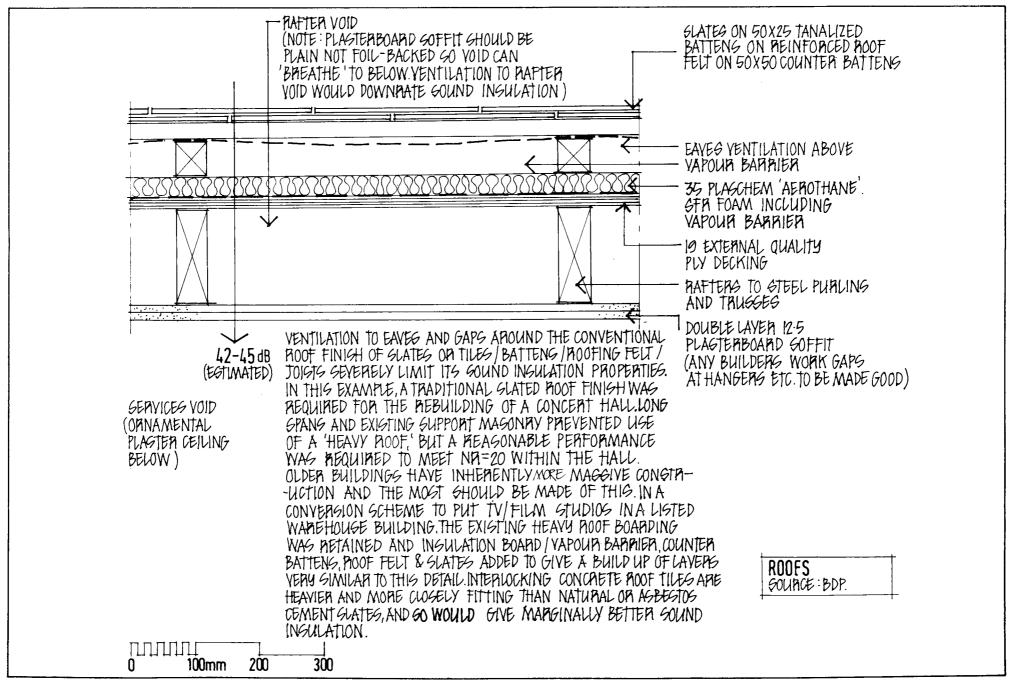
Testing and tuning of services systems and sound systems and checking that sound insulation standards are provided in practice are advisable as the logical follow-up to care in detailing.

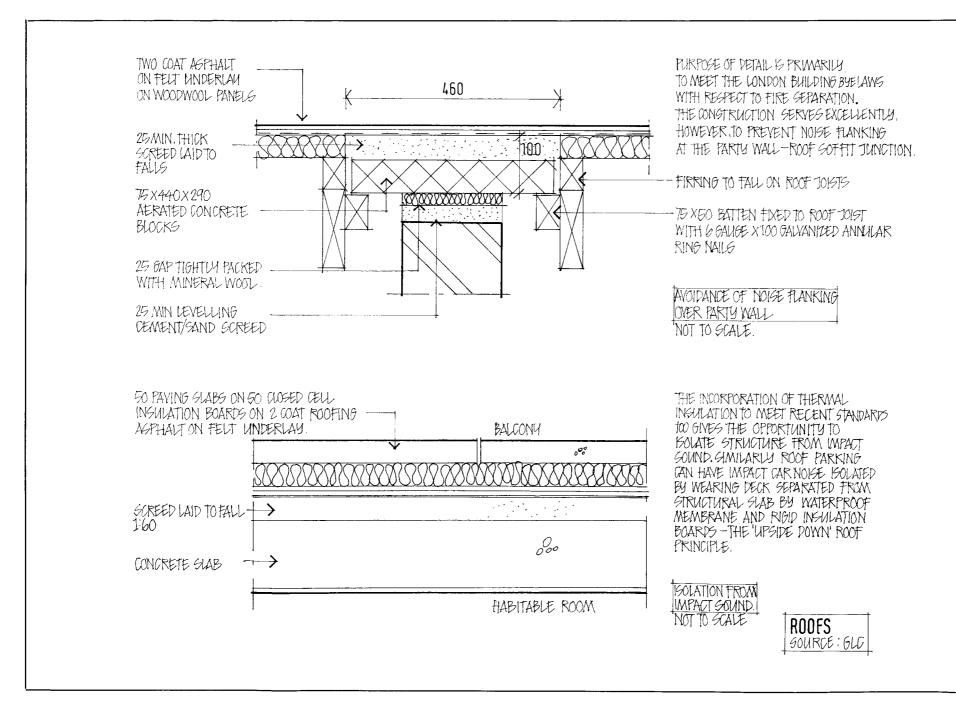
ROOFS



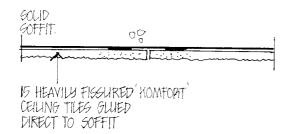








CEILINGS

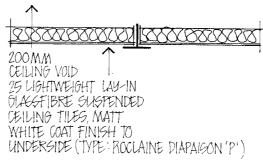


0.09 0.30 0.82 0.95 0.76 0.61



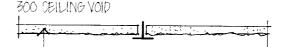
15 HEAVILY FIGGURED
CONCEALED GRID PLAGTER GYPTONE'
CEILING TILES METAL
SUSPENSION SYSTEM

0.30 0.35 0.40 0.55 0.80 0.70 ABSOMPTION FIGURES RELATE TO FREQUENCIES. 125tz. 250 500 1K 2K 4K



0.33 0.84 0.84 0.88 0.89 0.92

40 FIBREGLASS TILES OVER 400 VOID 0.70 0.75 0.65 0.75 0.60 0.35



15 FISSURED-FINISH ARMSTRONG 'CERAMGUARD'
KILN-FIRED MINERAL
FIBRE TILES (FOR USE
IN CORROSIVE OR HUMID
SITUATION ES.SWIMMING POOLS)

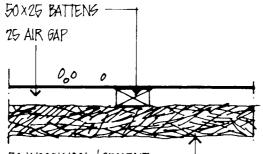
0.25 0.25 0.45 0.70 0.80 1.10

GTANDARD DETAILS
CEILINGS
SOUND ABSORPTION



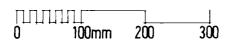
FABRIC COVER TO PROPRIETARY
PANELS 600 WIDE. PANELS.
19 PERFORATED MINERAL
FIBREBOARD BY ARMSTRONG.
50X25 BATTENS ON MASONRY—

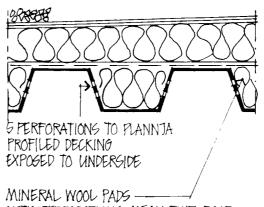
022 056 0.56 072 076 081



0.30 0.40 0.50 0.85 0.50 0.65 0.15 0.20 0.55 0.75 0.65 0.85 (NO AIR GAP)

ABSORPTION FIGURES RELATE TO FREQUENCIES 125 250 500 lk 2k 4k.

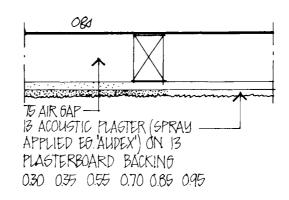




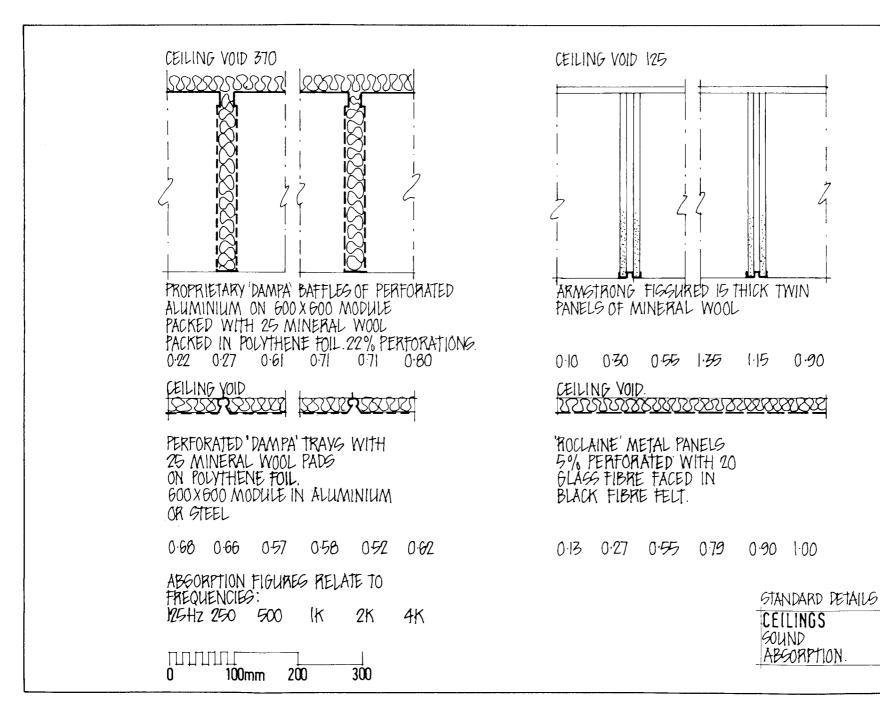
MINERAL WOOL PADS ————

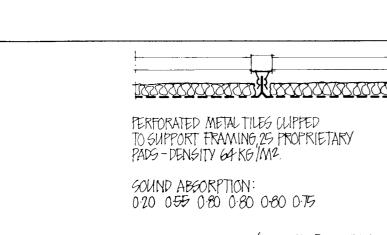
NOTE PERFORATIONS MEAN THAT ROOF
HAS POOR SOUND INSULATION PROPERTIES

0.20 0.50 0.80 0.85 0.60 0.50

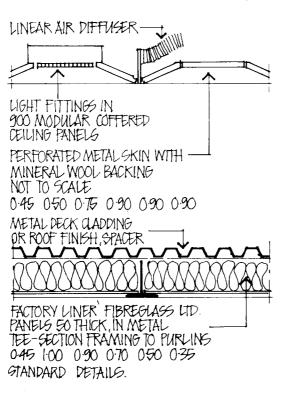








SOUND ATTENUATION (BS 2750 ROOM TO ROOM)
32 dB (40 dB FOR SOULD FACE TILE)

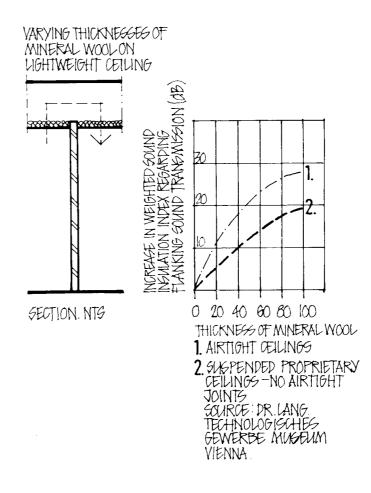


200

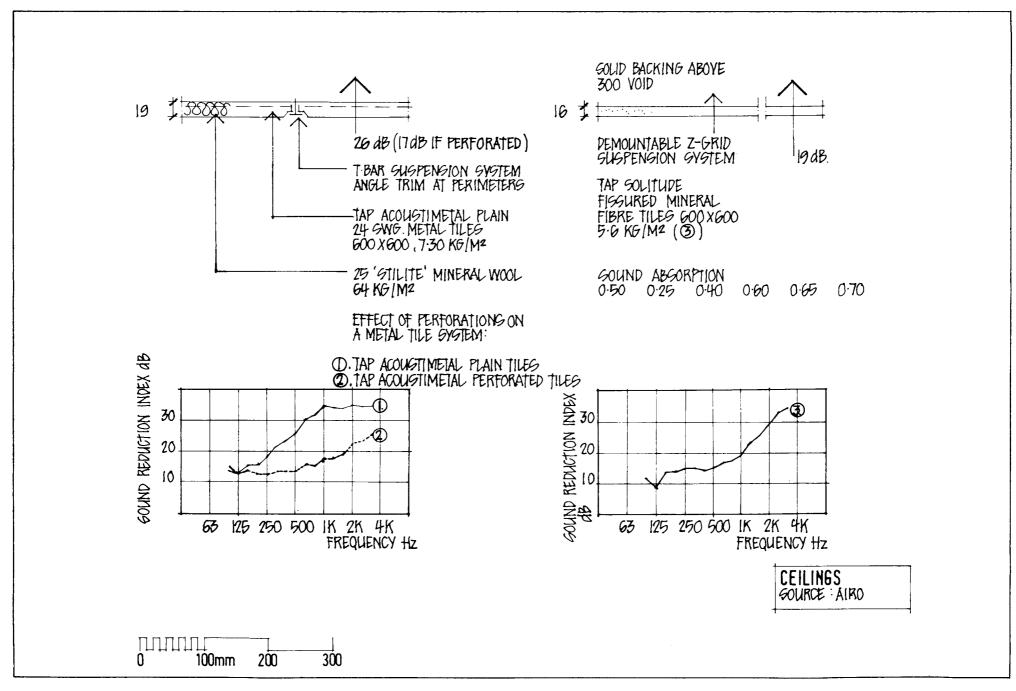
100mm

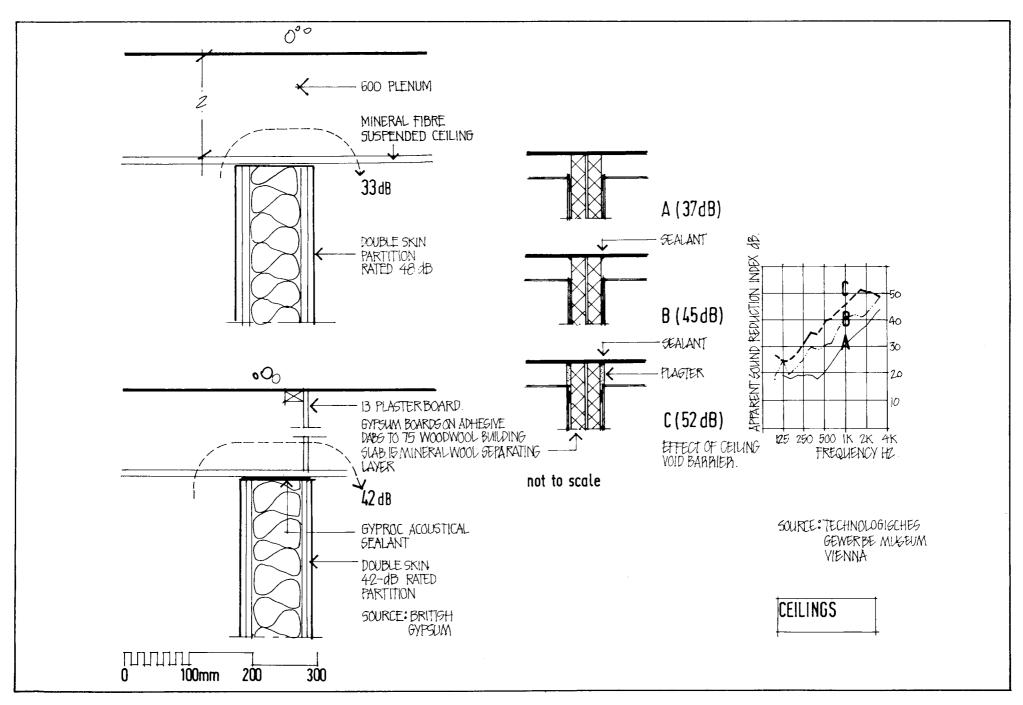
N

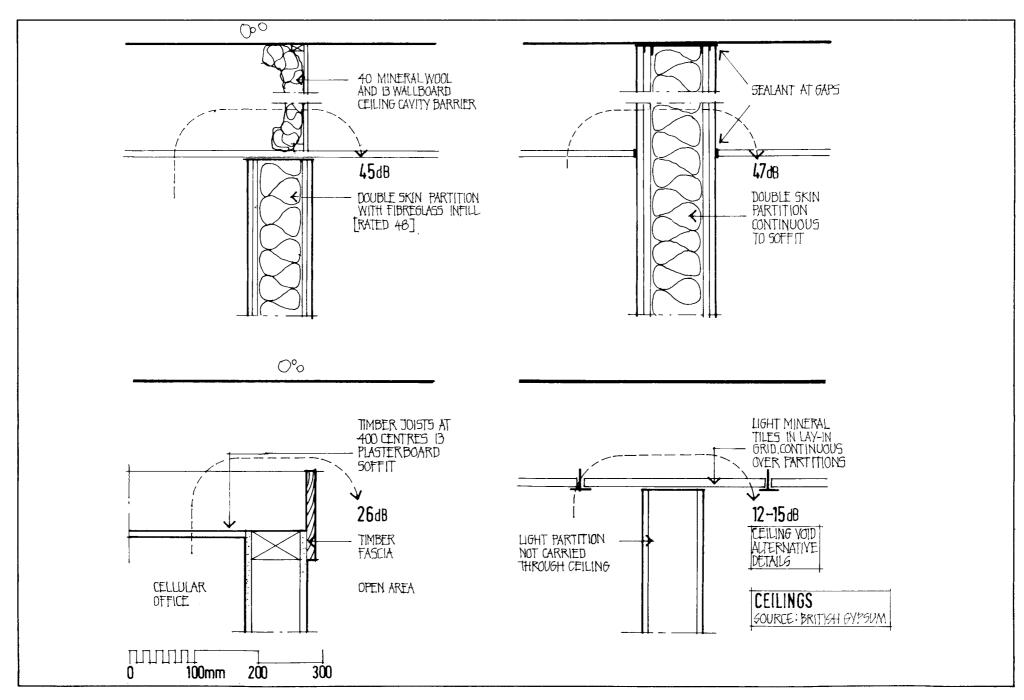
300

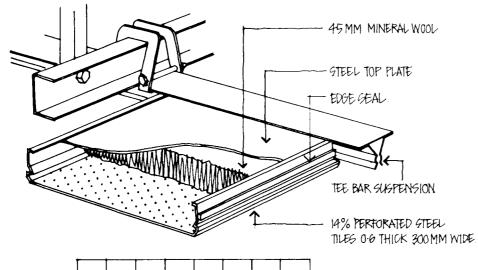


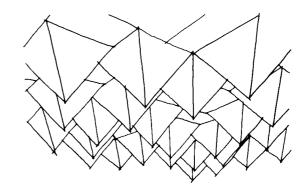
CEILINGS



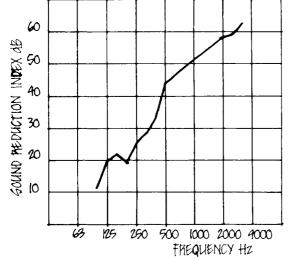








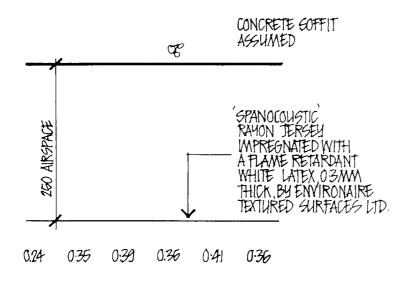
SPECIAL METAL CEILING UNITS GOO XGOO XO G THICK PYRAMIDS FORMING A SOUND DIFFUSING CEILING

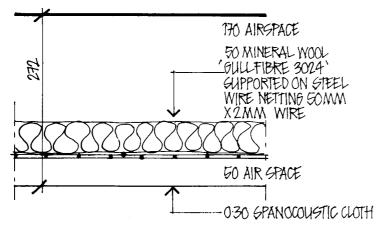


SOUND ABSORPTION 0.50 0.70 0.80 1.00 1.00 1.00

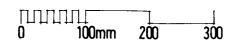
PROPRIETARY CEILING TILE FOR SOUND INSULATION AND SOUND ABSORBTION UNPERFORATED METAL TILES CAN GIVE PLOOM-TO-PLOOM (BG 2750) AVEPLAGE NORMALIZED GL. DIFFERIENCE 41 dB.

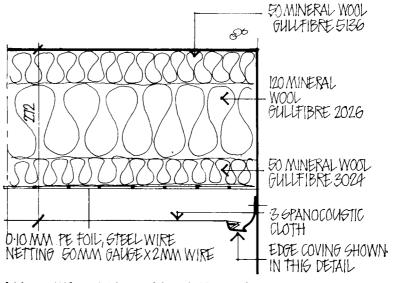






0.66 0.65 0.79 0.85 0.91 0.92 (TEGT STANDARD: 160/R354, SIMILAR TO BG 3638/1963)

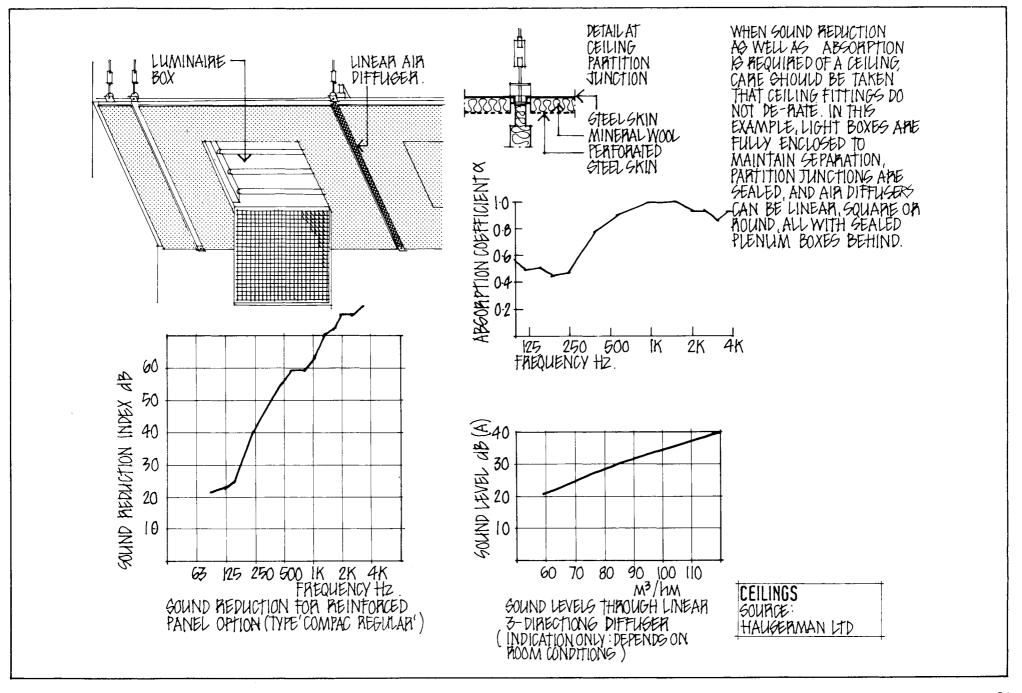




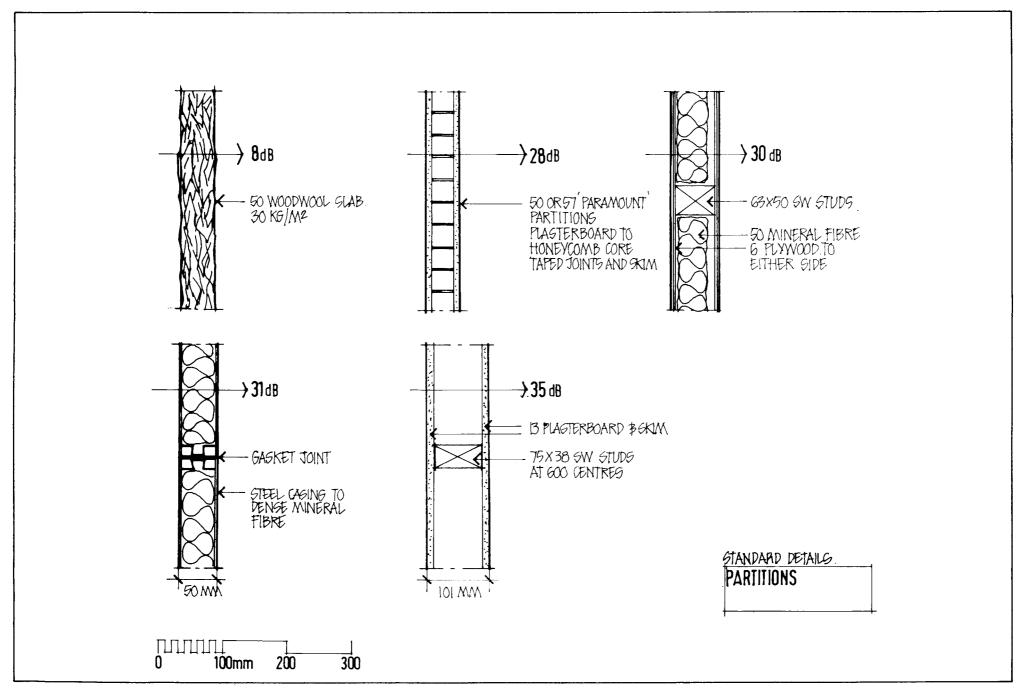
104 0.73 0.86 0.94 0.93 0.89

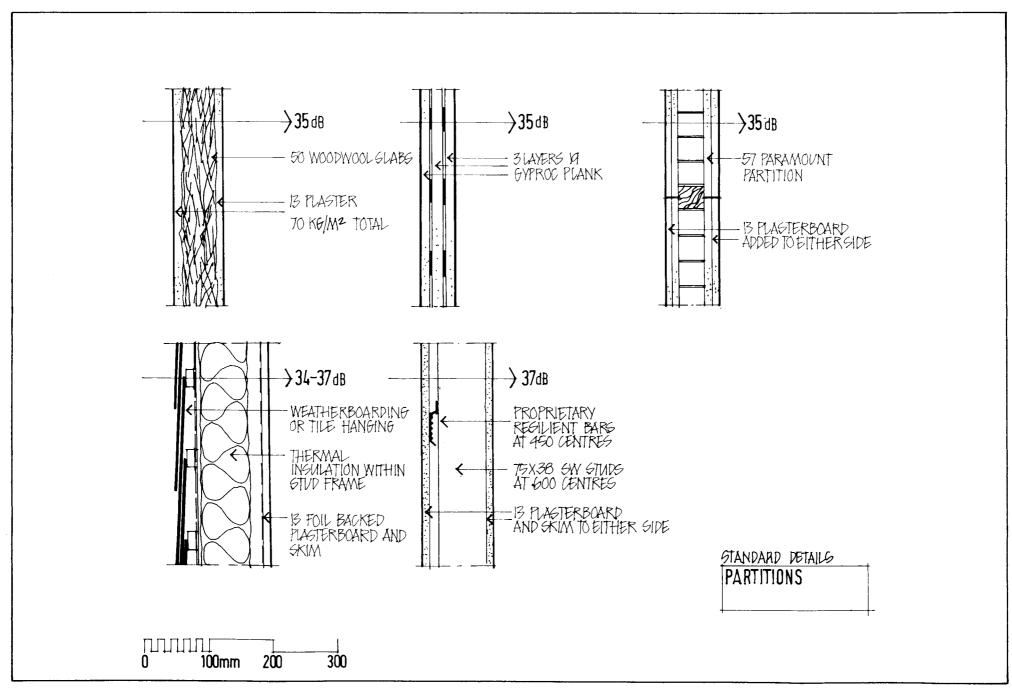
THE IS A RECENT INNOVATION TO THE LIKE MOIST TEXTILE MATERIAL IS GTRETCHED TO EDGE BATTENS AND A ONE-OFF EVAPORATION RESULTS IN A TAUT CEILING MEMBRANE LINAFFECTED BY SUBSEQUENT CHANGES IN HUMIDITY AND TEMPERATURE. CLAIMED LIFE EXPECTANCY IS 20 URS. NO FIRE PROTECTION OVEN BY THIS CEILING, WHICH IS TESTED TO BY 476: PART 7: CLASS]. A LIGHT CEILING OF THIS FORM MAY BE CONSIDERED IN REFURBISHMENT WHERE WEIGHT OF SUSPENDED CEILING WOULD BE PROBLEMATIC.

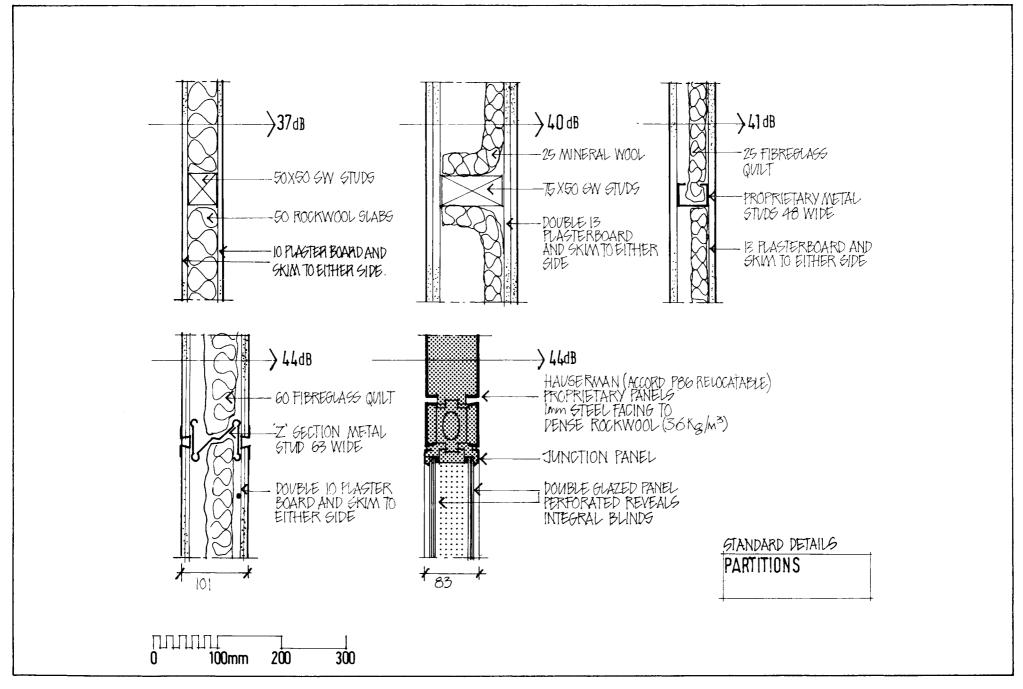
CEILINGS SOURCE UNIVERSITY OF TECHNOLOGY, LUNDSWEDEN

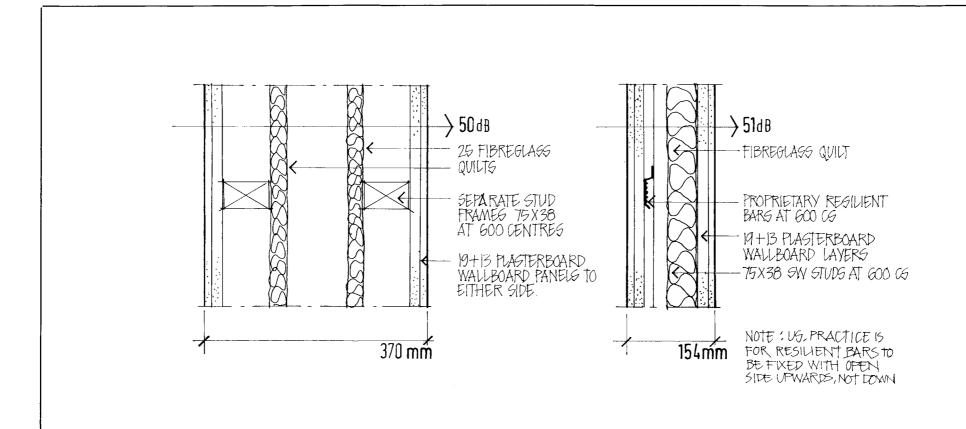


PARTITIONS



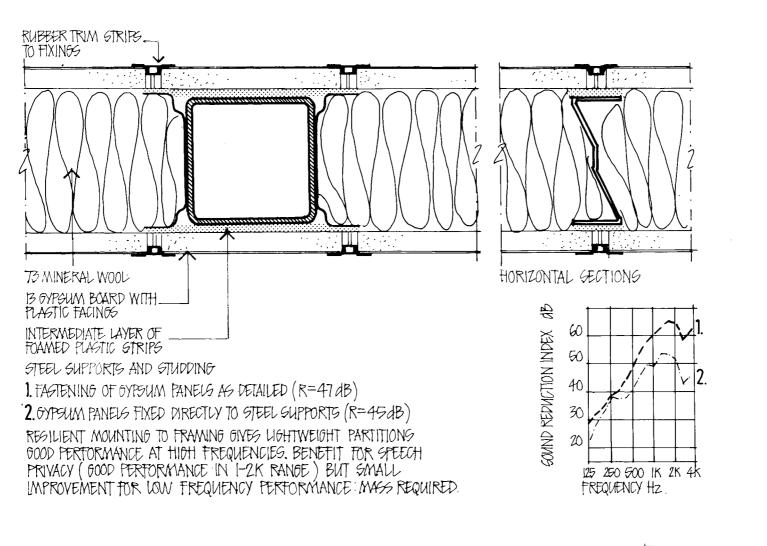




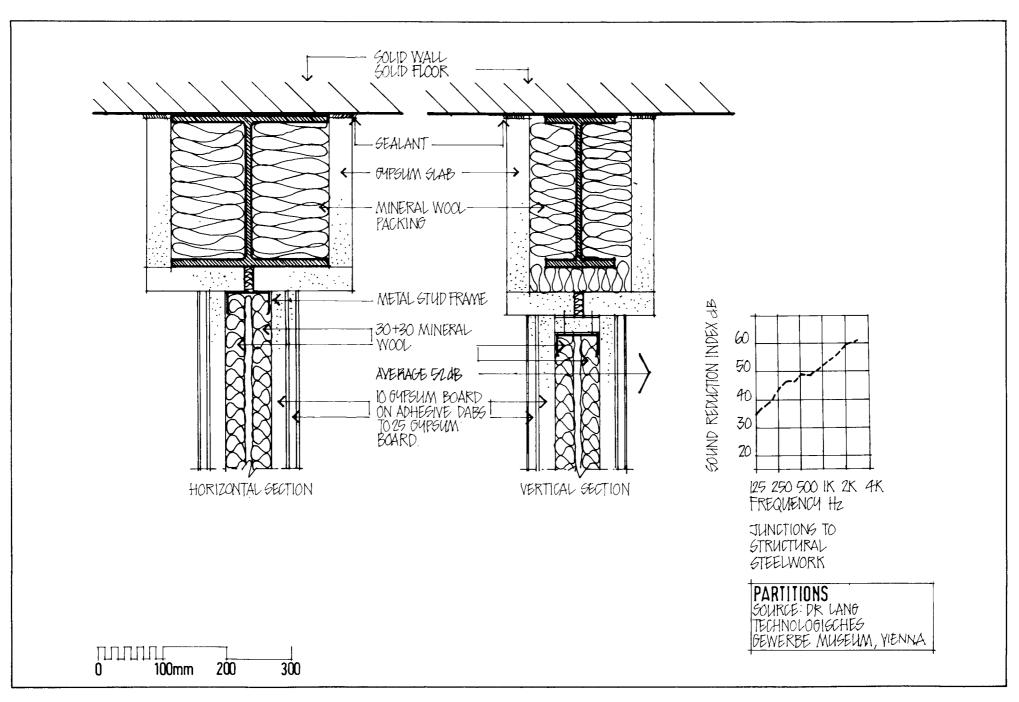


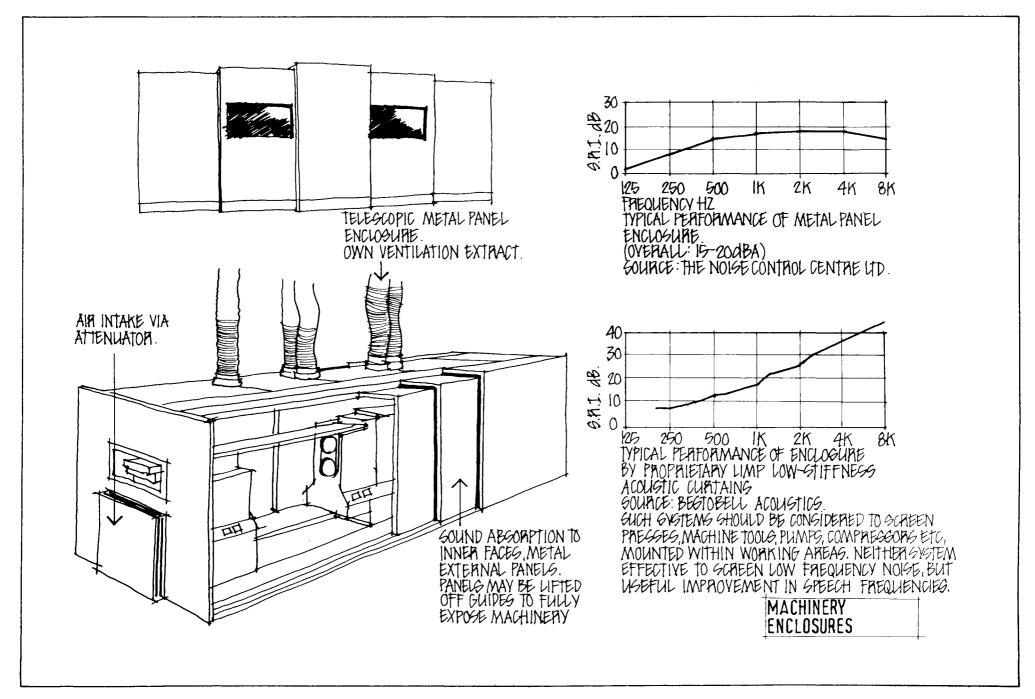
STANDARD DETAILS.

PARTITIONS

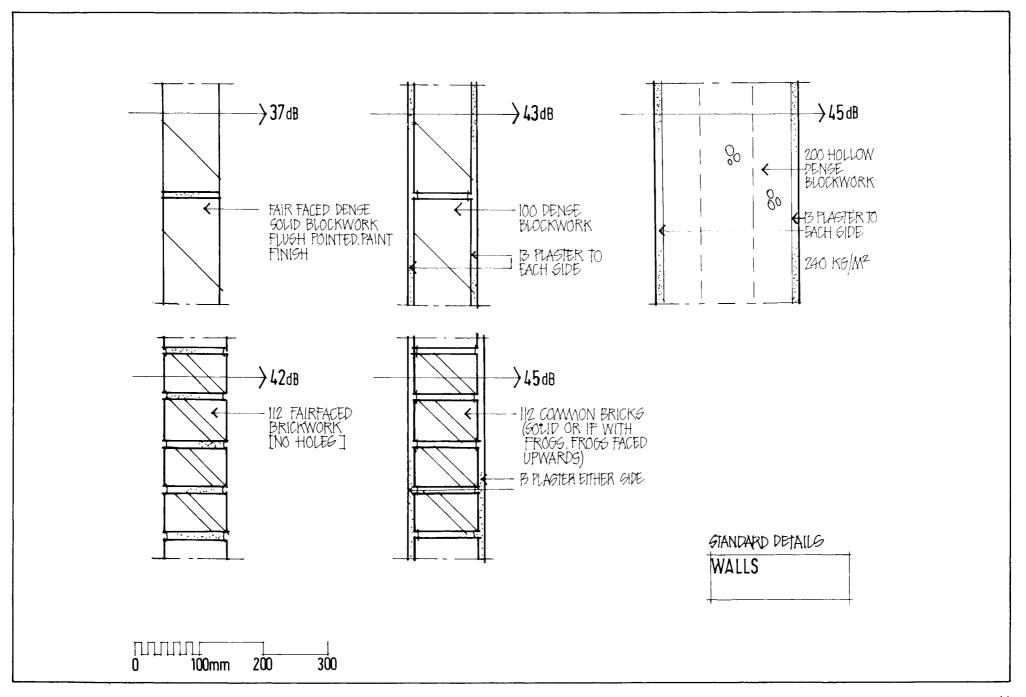


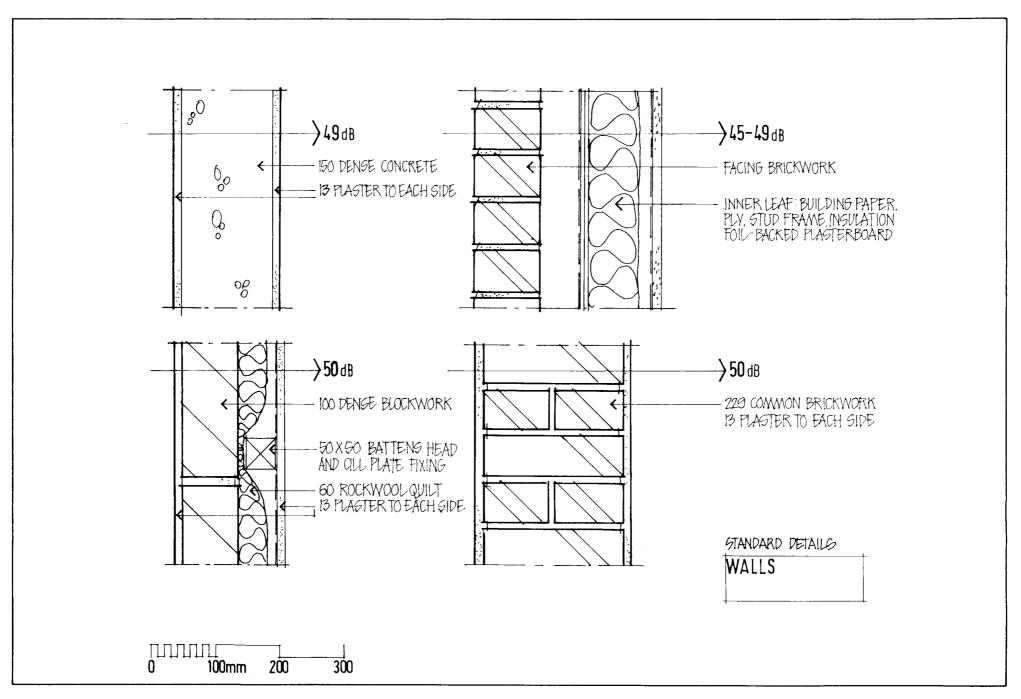


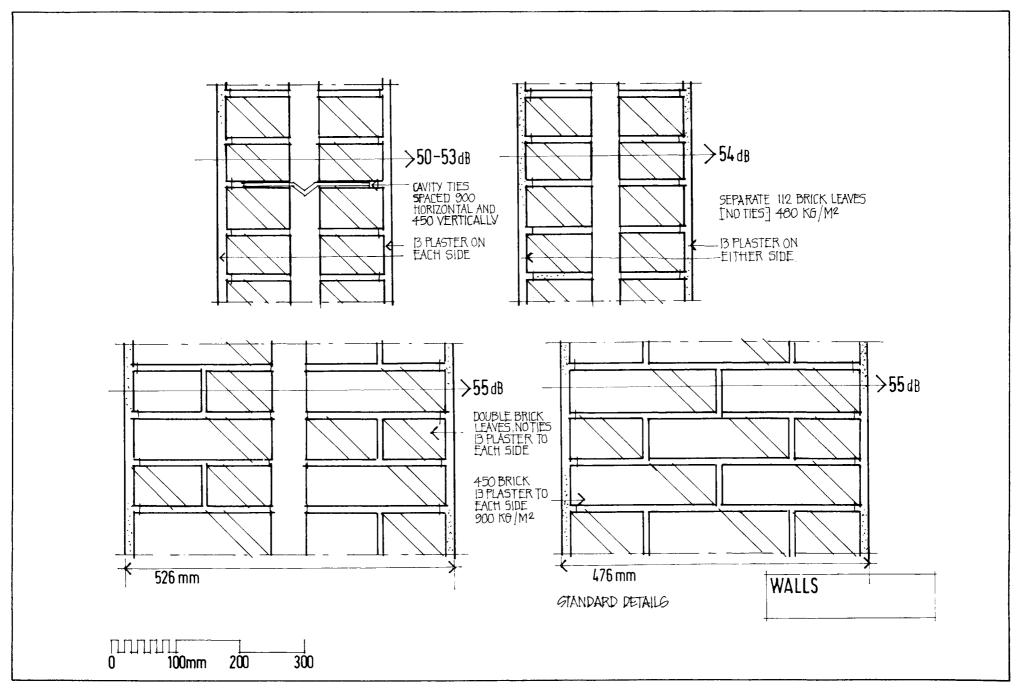




WALLS







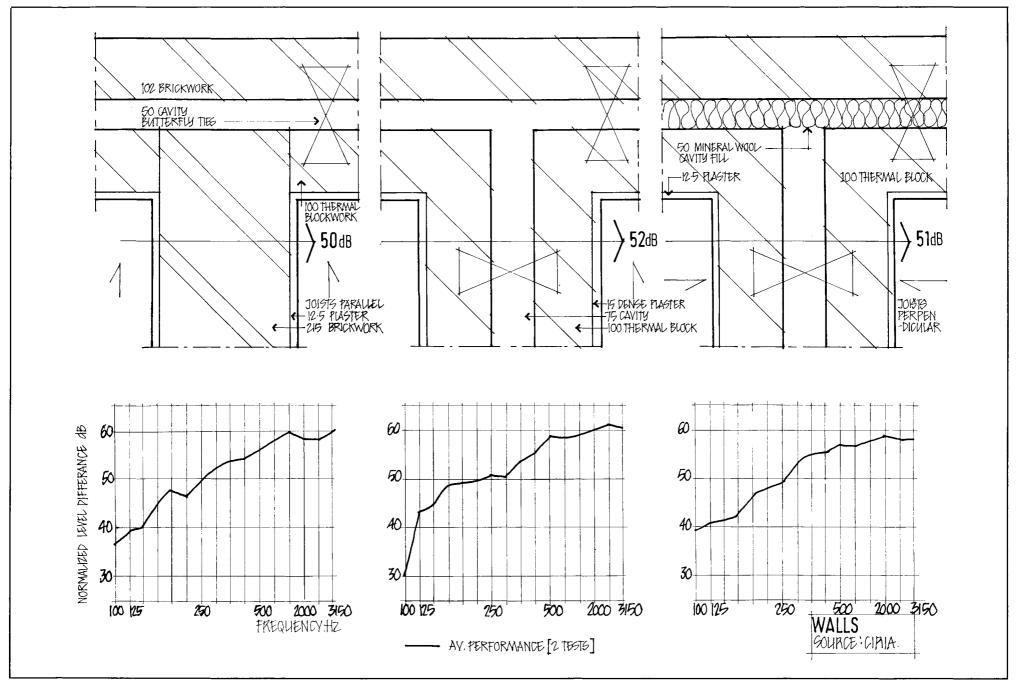
+10 +5 0 FREQUENCY HZ EXTERNAL AND SEPARATING WALL LINING EITHER: - 1 LAYER 9.5 PLASTERBOARD 2 LAYER 95 PLASTERBOARD (I LAYER TO EXTERNAL WALL) 12.5 LIGHTWEIGHT PLASTER 275 SOURCE: CIRIA REPORT 1988

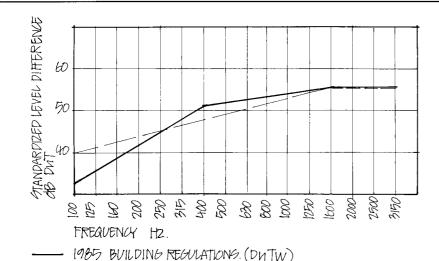
PARTY WALLS

AS WELL AS THE MASS OF SEPARATING AND EXTERNAL WALLS THE FOLLOWING ASPECTS AFFECT THE SOUND INSULATION THROUGH THE OPERATING WALLS

- (1.) TIEG. ABSENCE OF TIES CONSIDERABLY IMPROYES THE SOUND INSULATION. BUTTENFLY TIES PREFERABLE TO STRIP TIES.
- (2.) CAVITY INSULATION . 60-70 KG./M³ MINERAL WOOL LINING TO SEPARATING WALL CAVITY IMPROVES SOUND INSULATION BY IMPEDING SOUND TRACKING ACROSS THE CAVITY. (MUST BE LOOSELY PLACED IN CAVITY.)
- (3.) JOIST DIRECTION JOISTS PARALLEL TO SEPARATING WALLS HAYE IN TESTS GIVEN CONSISTENTLY HIGHER SOUND INSULATION THAN JOISTS PERPENDICULAR TO SEPARATING WALL
- 4. JOIST TIGHTNESS. RATHER THAN LOOSE POCKETS AT JOIST ENDS, CONSIDER USE OF JOIST HANGERS TO ALLOW THE WALL INTEGRITY TO BE MAINTAINED.
- 5) DRY LINING. THE EFFECT OF WALL FINISHES IS SHOWN AT LHS. 2 LAYERS TO SEPARATING WALL ARE NECESSARY TO IMPROYE ON PLASTER. I LAYER CAN ACTUALLY REDUCE SOUND INSULATION AT SOME FREQUENCIES BECAUSE OF RESONANCE.

WALLS	





--- 1976 BUILDING REGULATIONS MAX AAD 23 dB.

· PARTY WALLS (855821/1961/160717:1982)

GINGLE VALUE TAKEN FROM REFERENCE CURVE AT 500 Hz

REQUIREMENT IN AB.

INDIVIDUAL

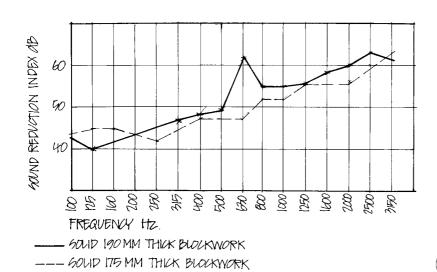
MEAN

49

<4 PAIRS OF TESTS 53 >4 PAIRS OF TESTS 52

UNFAVOURABLE DEVIATION IF MORE THAN BAB AT ANY ONE 13 OCTAVE FREQUENCY BAND.

THE NEW STANDARDS IN THE UK MEAN THAT FOR AIRBORNE SOUND INSULATION, FRANCE, DENMARK, SWEDEN AND THE NETHERLANDS NOW HAVE MORE STRINGENT CRITERIA TO BE MET IN HOUSING.



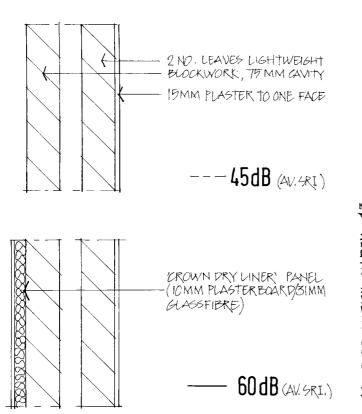
Rep	HILES	A STATE OF THE STA	THE WAY
41	90 100	150	GOUD HOLLOW
43	90 140	180	NOVOIDGOLID HOLLOW
46	190	240	HOLLOW
48	140	240	GOLID
50	190	340	GOLID

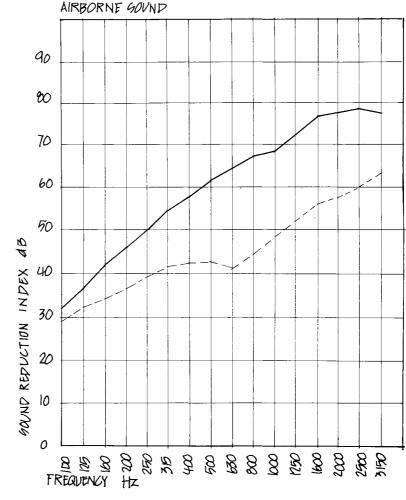
60UND ABGORPTION: 0.2 02 0.2 0.15 0.2 0.25 (UNPAINTED BLOCKWORK) OBLOCKWORK

(FORTICRETE DCM)

FOR SOUND INSULATION BLOCKWORK
BEST PLASTERED AS THE CLOSES
FISOURES, USING NON VOID SOLID
DOM BLOCKS. BEWARE SHRINKASE
CRACKS PARTICULARLY AT BEAM OR
COWMN JUNCTIONS.
TEST FINDINGS ARE FOR BLOCKWORK
LAID IN 11:6 (EMENT: LIME 'SAND MORTAR
AND PAINTED 2 LOATS. (UNPAINTED
PERFORMANCE !-2 AB LESS THROUGHOUT
FREQUENCY RANGE).

PARTY WALLS

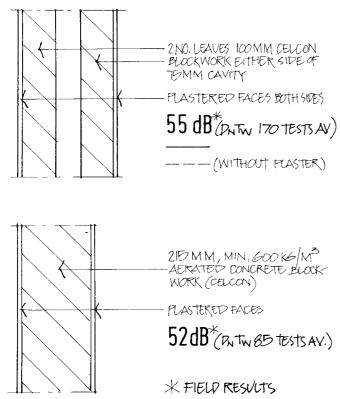




RESULTS FROM A TEST PROGRAMME ON THIS FORM OF LINING TO UPGRADE MASONRY WALLS INDICATES;
I, GOOD IMPROVEMENT BY LINING ONE SIPE ONLY (TO LINE BOTH SIDES IS OF LITTLE ADDITIONAL BENEFIT)
2. ADHESIVE NOT MECHANICAL FIXING OF PANELS HAS TO BE USED.

PARTY WALLS

GOURCE: PILKINGTON FIBREGUASSY UNIVERSITY OF SALFORD DEPT. OF APPLIED ACOUSTICES



AND WALLS

TYPICAL LABORATORY TEST RESULTS

PARTY WALLS

90

80

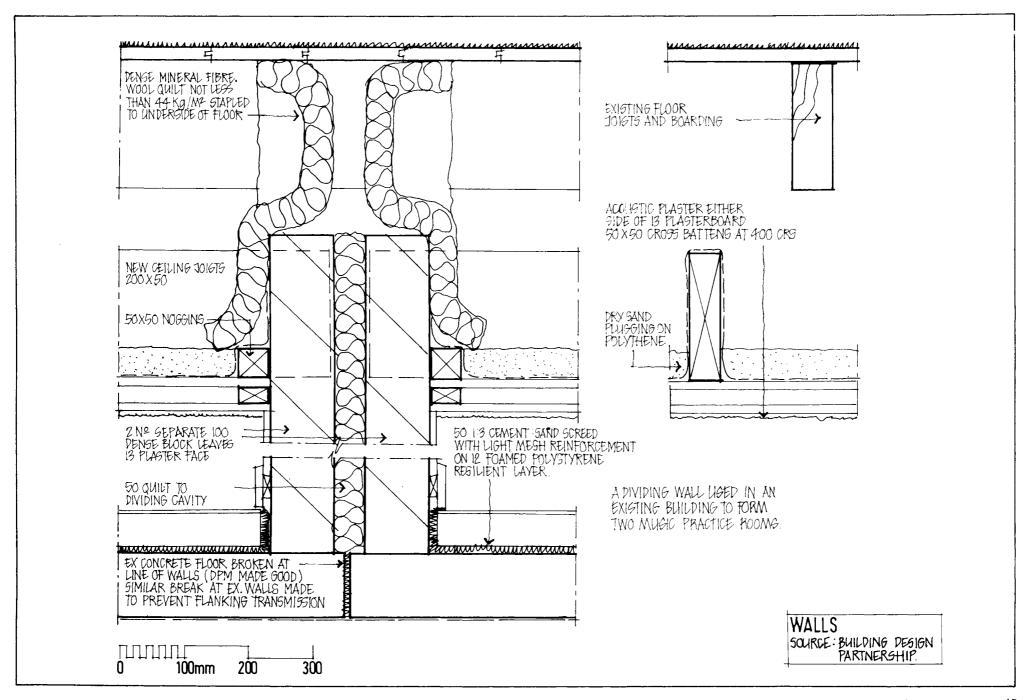
70

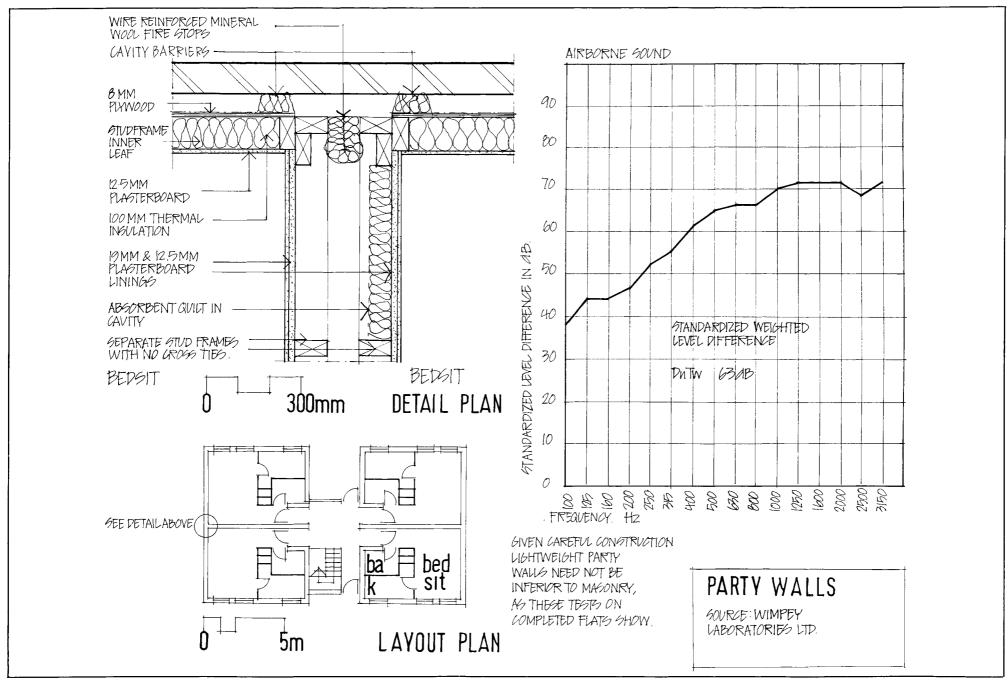
60

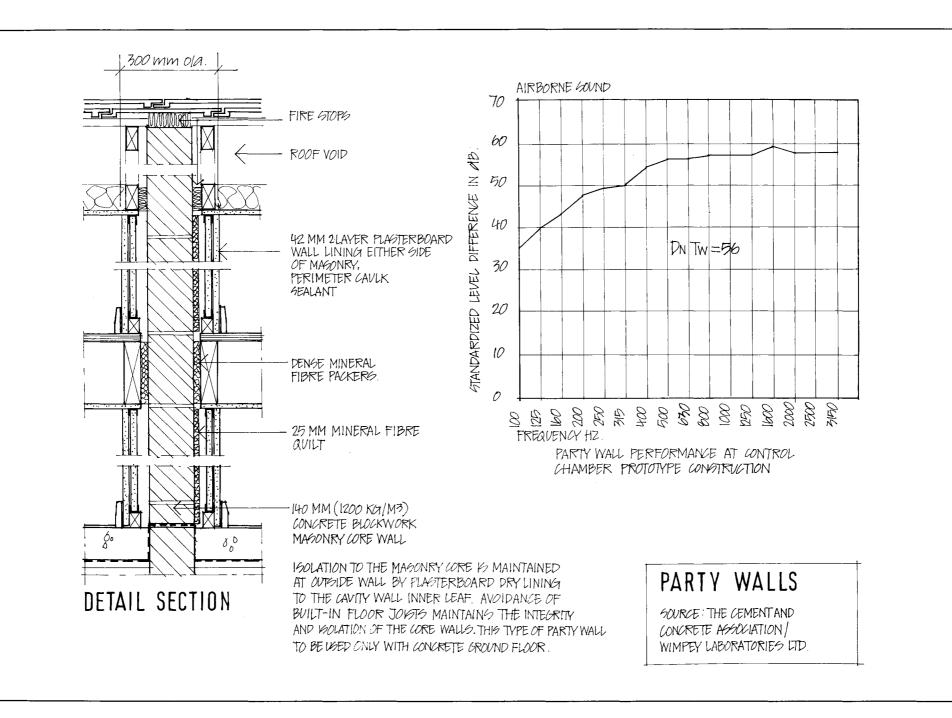
RESULTS COMPARE FAVOURABLY WITH TABLE L'SECTION 3/APPROVED DOCUMENT'E; BUILDING RECULATIONS 1985, AUTHOUGH THESE ARE NOT CONSTRUCTIONS SPECIFICALLY LISTED IN THE APPROVED DOCUMENT.

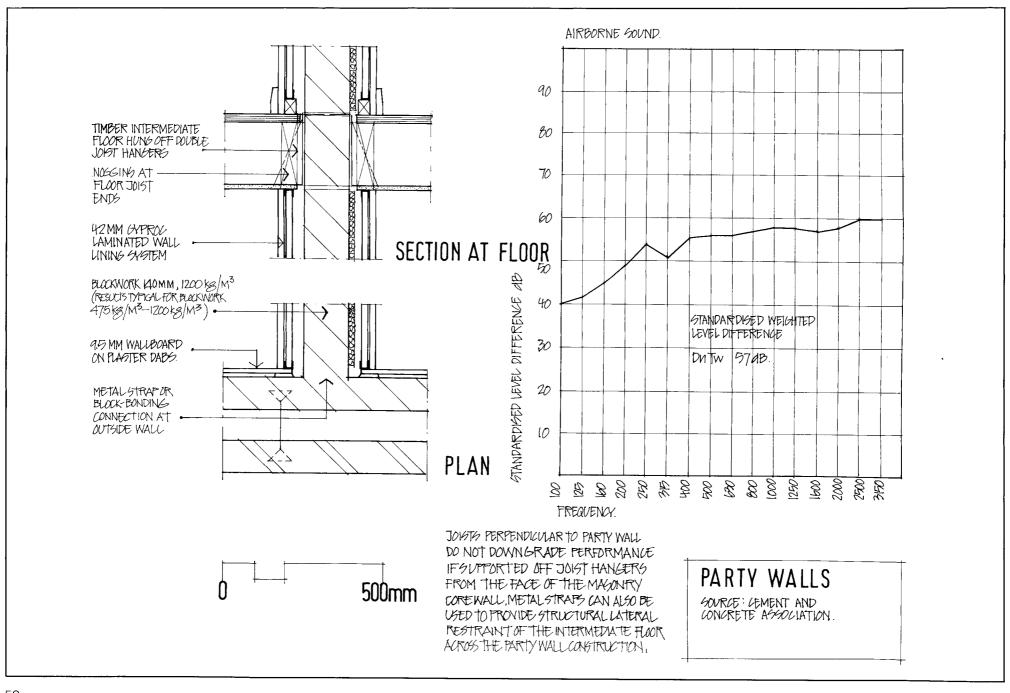
AIRO HAVE FOUND THAT A CORRECTION FACTOR OF BAB, APPLIES FOR FIELD RESULTS COMPARED WITH LABORATORY.

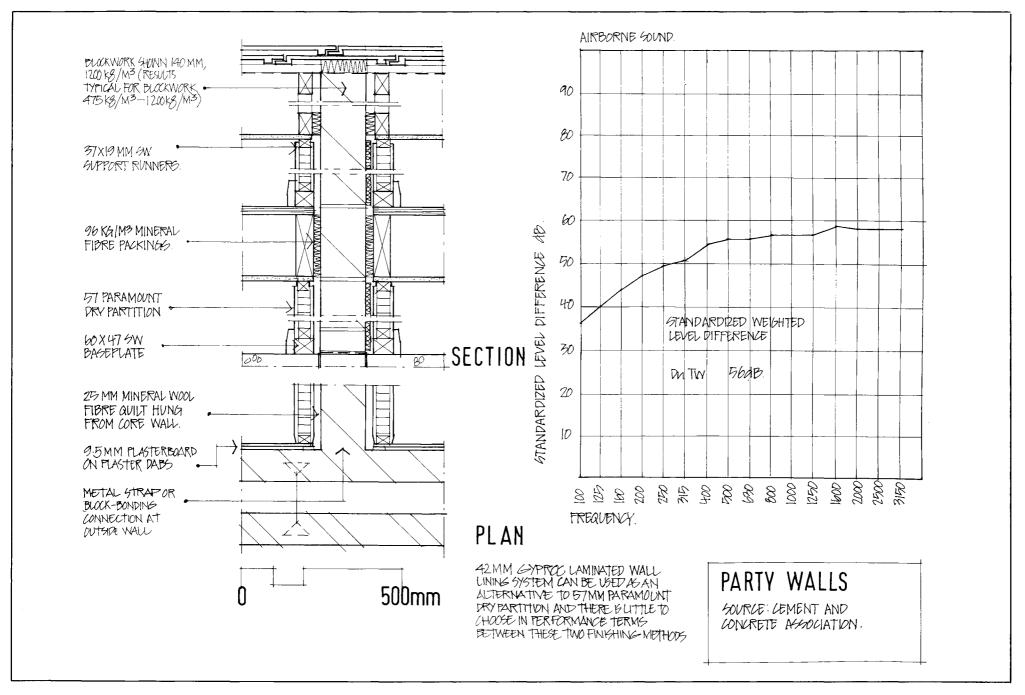
PARTY WALLS
GOURCE: CELCON LTD. /AIRO,

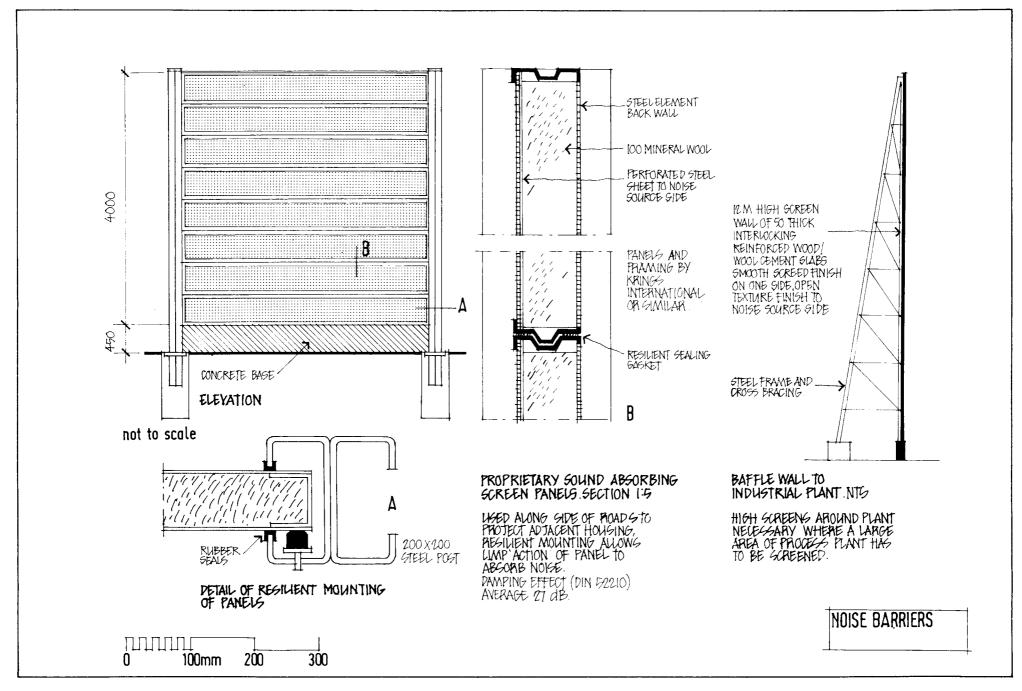






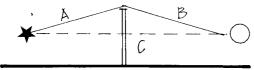




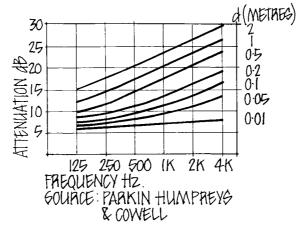




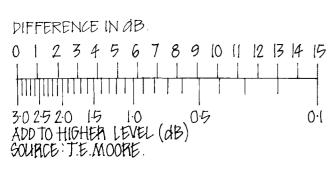
YARYING DIFFRACTION OVER A BARRIER AT DIFFERENT FREQUENCIES

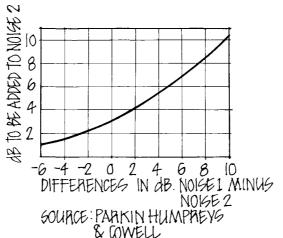


DIFFERENCE IN SOUND PATHS, d=A+B-C



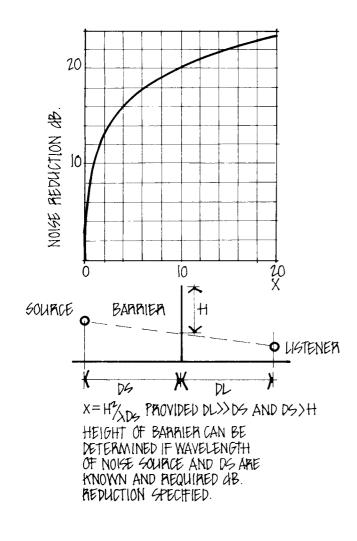
ATTENUATION DUE TO ECREENS IN OPEN AIR IS RELATED TO HOW MUCH FURTHER THE SOUND HAS TO TRAVEL AROUND THE SCREEN. FOR ATTENUATION DUE TO A FINITE SCREEN LENGTH, CARRY OUT PATH DIFFERENCE CALCULATIONS IN PLAN AS WELL AS SECTION AND COMBINE ATTENUATIONS WEIGHT OF SCREEN MATERIAL IS IMMATERIAL, BUT NEEDS TO BE SOUD FACED TO NOISE SIDE.

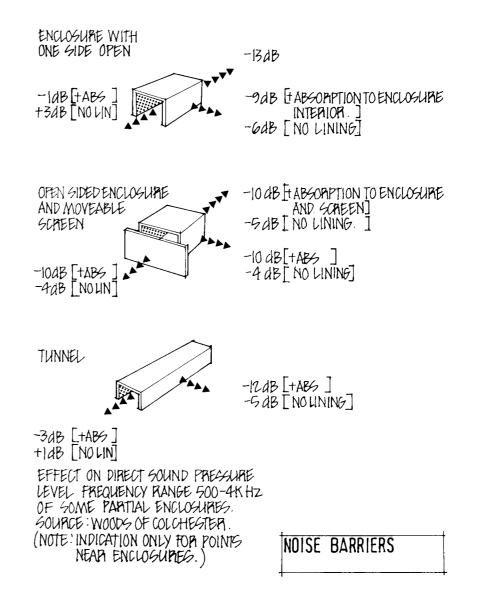




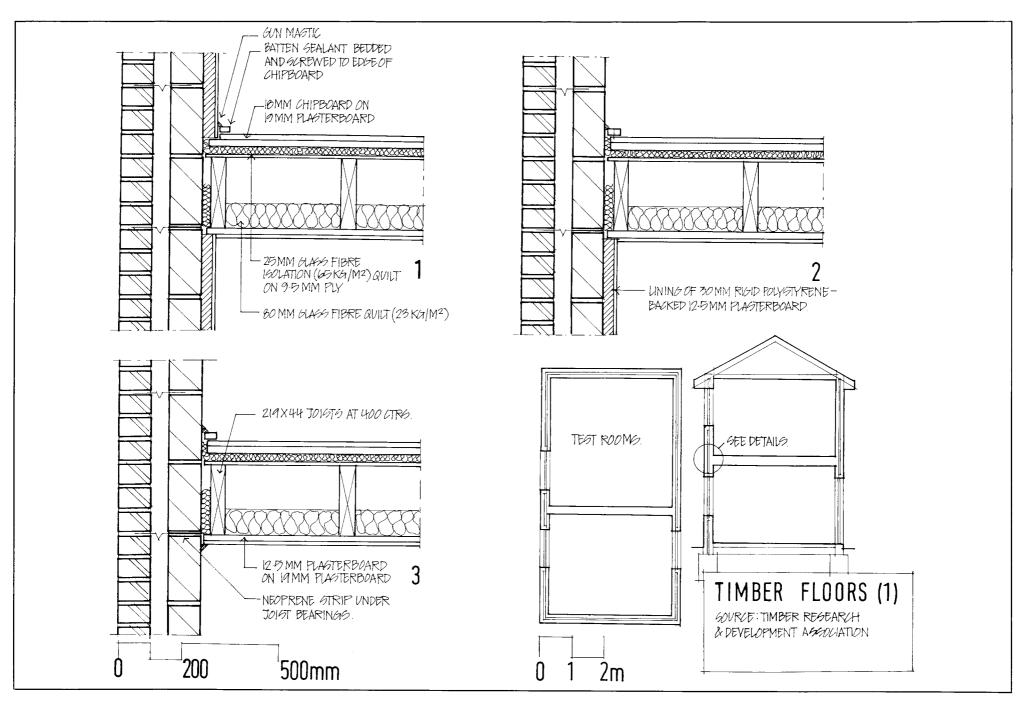
COMBINING GOUND LEVELS, FOR EXAMPLE IN PATH DIFFERENCE CALCULATIONS ABOVE. CAN BE CAPRIED OUT USING EITHER OF THE FIGURES AT LHS. FOR INGTANCE, A TELEPHONE BELL 3M. AWAY AT 73 dB ADDS TO THE BACKGROUND TO AB. IN A TYPISTS POOL TO GIVE A RESULTANT SOUND OF 74.75 dB (10.75)

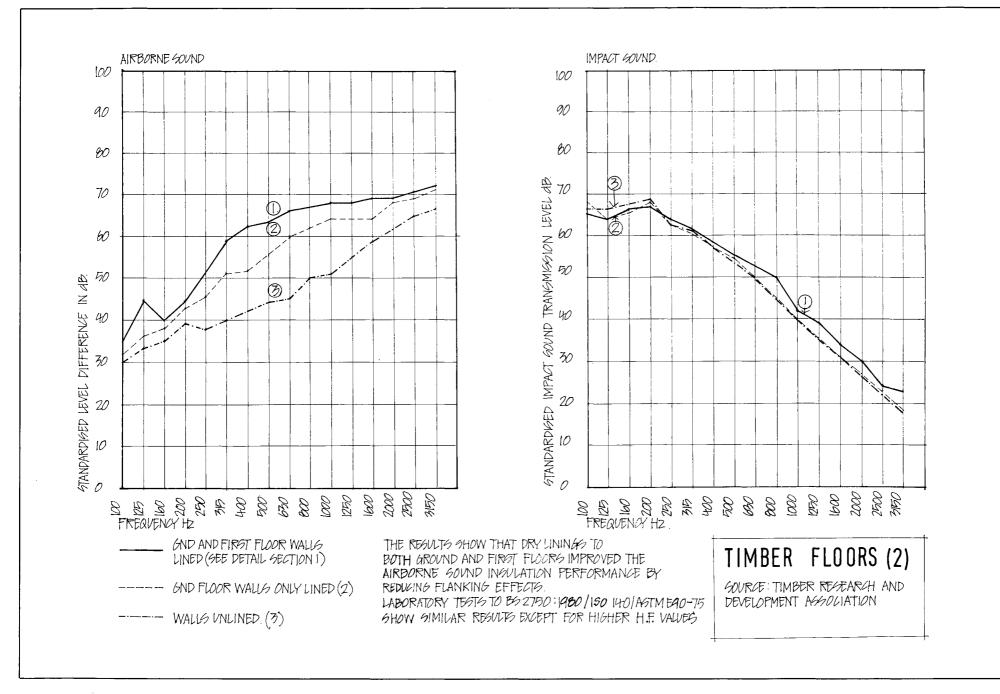
BARRIERS AND SCREENS

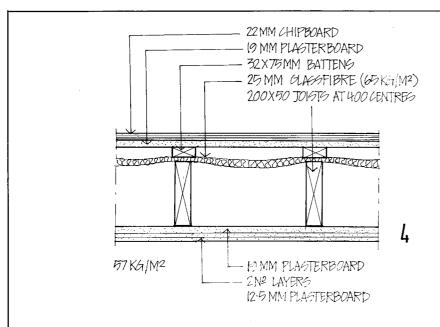


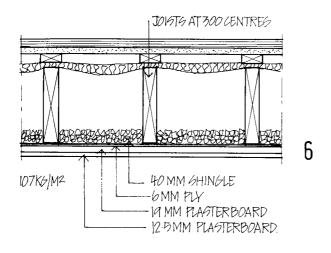


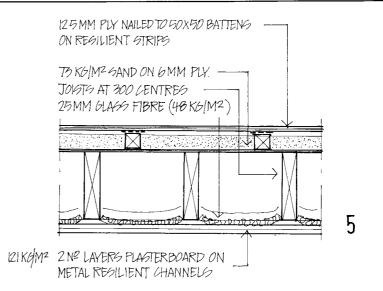
FL00RS











GOOD TIMBER FLOORS SHOULD INCLUDE AS FEATURES:

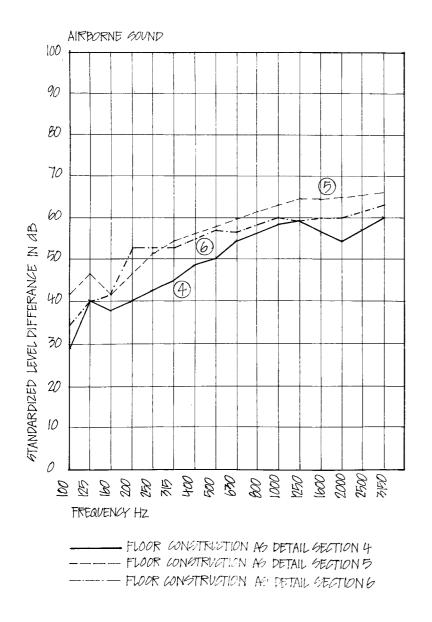
- -GUBGTANTIAL GOLATED FLOOR DECK
- -STIFF GUPPORT FRAME OF JOIGTS
- -ABGORPTIVE QUILT IN FLOOR CAVITY
- -GUBSTANTIAL CEILING

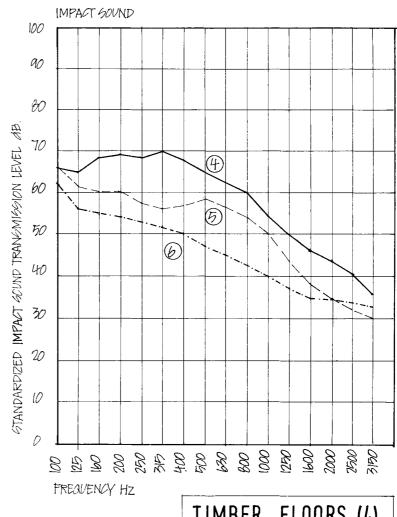
CONSTRUCTION SHOULD NOT BE OVER INTRICATE AND UNREALISTIC IN WORKMANSHIP REQUIRED.

PUBLING (6) IS FAVOURED IN SCOTTISH CONSTRUCTION ELECTRICAL CONDUITS CAN BE RUN IN THE SAND (5)

TIMBER FLOORS (3)

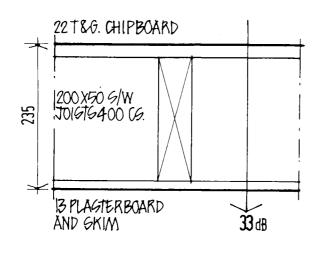
GOURCE: TIMBER RESEARCH AND DEVELOPMENT ASSOCIATION

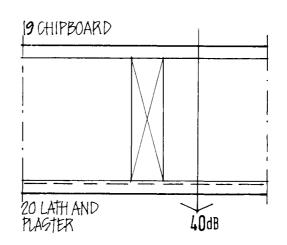


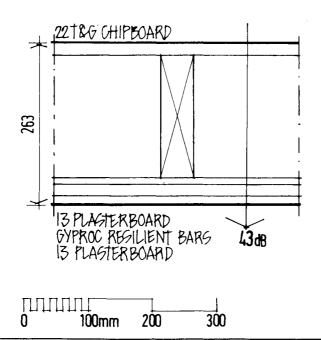


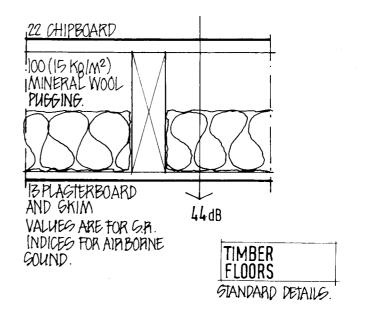
TIMBER FLOORS (4)

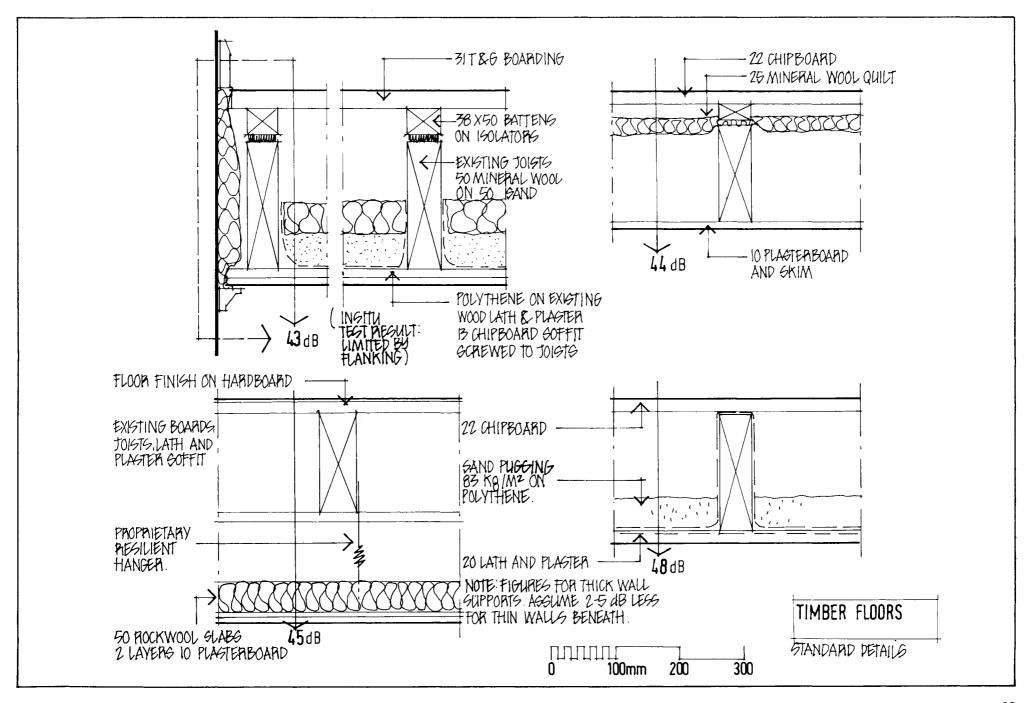
GOURCE: TIMBER REGEARCH AND DEVELOPMENT ASSOCIATION

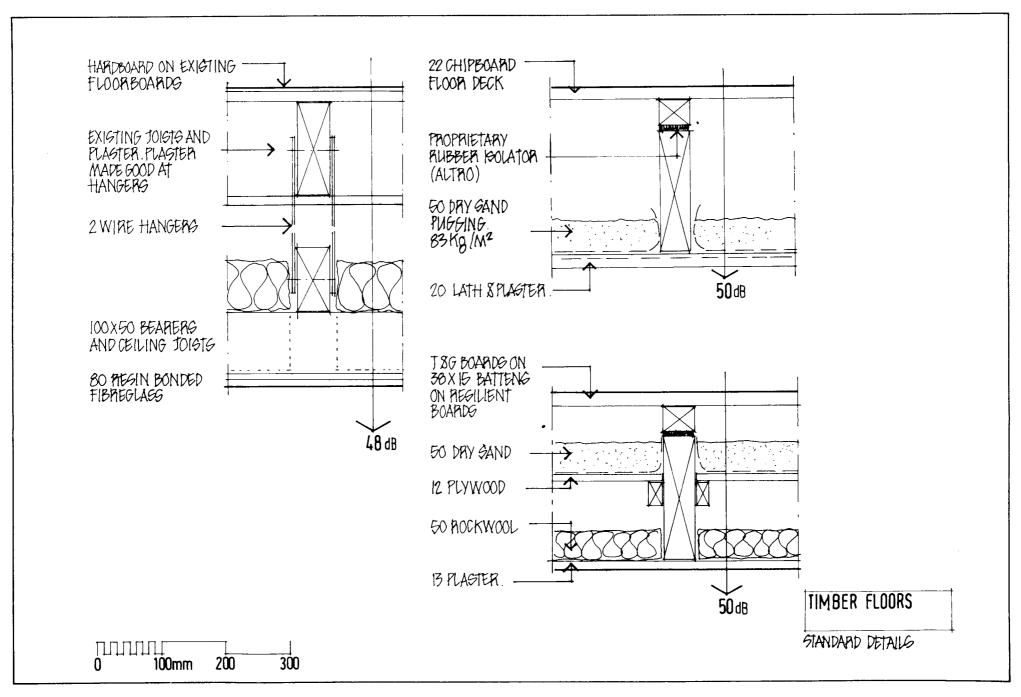


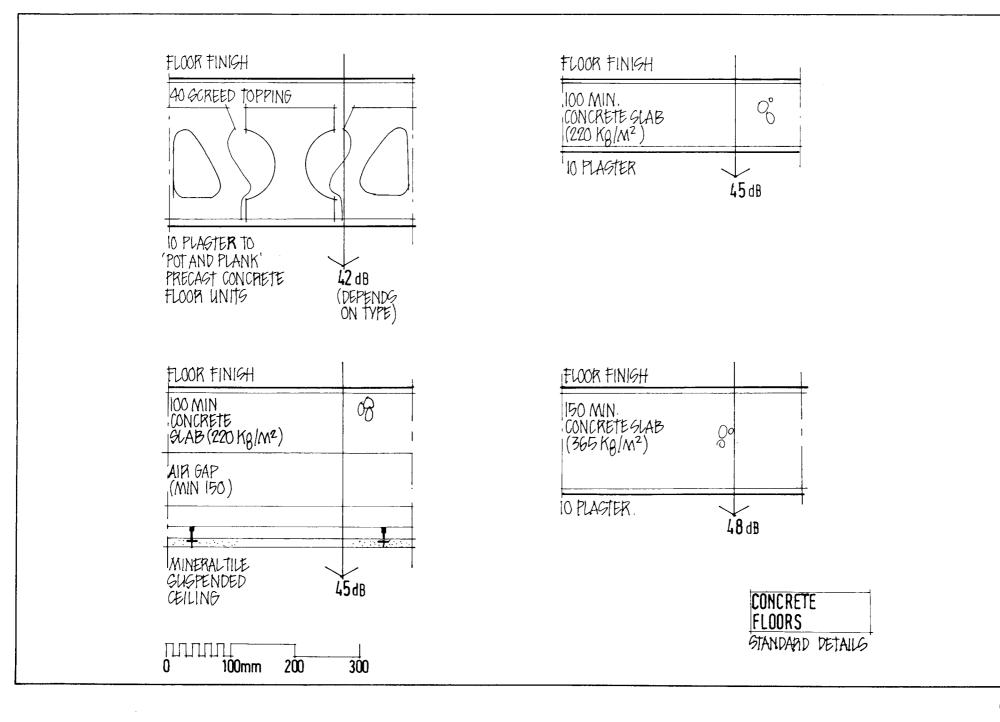


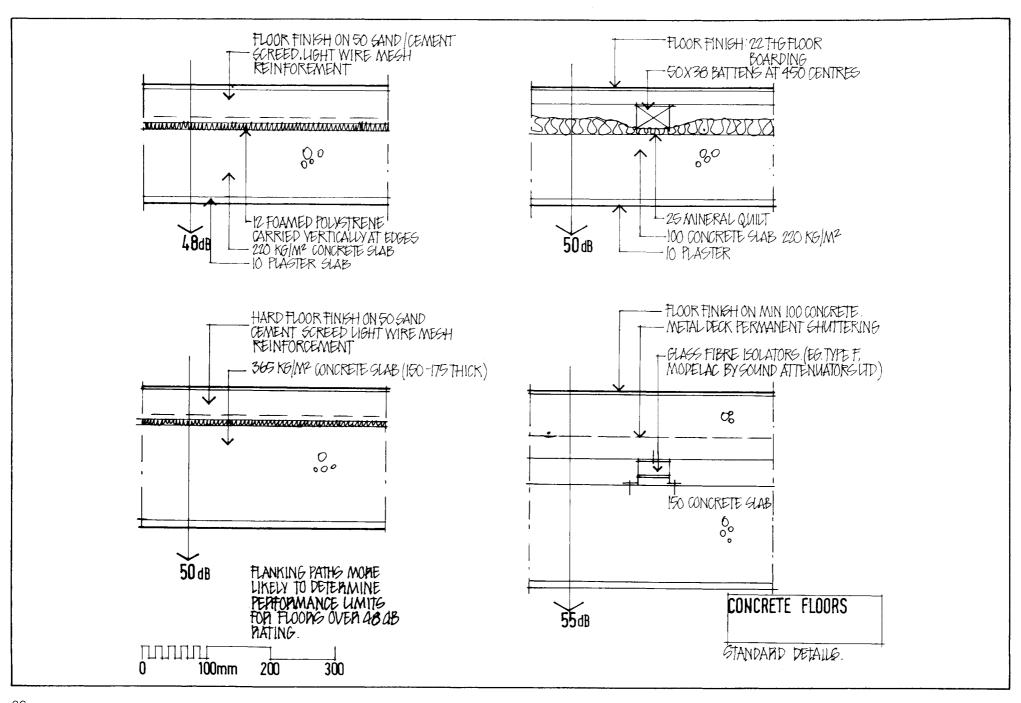




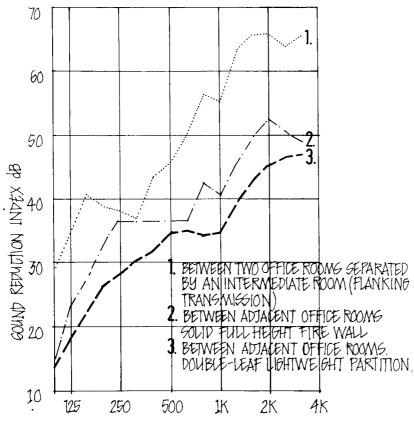




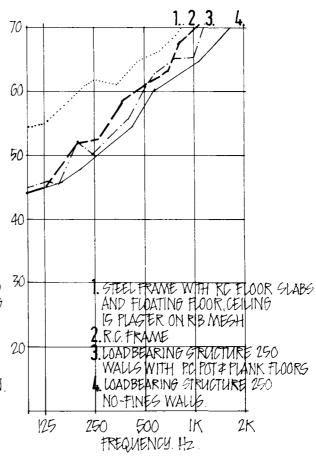




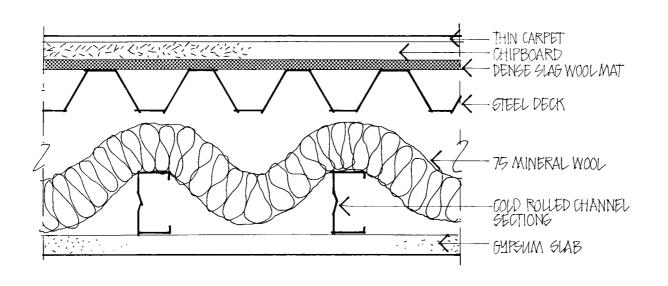
AIRBORNE SOUND INSULATION IN AN OFFICE BUILDING WITH A STEEL FRAME, LIGHT-WEIGHT SOLID FLOORS AND DOUBLE-LEAF WALLS. GUSPENDED CEILINGS AIRBORNE SOUND INSULATION BETWEEN 2 ROOMS SEPARATED BY AN INTERMEDIATE FLOOR

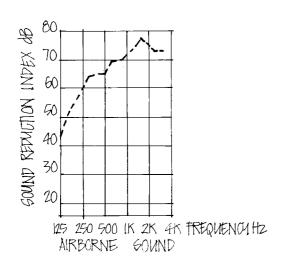


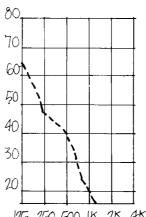
IMPROVEMENT IS ACHIEVED AT ALL FREQUENCIES IN SPITE OF FLANKING TRANSMISSION, BY INCREASING SOLIDITY OF SUBDIVISION AND SEPARATING NOISY AND NOISE-SENSITIVE ROOMS.



STRUCTURE SOURCE: DR. LANG. TECHNOLOGISCHE GEWERBE MUSEUM. YIENNA



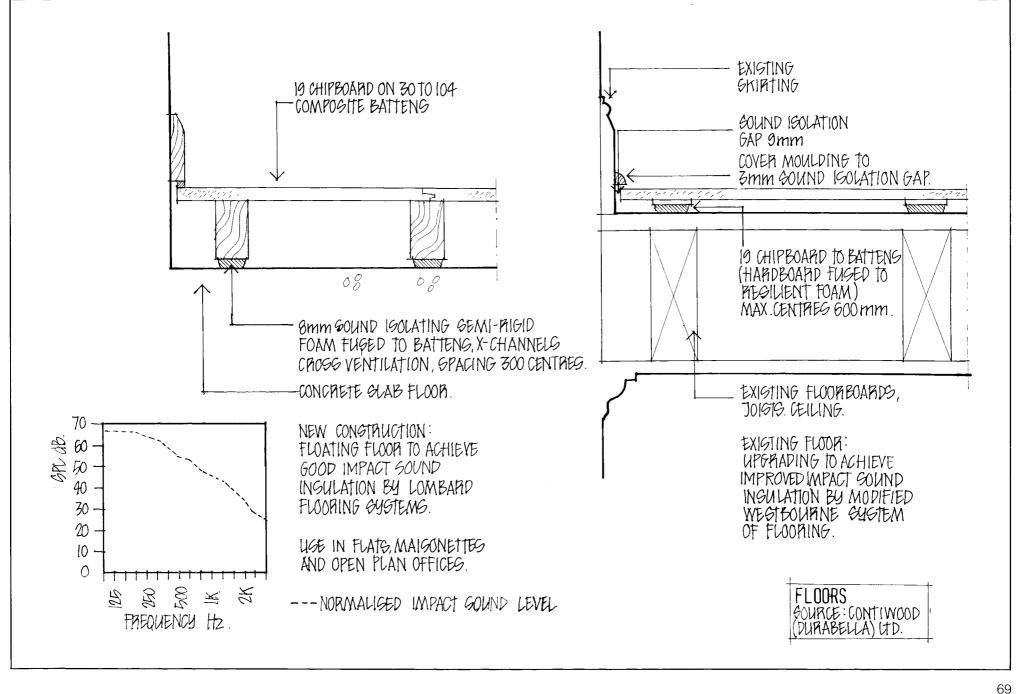


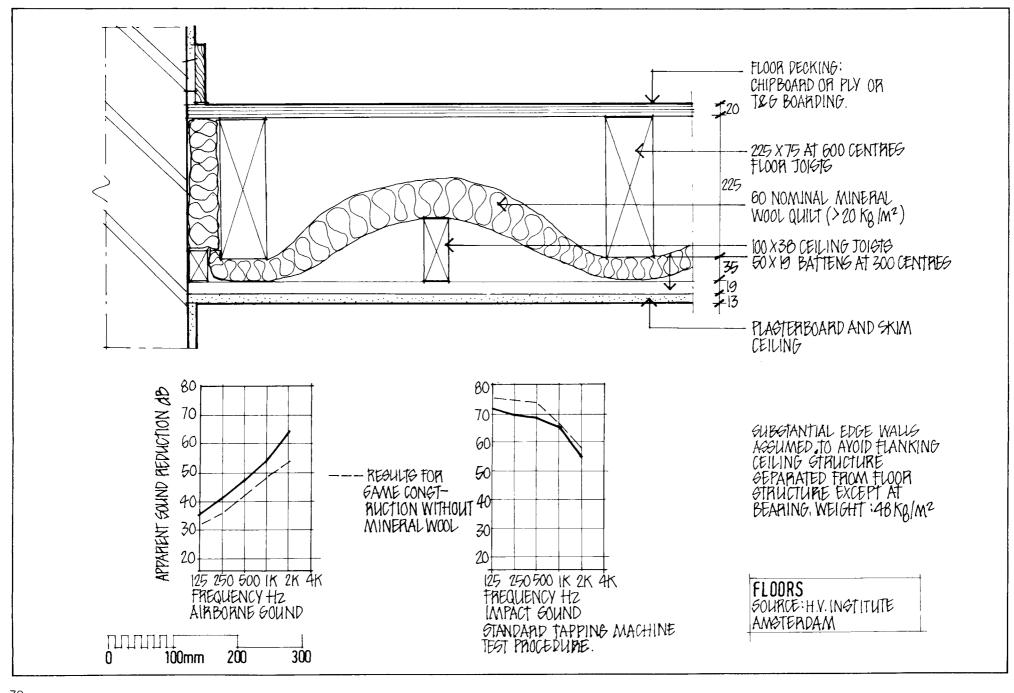


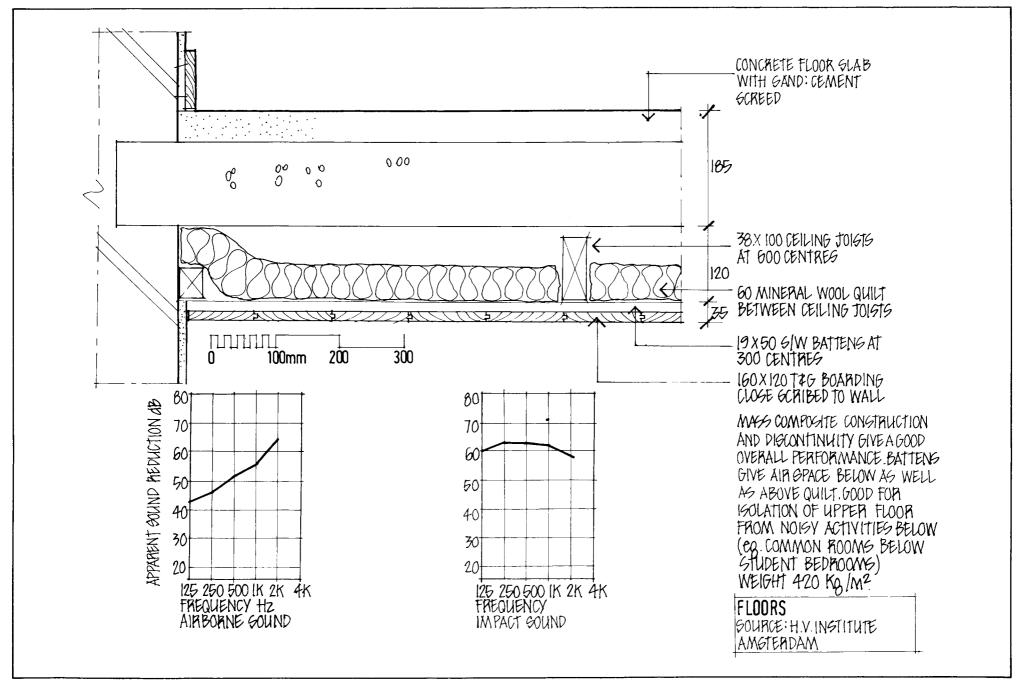
THE PROPERTY OF ELEMENTS
OF STRUCTURE TO PREVENT
NOISE TRANSMISSION DIFFERS
GREATLY FOR WHETHER
AIRBORNE OR IMPACT SOUND
IS THE NOISE SOURCE NOTE
THESE RESULTS WOULD ONLY BE
BE OBTAINED WITH NEGLIGIBLE
FLANKING.

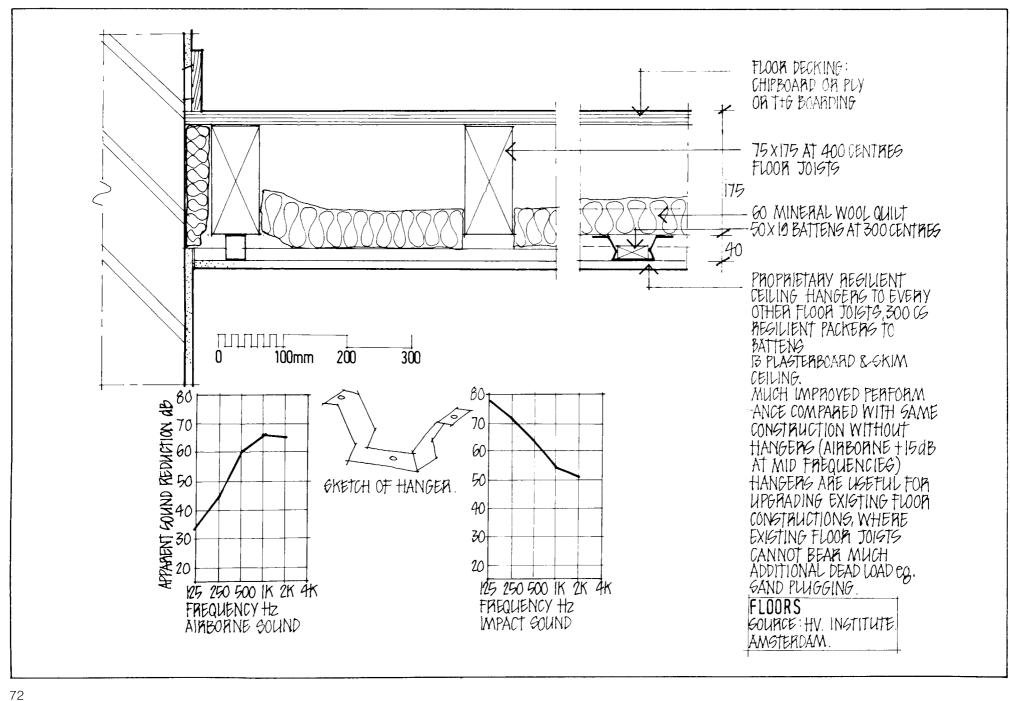
125 250 500 IK 2K 4K FREQUENCY HZ IMPACT SOUND

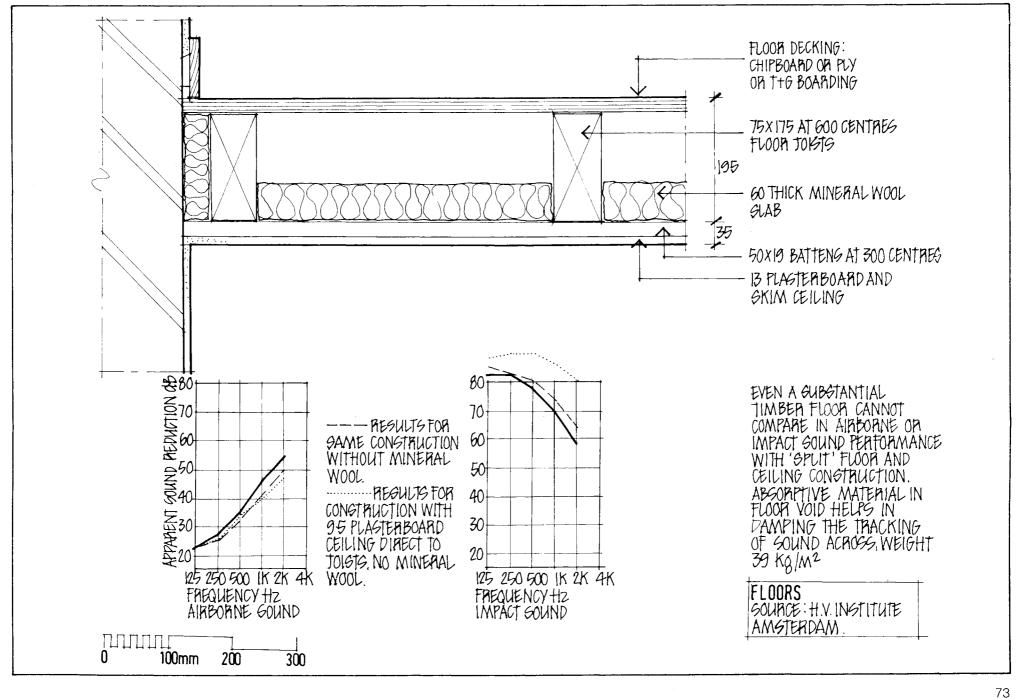
FLOORS
SOURCE: DR. LANG
TECHNOLOGISCHEG
GEWERBE MUGEUM: VIENNA

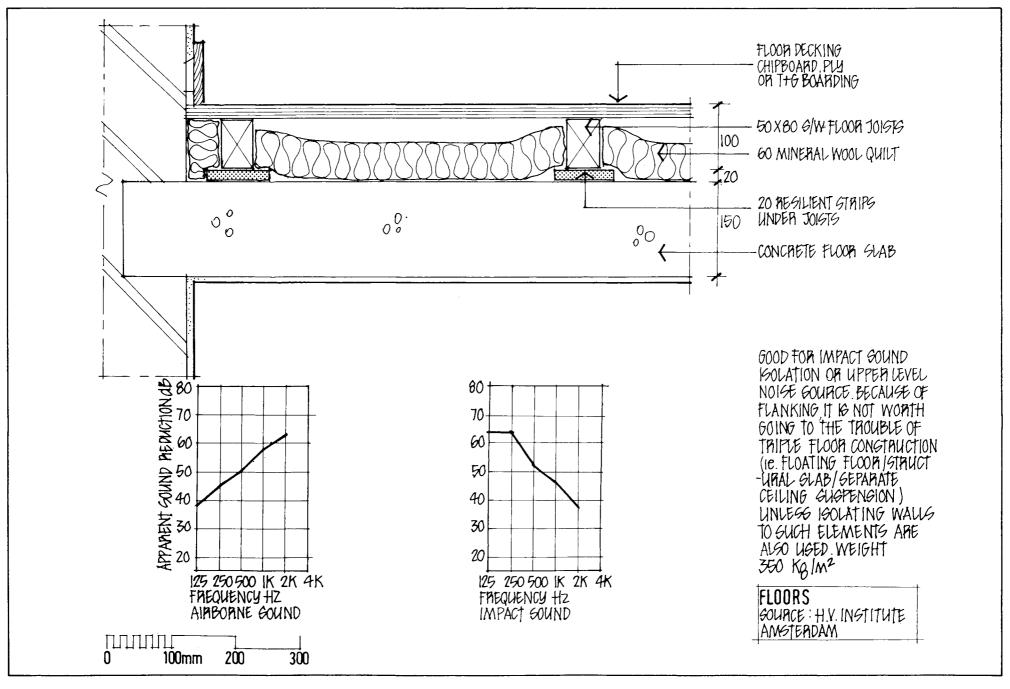


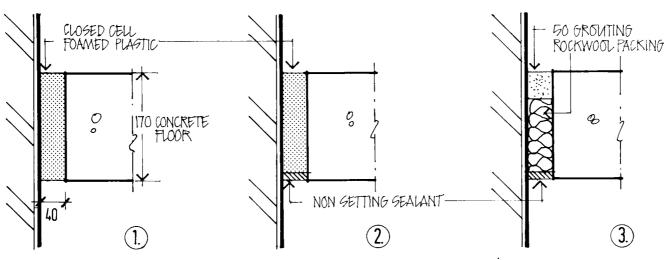








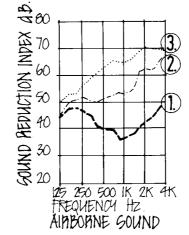




VERTICAL SECTIONS

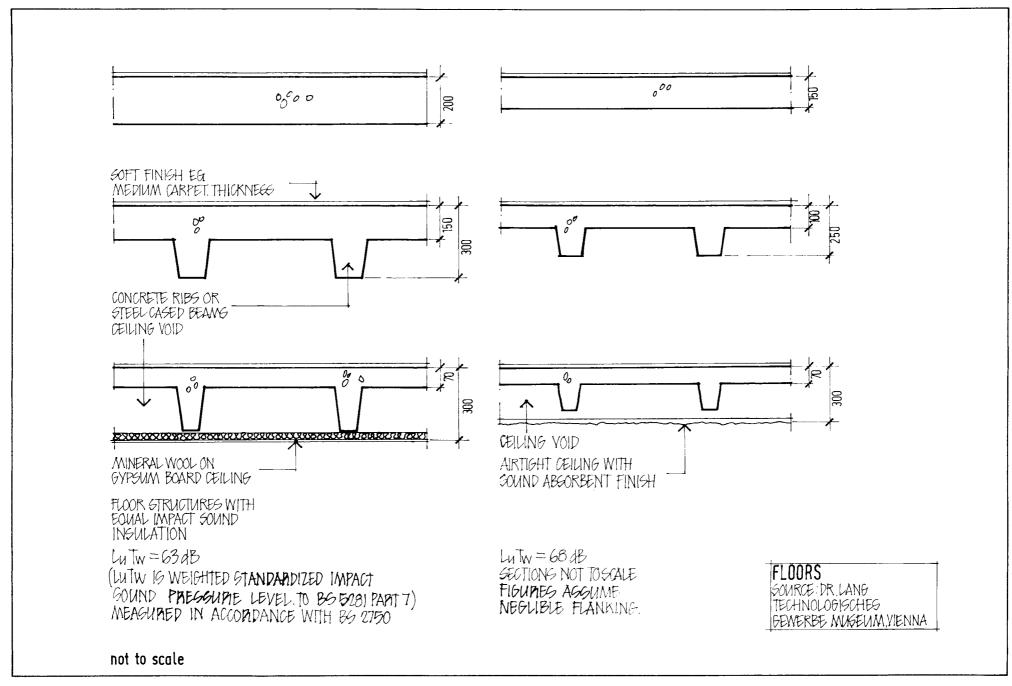
SOUND LEVEL DIFFERENCE BETWEEN TWO ROOMS CAUGED BY A 2 METRE SLOT IN ONE SIDE OF A FLOOR (LABORATORY TEST). GOOD GEALING OF GAPS NECESSARY FOR SPEECH FREQUENCY PRIVACY, GEALING LEGS CRITICAL AT LOW FREQUENCIES.

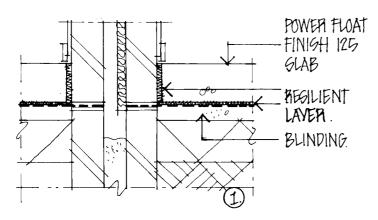
A SMALL STOREY-HEIGHT CRACK O-ZMM WIDE IN A WALL IOM? IN AREA WOULD RESULT IN A 7 dB LOSS IN A SO dB-RATED WALL, BUT I dB ONLY REDUCTION OF INSULATION IN A 35 dB. PARTITION: LACK OF CRACKS OR GAPS IS PARTICULARLY IMPORTANT FOR SUBSTANTIAL SEPARATING ELEMENTS.











2) Bo

(1) IS POOR COMPARED WITH (3): REGILIENT QUILT IS SUBJECT TO EXTRA COMPRESSION LOAD AND WATER FROM CONCRETE MIX. ABGORBENT MATERIAL IN CAYITY CUTS DOWN TRACKING OF NOISE ACROSS CAVITY.

(1)-(4) SHOW VARYING MEANS OF ISOLATING FLOOR SLABS IN ADJACENT ROOMS TO PREYENT FLANKING (CO. IN MUSIC ROOMS, CONTERENCE ROOMS)

4 IS IMPRACTICAL TO INSTALL

ELAGTOMERIC LAYER OVER DPC

PROPRIETARY BUILT-UP FLOOR:
19 OR 22 CHIPBOARD ON
EXPANDED POLYGTYRENETO
FLOOR GLAB

LONG FIBRE GLAGG WOOL AND MINERAL WOOL QUILTS HAVE BEEN GUGGEGTED AS THE MOST PROVEN MATERIALS (BRE 103). FIBREBOARD AND HAIR FELT HAVE GHOWN UNGATISTACTORY COMPACTION UNDER CONTINUOUS LOAD. MATERIAL TO BE USED TO HAVE FOLLOWING FEATURES:

A-DENGITY 15-25 Ka/M2 MIN

B.- THICKNESS NOT LESS THAN 13mm

C.— BOAND PRECOMPRESSED TO HALF INITIAL THICKNESS
WITH RAPID RECOVERY TO 9% INITIAL THICKNESS.
THIN MATERIALS ARE PROMISING IN PERFORMANCE:
REDUC HAVE A MEMBRANE ONLY 1:5MM THICK. OTHER
INSULATION PANELS OF TRY PANELS CONSIST OF
CHIPBOARD, HARDBOARD OR PLY EITHER SIDE OF A
THIN VISCO ELASTIC LAYER WHICH HAS THE PROPERTY
OF A HIGH DEGREE OF INTERNAL DAMPING.

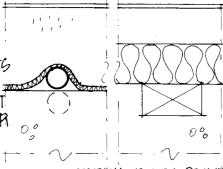
WORMALISED IMPACT

SOUND TRANSMISED ON LATA

OF 125 250 500 IK 2K

UNDAMPED CONCRETE

CONCRETE DAMPED WITH
REDUC MAT



CONDUIT OR PIPE POCKETS

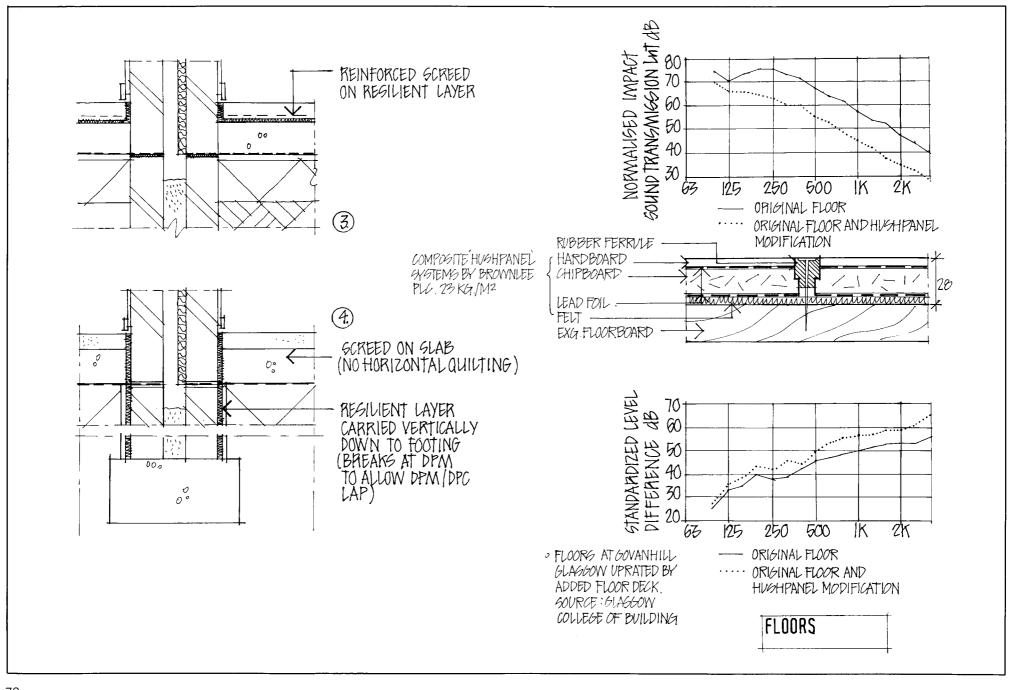
GET UNDER UNDER EXPA
GCREED (NOT NOED POLY

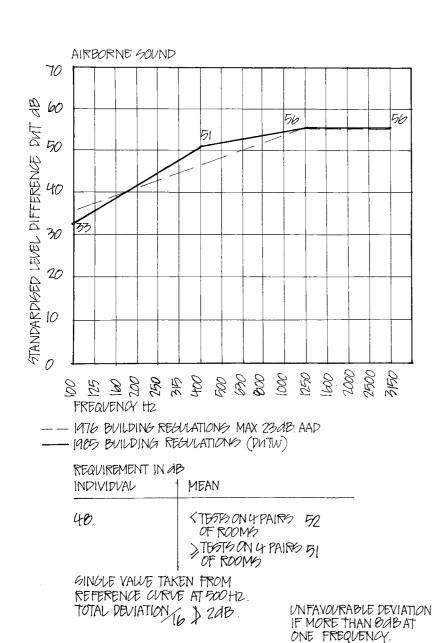
TO EXCEED 25 GTYRENE NOT

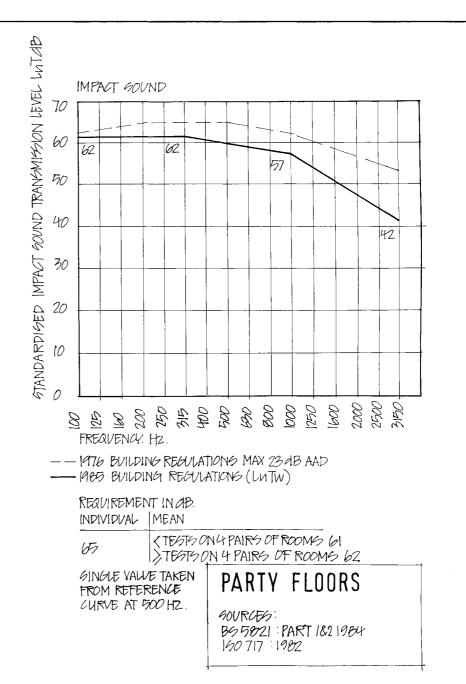
IN 50 GCREED) EXCEEDING 75

WIDTH

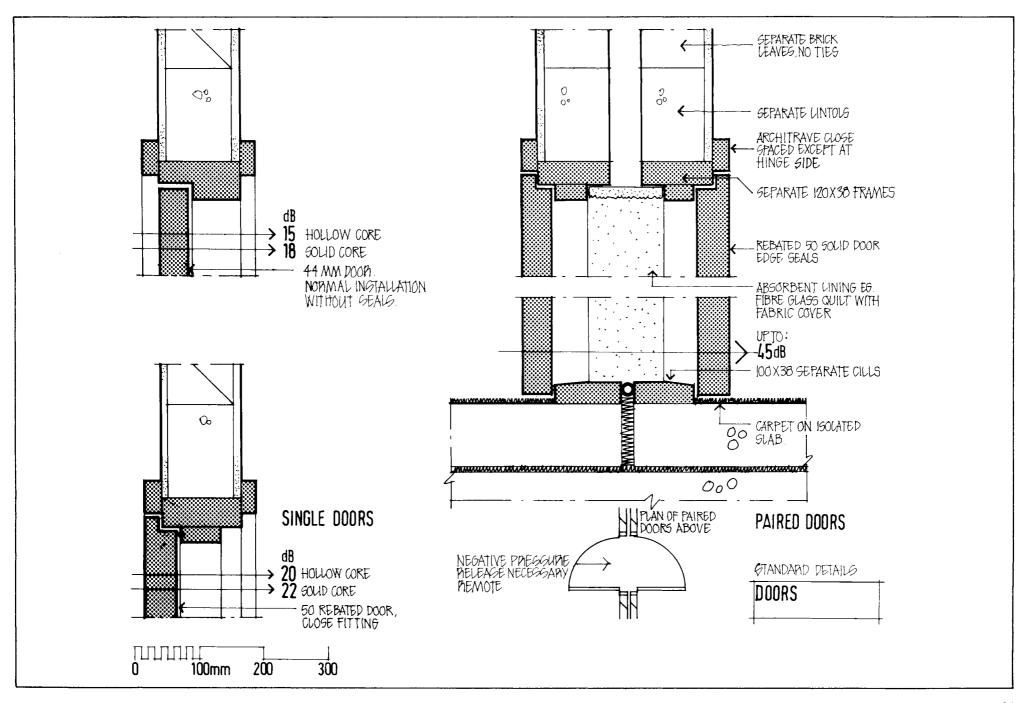
FLÖORS

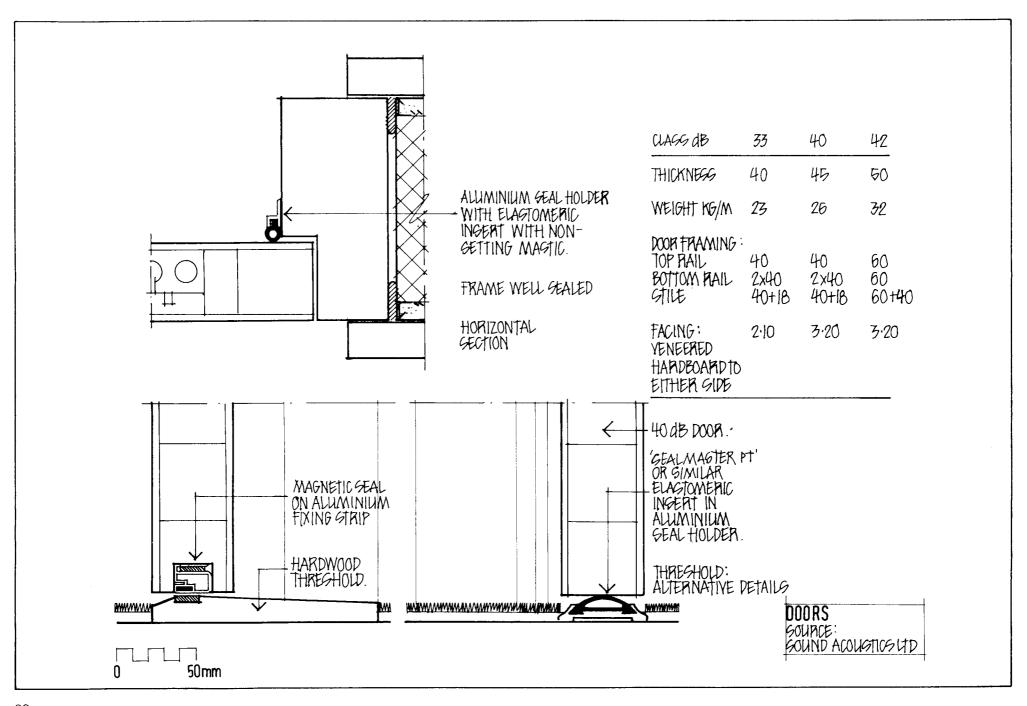


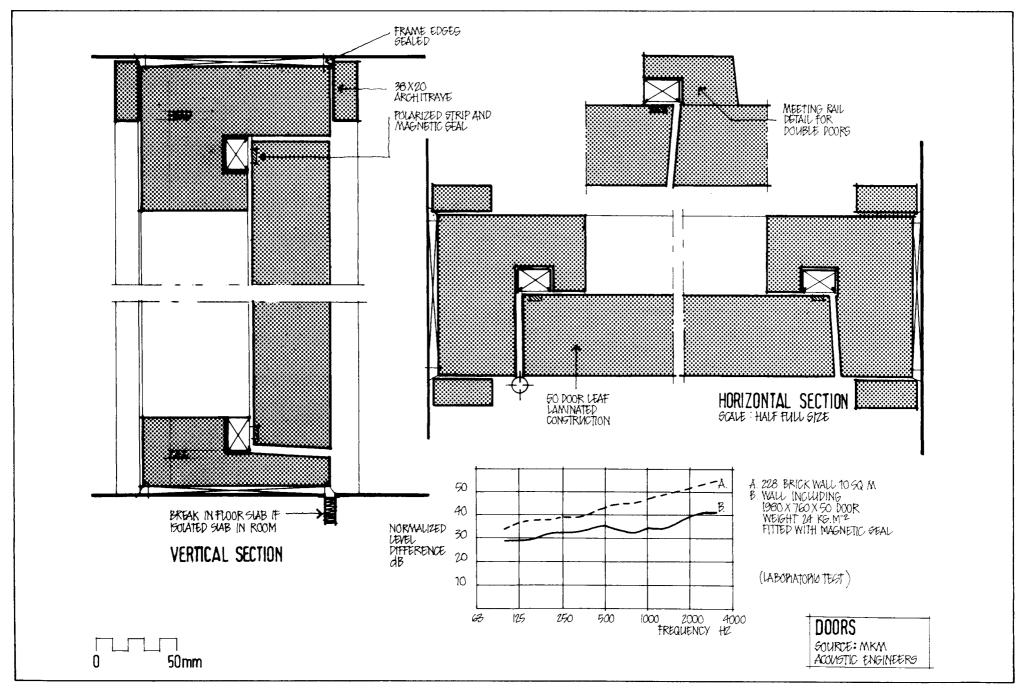


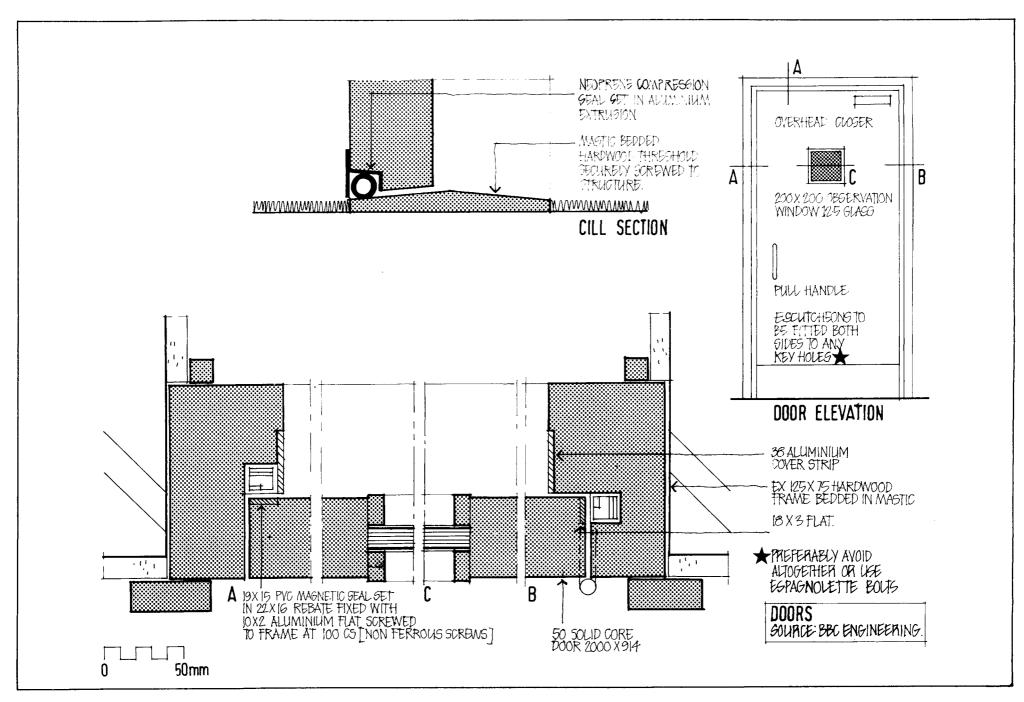


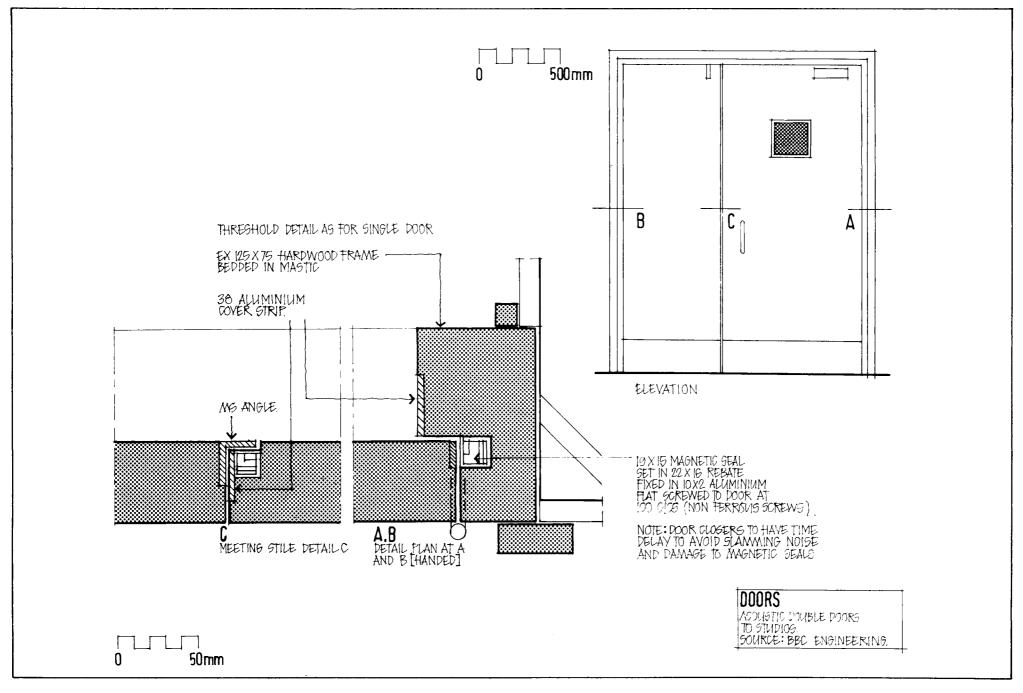
D00RS

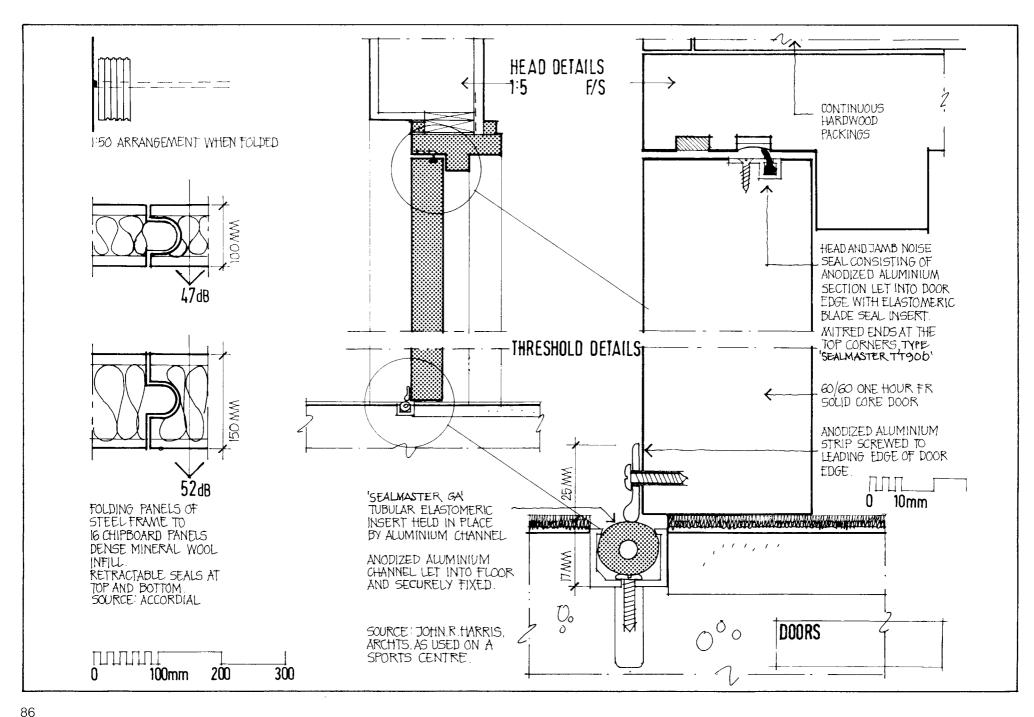


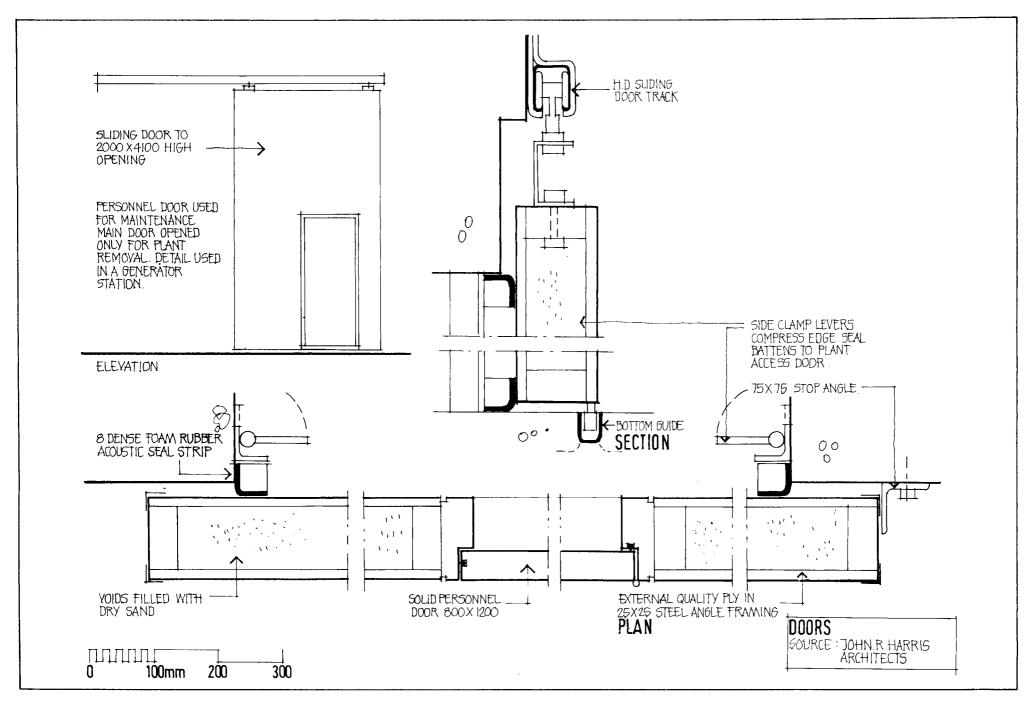


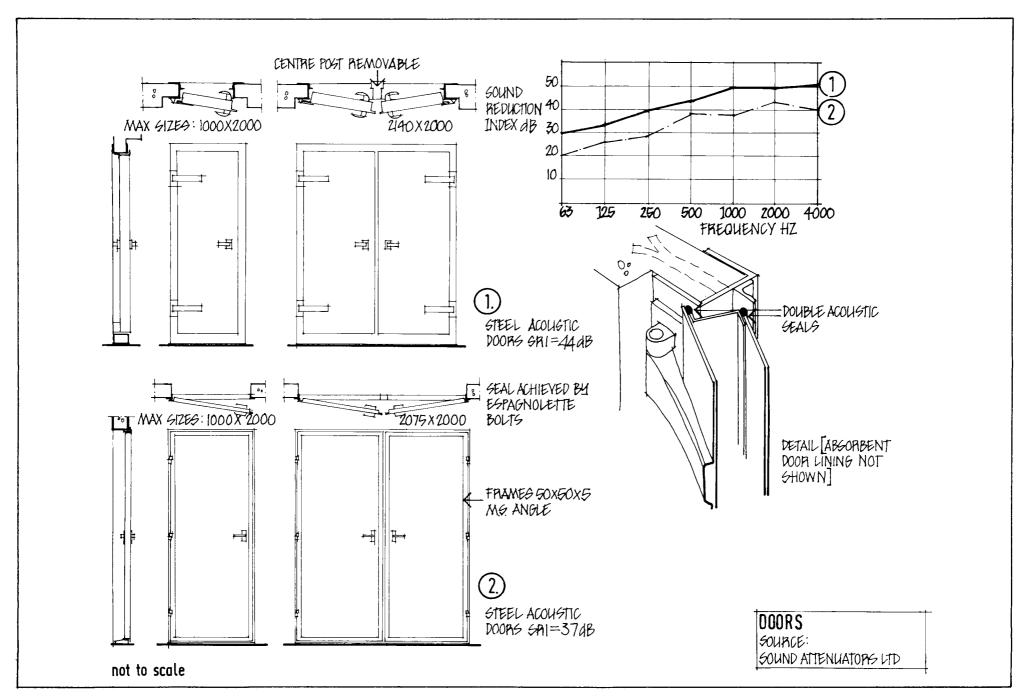


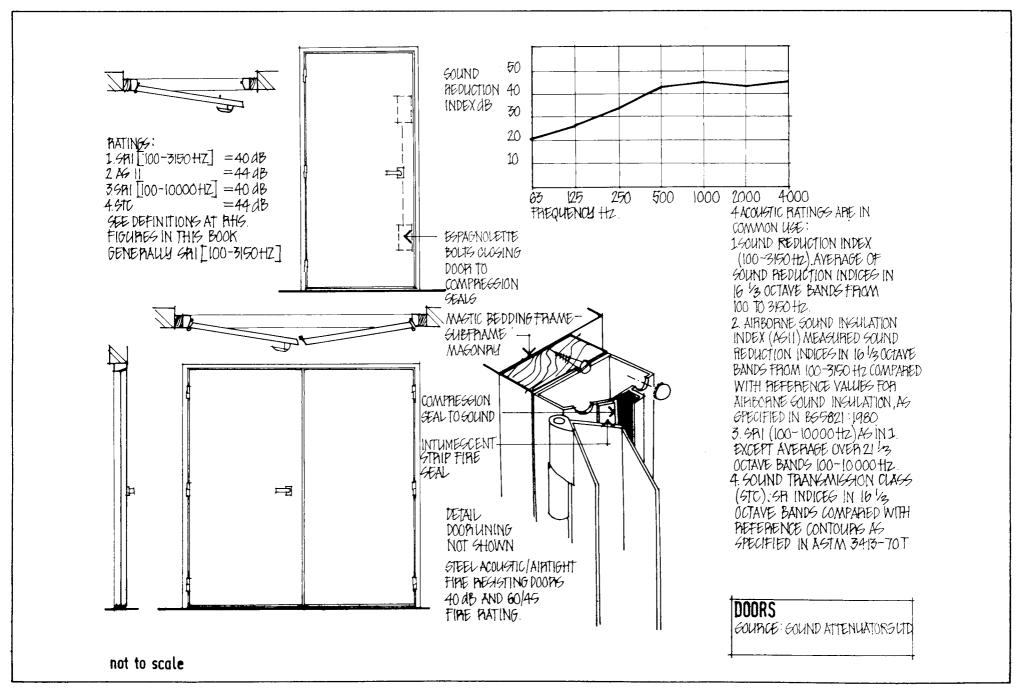


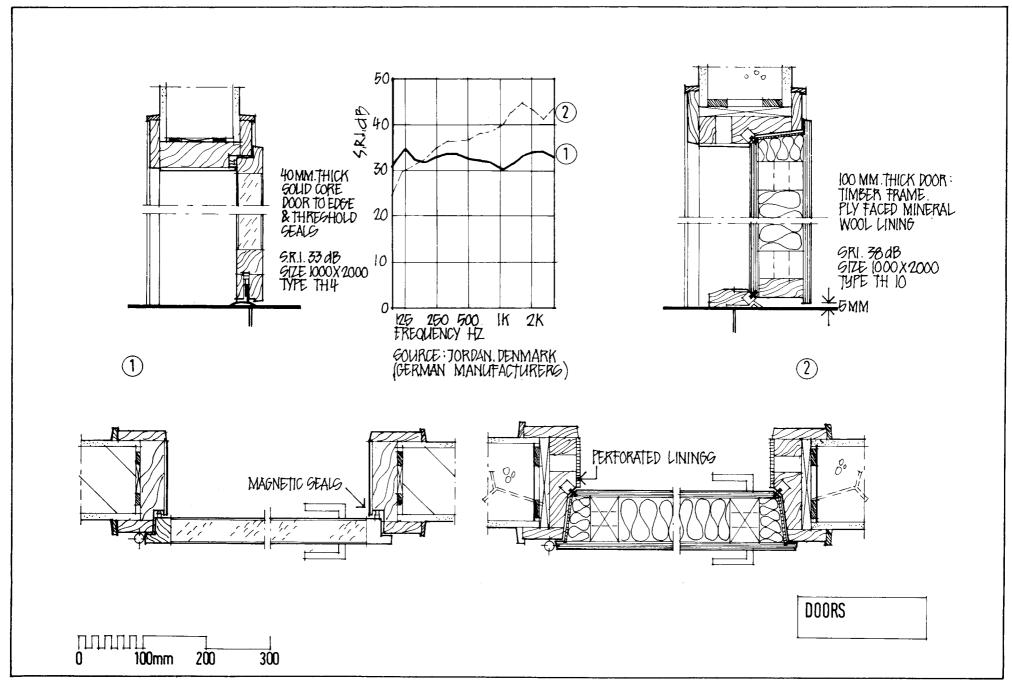


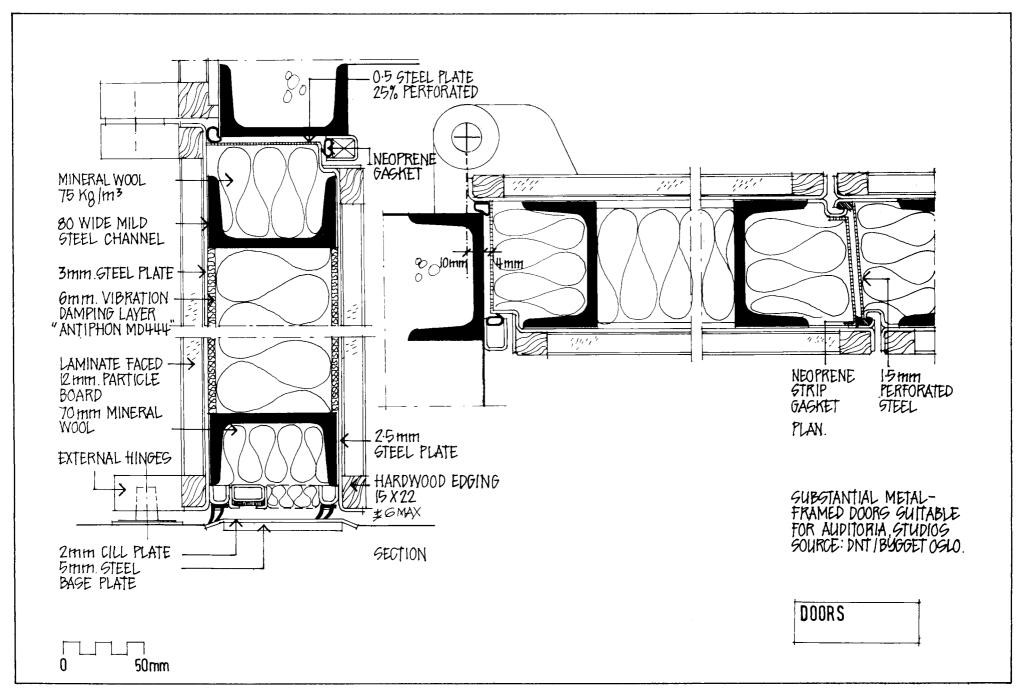


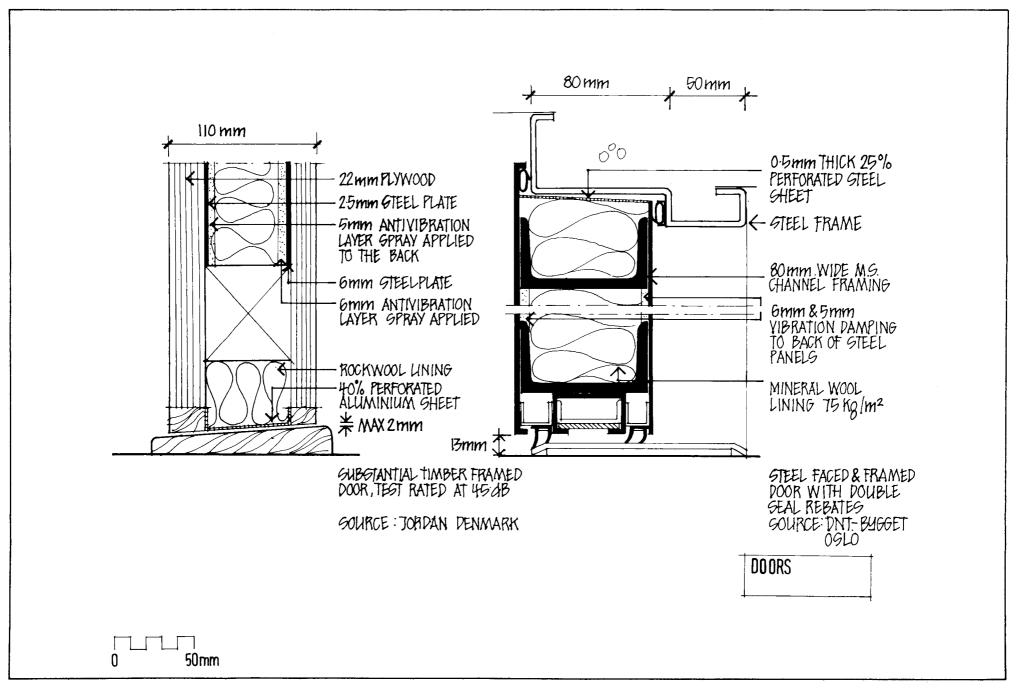


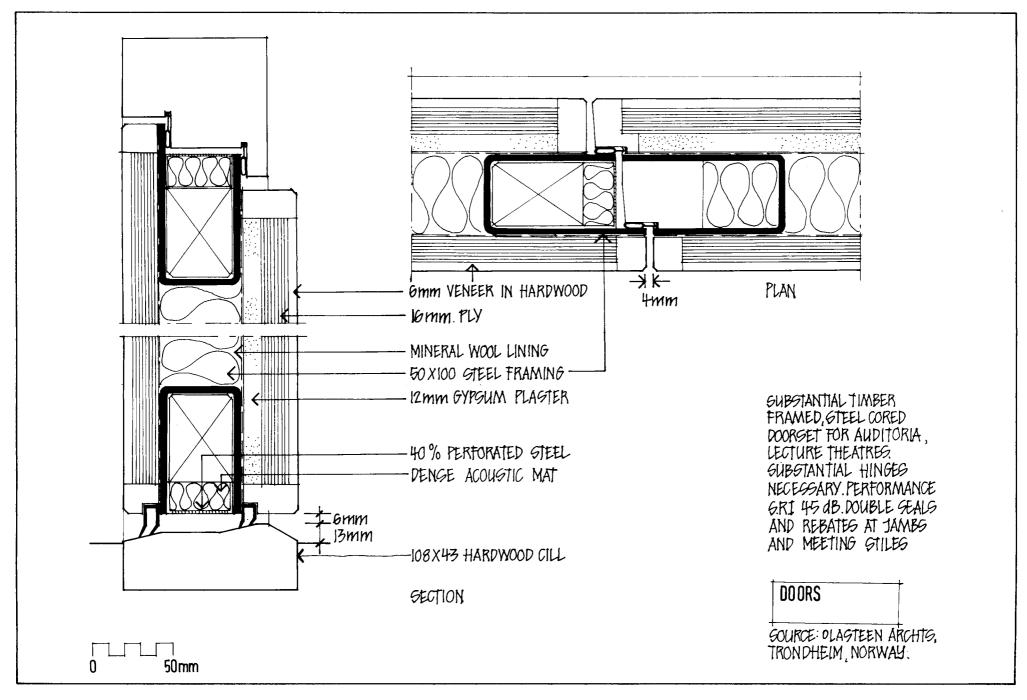


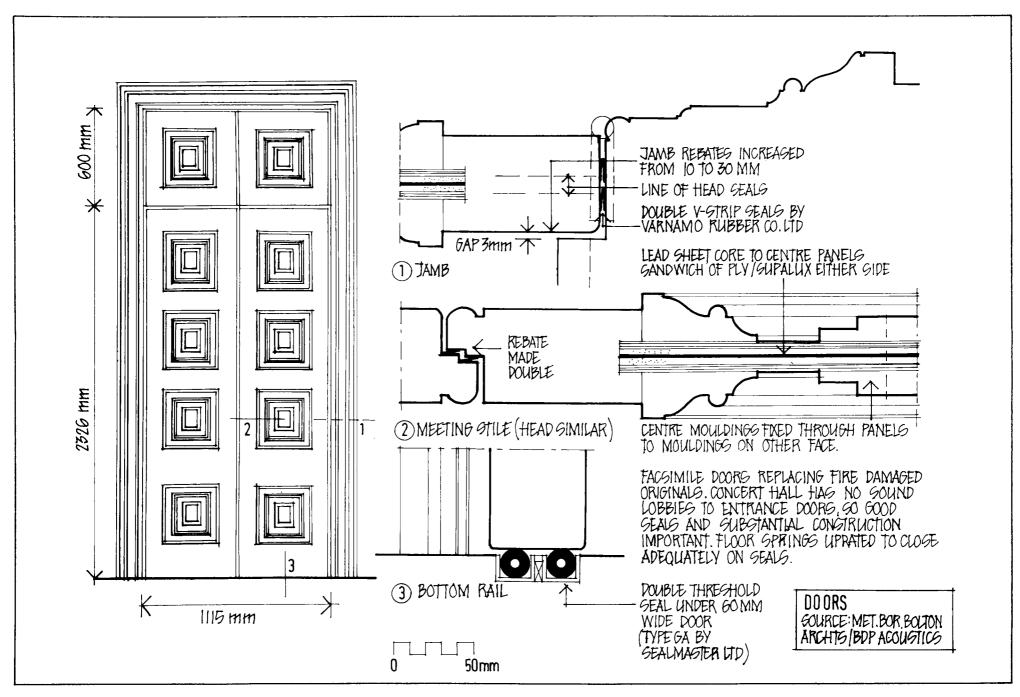


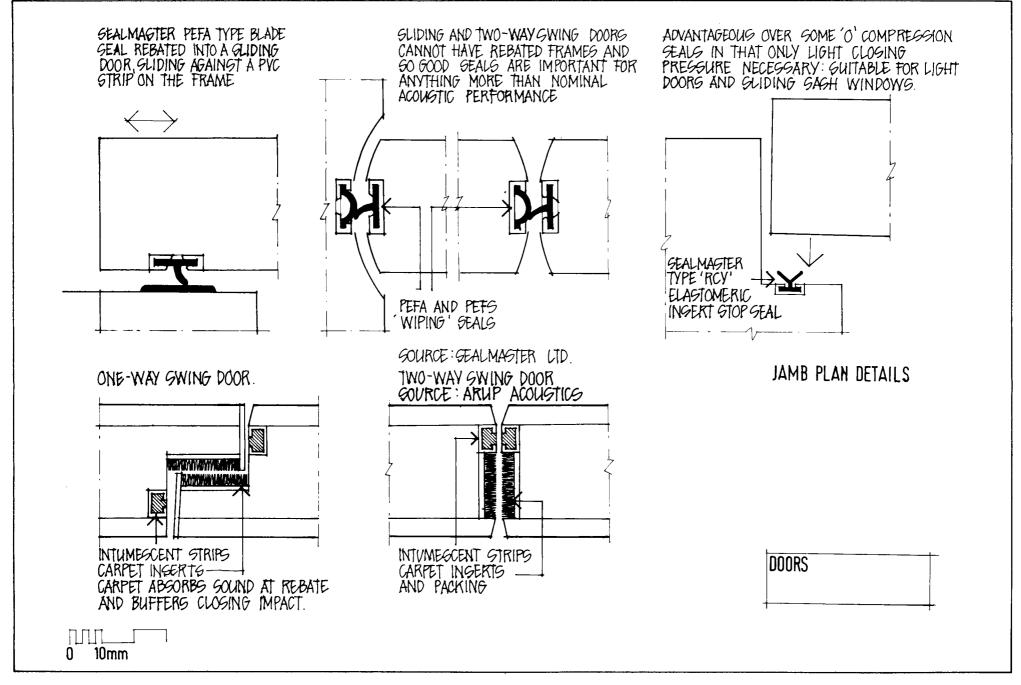


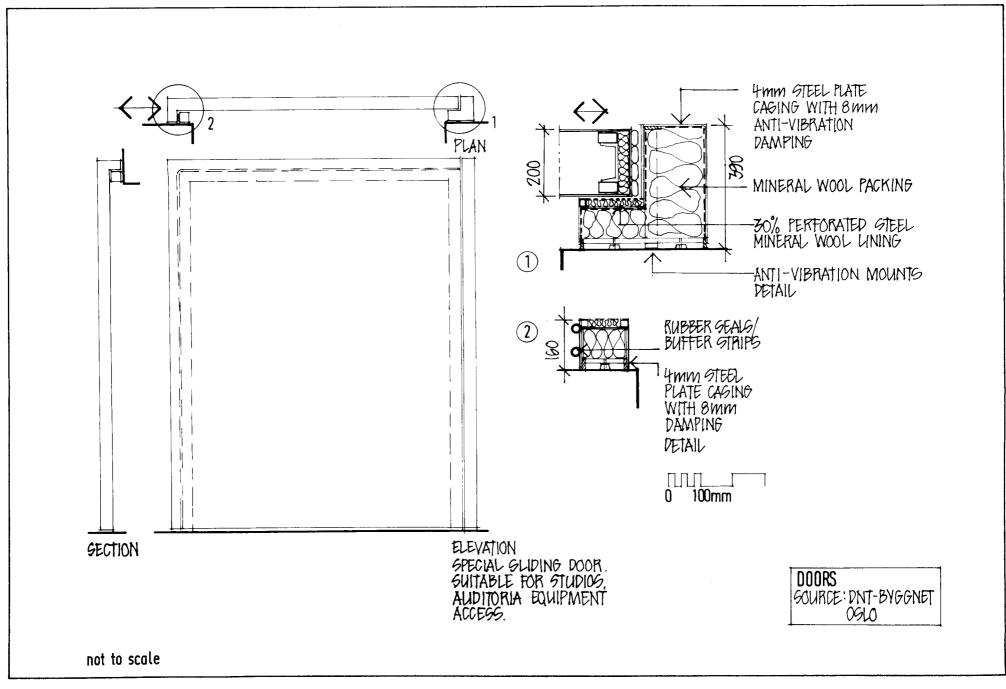


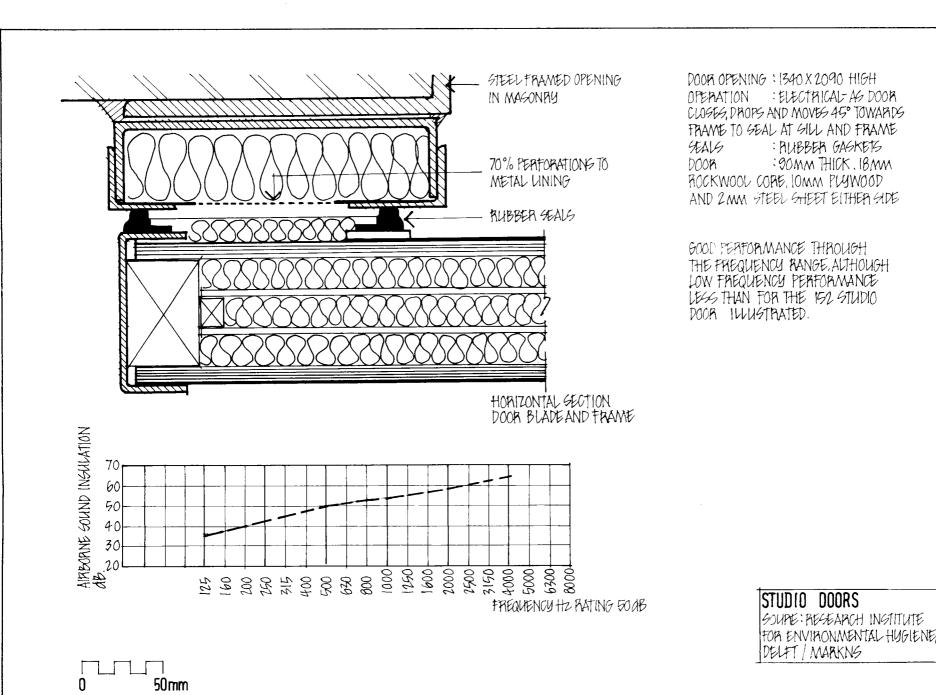


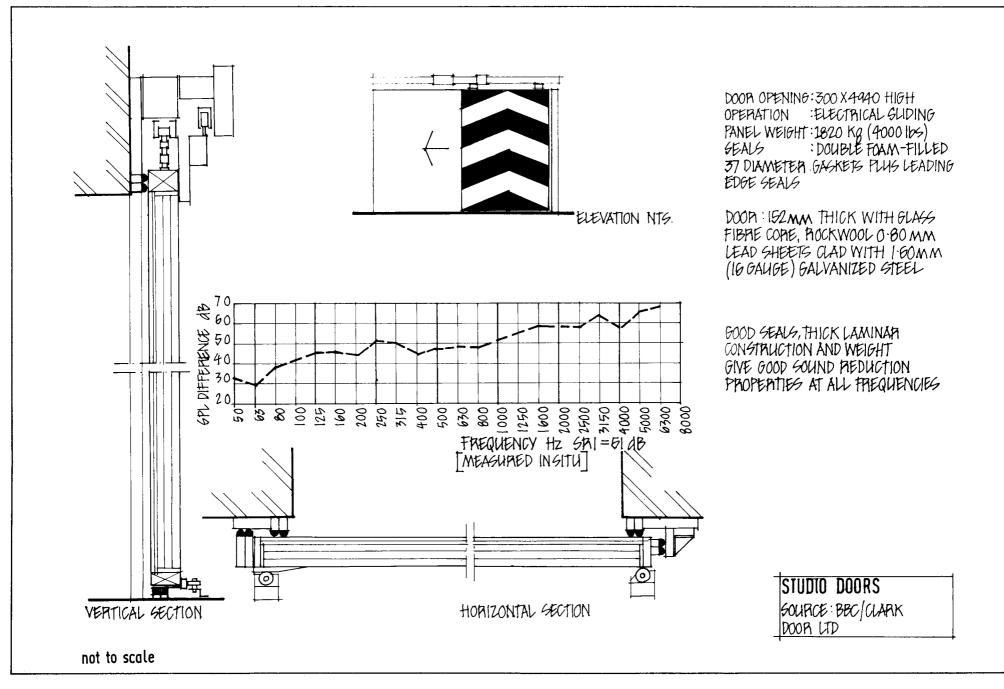




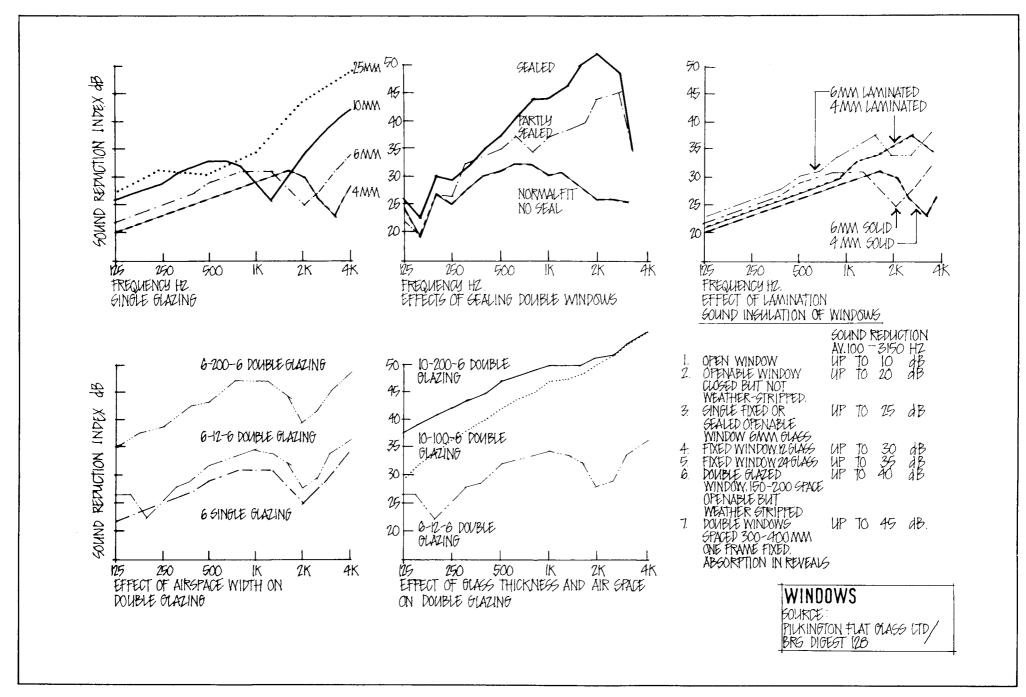


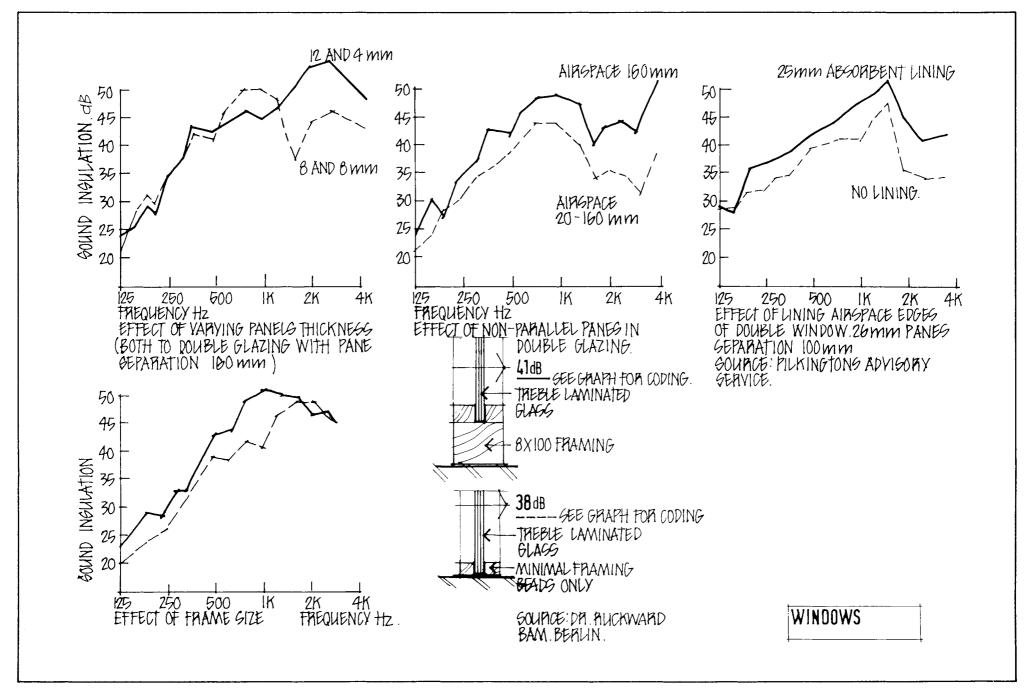


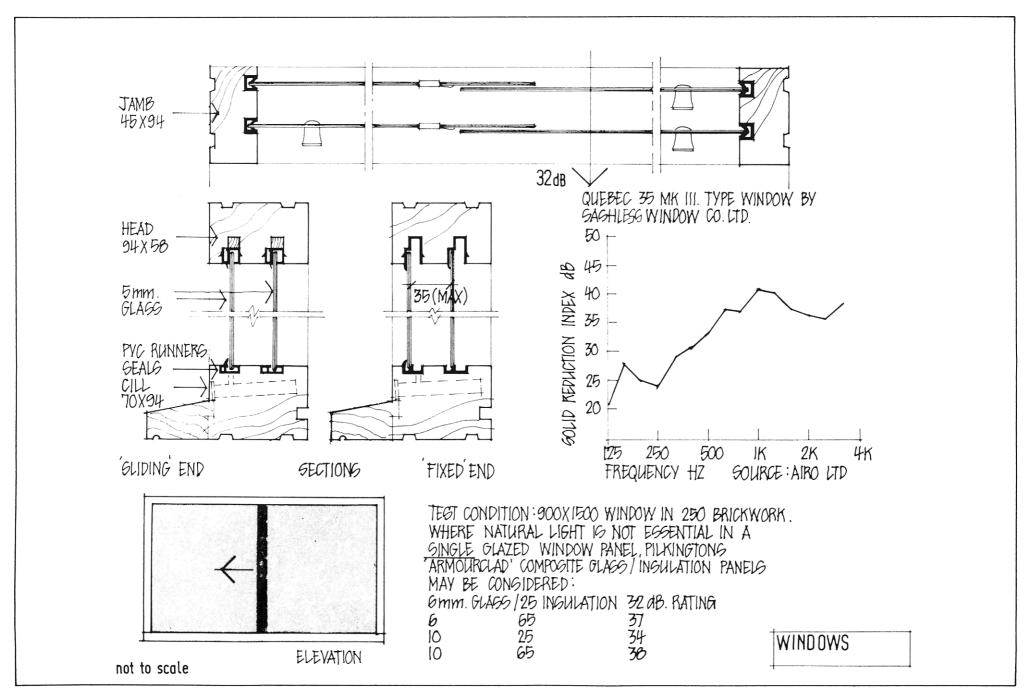


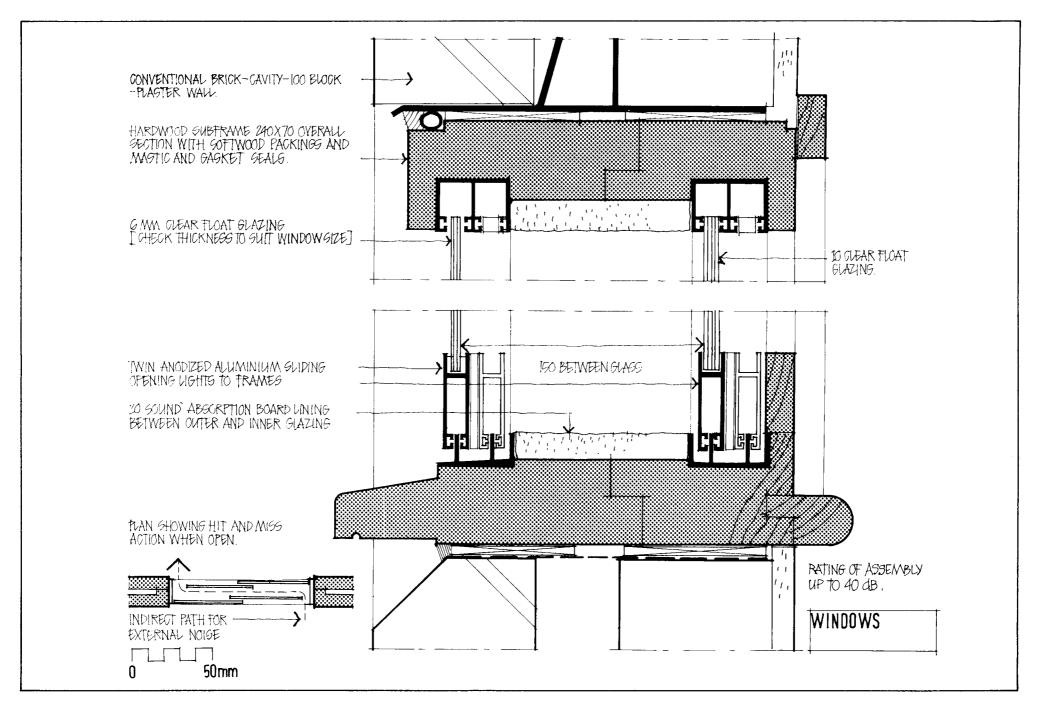


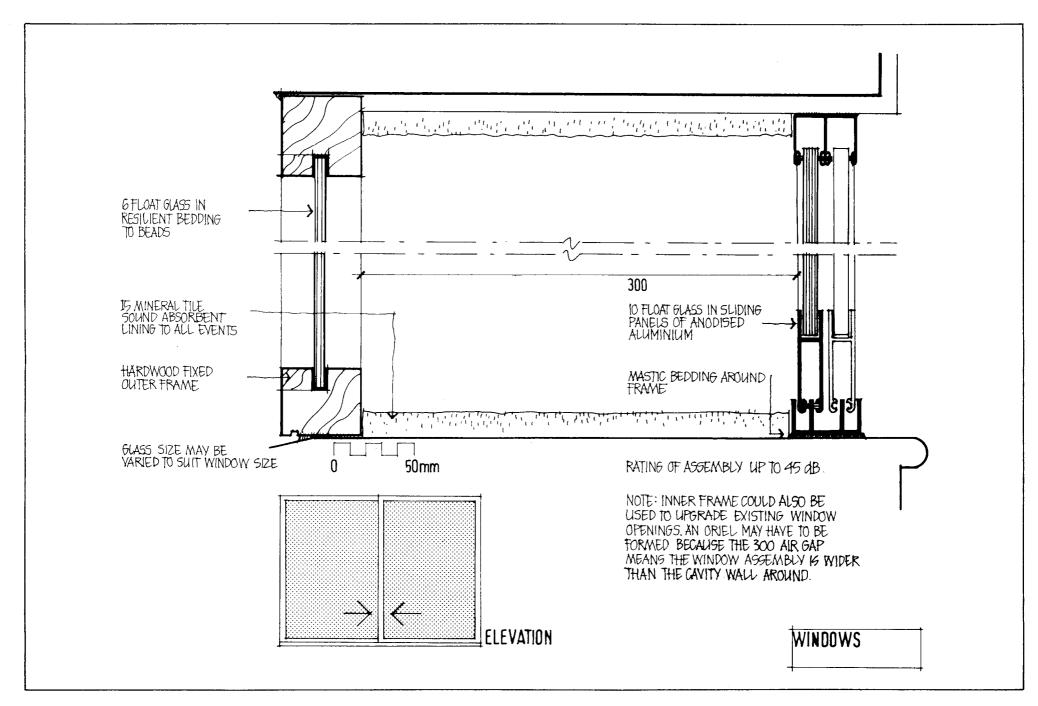
WINDOWS

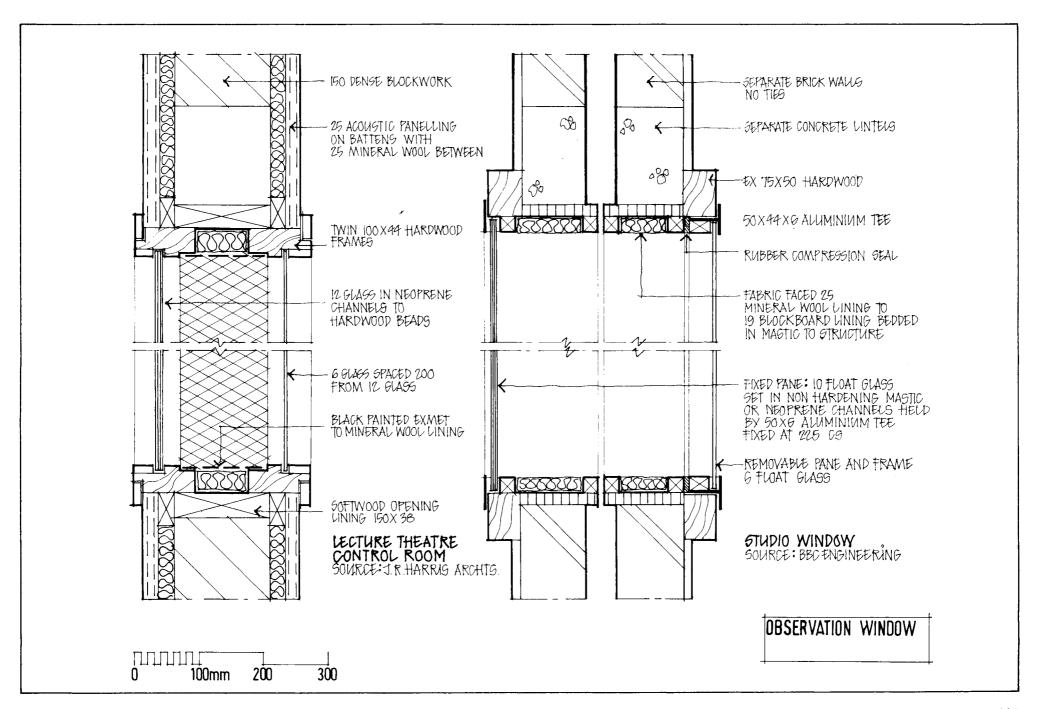


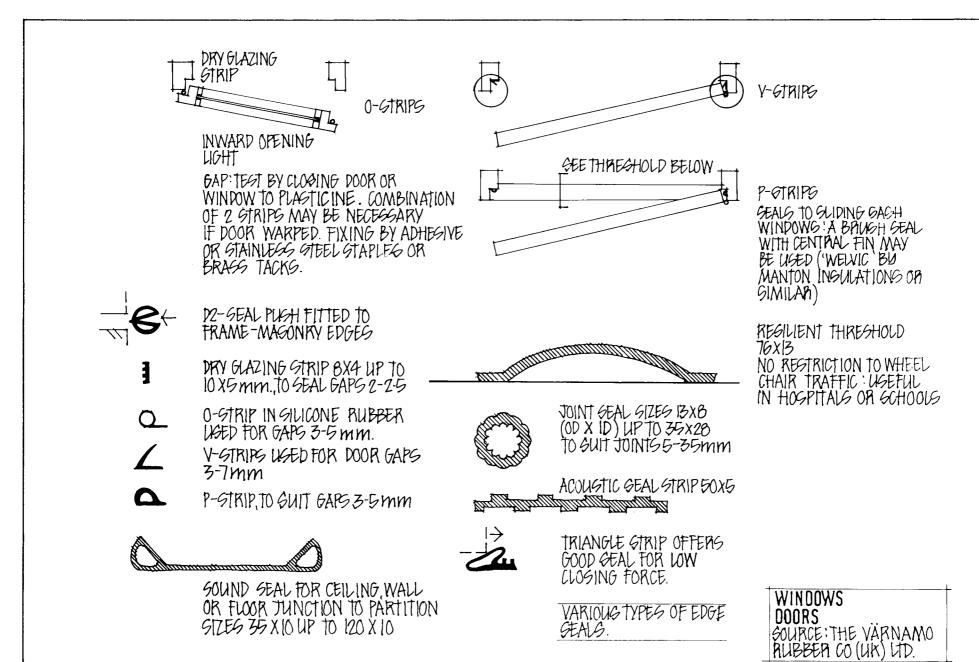






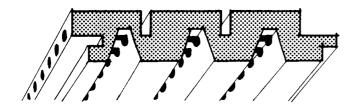






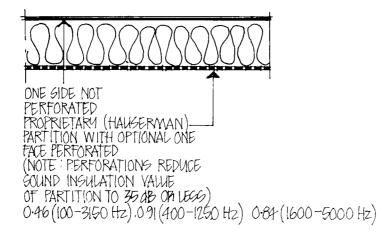
not to scale

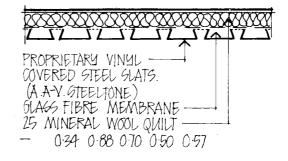
LININGS

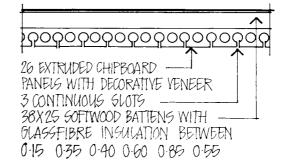


APPLIED ACQUIGITICG VENABLES
PROFILED PROPRIETARY
HARDWOOD PANELS
PATTERN PERFORATED
AS SKETCH

50 X 50 BATTENS TO CEILING (OR WALL) 0:1 0:35 0:80 0:40 0:25 0:35

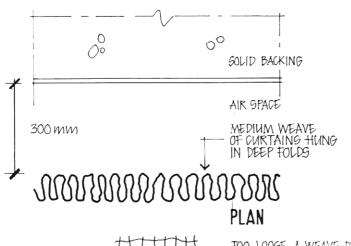


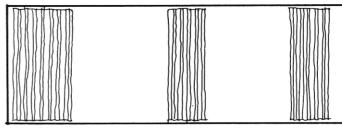




STANDARD VETAILS.

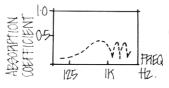
WALL FINISHES /
PARTITIONS
GOUND ABSORPTION.





ROOM ELEVATION

AREAS OF CURTAINS DISTRIBUTED
AROUND ARE MORE EFFECTIVE
IN TERMS OF SOUND ABSORPTION
AND GIVE MORE EVEN SOUND QUALITY
THAN IF CONCENTRATED IN ONE AREA



ABGORPTION CHAPACTERISTIC OF THIN CURTAIN NOT HUNG IN FOLDS SPACED OFF WALL

BEST USE OF CURTAIN IS AS IN PLAN, WITH MEDIUM, WEAVE FREE STANDING DIVIDER CURTAINS ARE LESS EFFECTIVE GURTAINS ARE A SIMPLE METHOD OF PROVIDING AN ADAPTABLE AMOUNT OF ABSORPTION ES. IN MUSIC PRACTICE ROOMS. CURTAIN LINING ALGO IMPROVES GOUND ABGORPTION.

CURTAINS



TOO LOOSE A WEAVE DENSITY AND MATERIAL IS ACOUSTICALLY TRANSPARENT

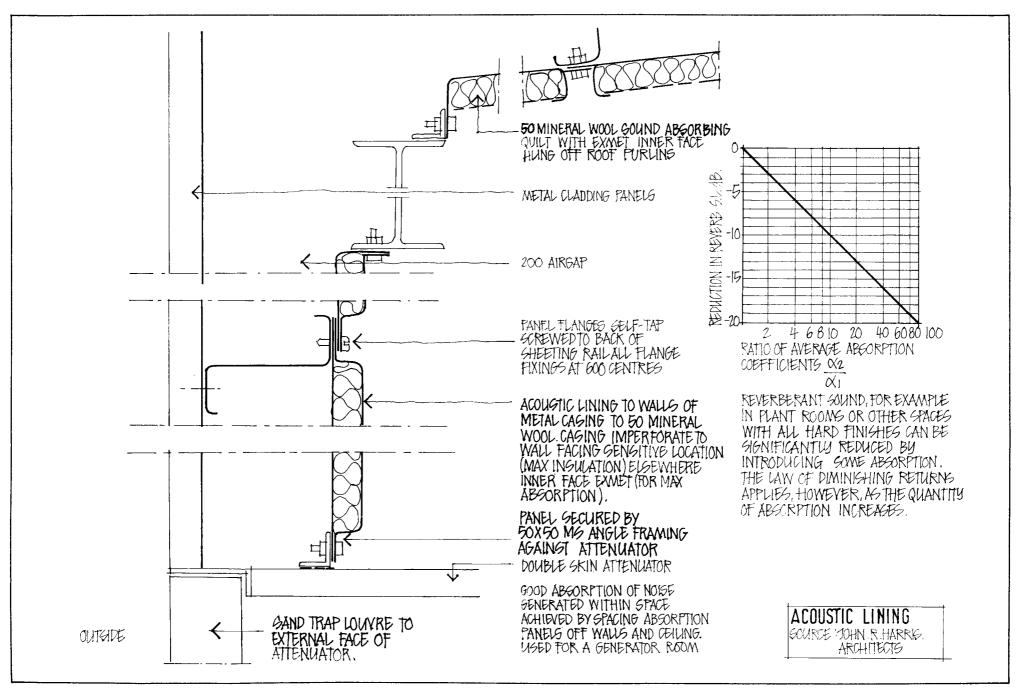


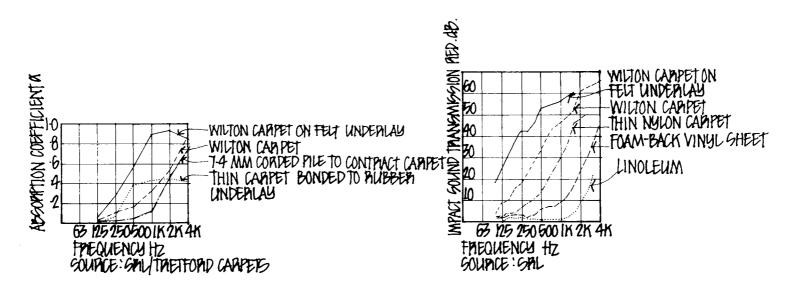
MEDILIM WEAVE GIVES MUCH BETTER ABGORPTION THAN 1. OR 2. TEST BY TRYING TO BLOW THROUGH MATERIAL IT SHOULD BE POSSIBLE TO BLOW THROUGH THE FABRIC BUT WITH GAME REGISTANCE: FABRIC HAS OFTIMUM FLOW RESISTANCE TO SOUND



TOC TIGHT A WEAVE AND THE MATERIAL IS ONLY SLIGHTLY SOUND ABSORPTIVE.

not to scale





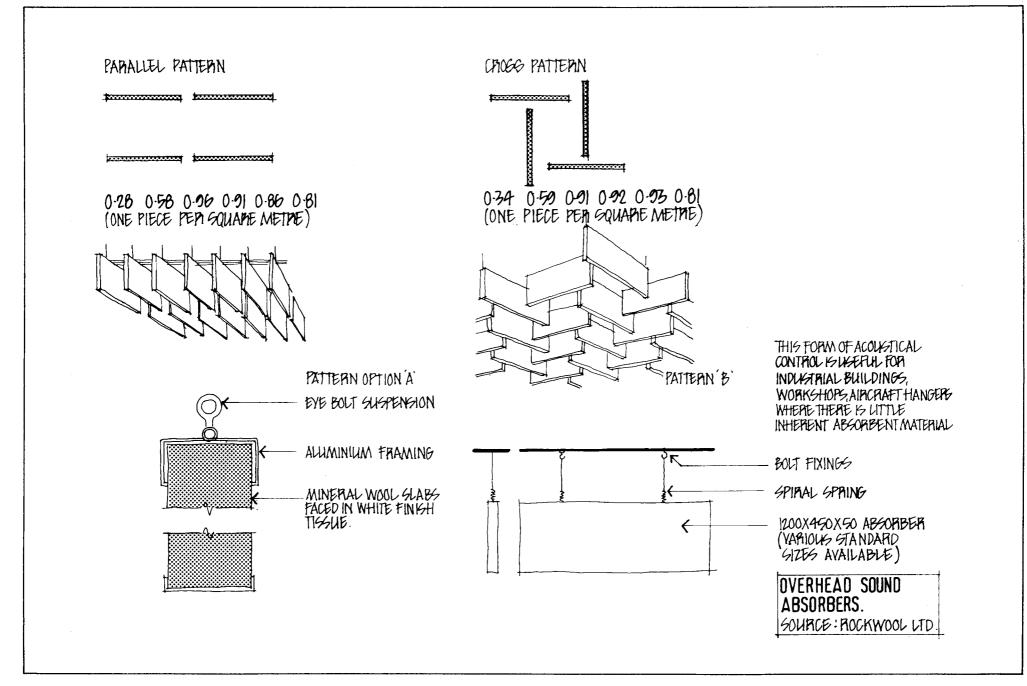
CARPET IS USEFUL FOR BOTH IMPACT GOUND REDUCTION [FOOTFALL AND TO FLOOR BELOW] AND FOR SOUND ABSORPTION. VALUES ARE SHOWN IN APPENDIX BUT FOR THIN CARPET ON SOLID BACKING [TYPICAL OFFICE FOR LEASE] YALUES ARE LOW FOR LOW AND MID FREQUENCIES. CARPET IS SOMETIMES LISED AS A HARDWEARING WALL FINISH, FOR EXAMPLE IN CINEMAS. CARPETS ON THIN WALL PANELS [SEE DETAIL ASSEMBLY (4)] GIVE A BROADER FREQUENCY PERFORMANCE.

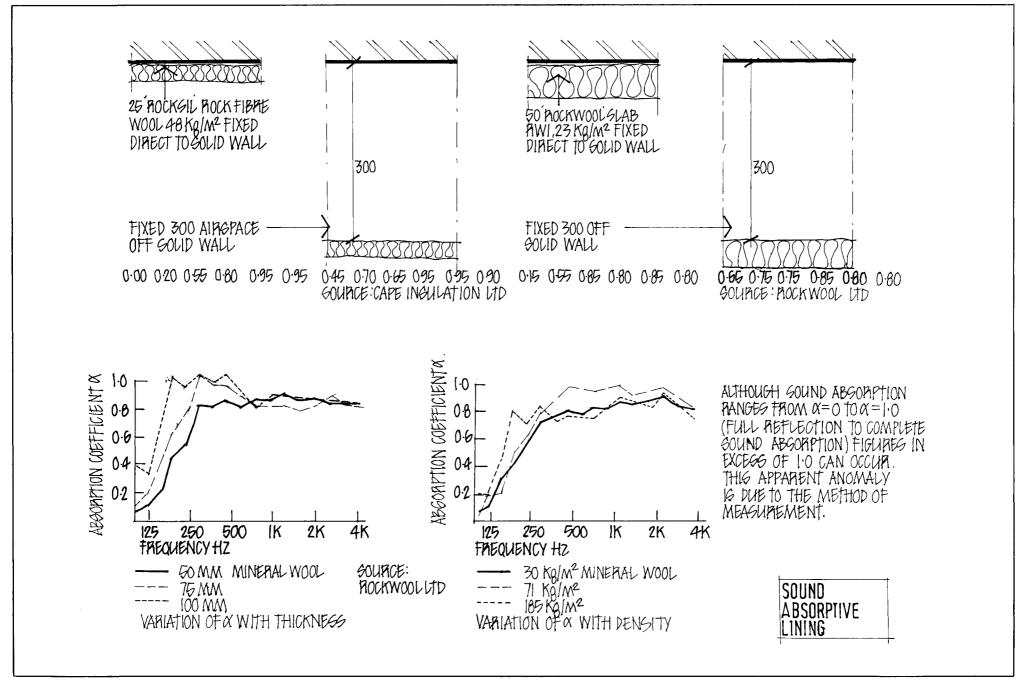
CUGHIONED YINYL GHEET.
CUGHIONED VINYL GHEET
ONLY 3MM THICK (POLYTHEAD ORGM.)
ON A CONCRETE GLAB CAN GIVE
IMPACT GOUND THANGMIGGION
PERFORMANCE, EXCEEDING
GRADE I BUILDING REGG.
THIS IS A LIGEFUL MATERIAL
FOR HOSPITALS, SCHOOLS AND
OLD PEOPLES HOMES WHERE
CARPET CANNOT BE LIGED

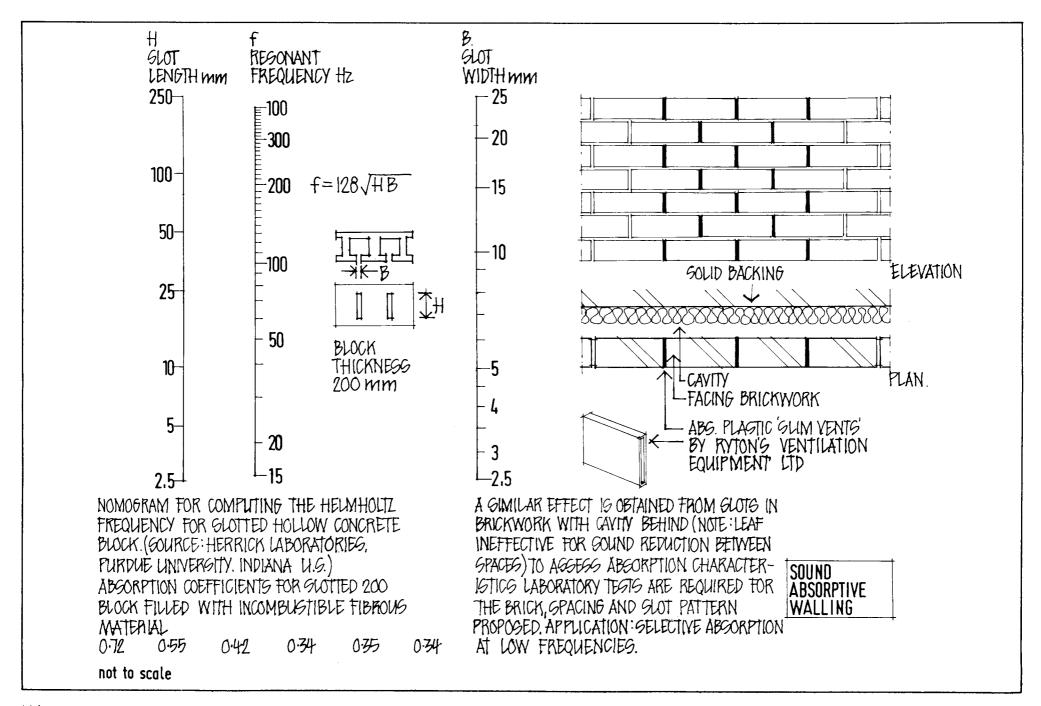
FINISHES [BRS 103 DEFINITION]
SOFT: CUSHIONED VINYL SHEET
THIN CARPET WITH
UNDERLAY THICK CARPET
WITH OR WITHOUT UNDERLAY, CORK TILES OVER 8MM
TILES.
HARD: CONCRETE, TERRAZZO,
PVC TILES, WOOD BLOCK.

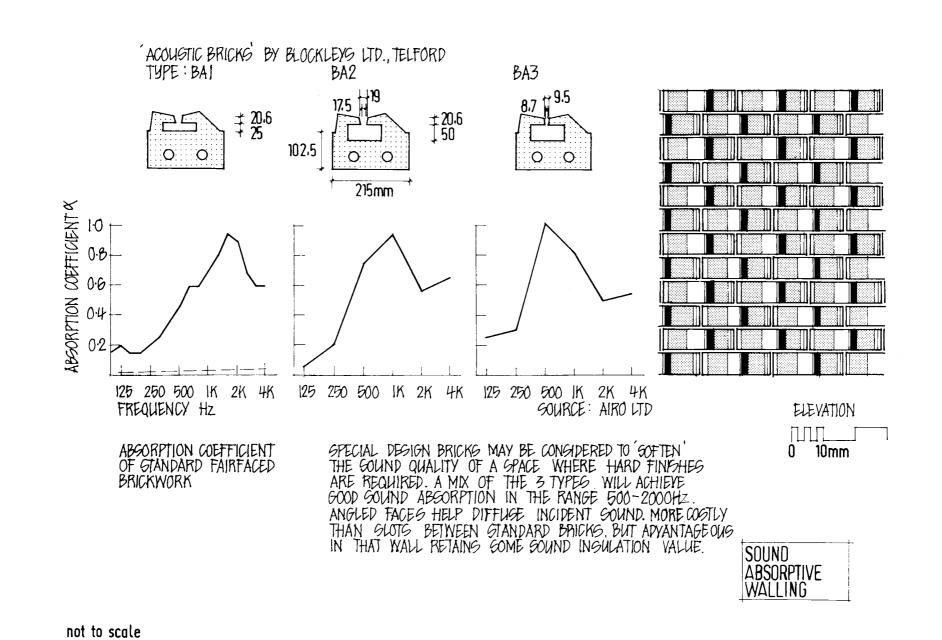
MASTIC ASPHALT.

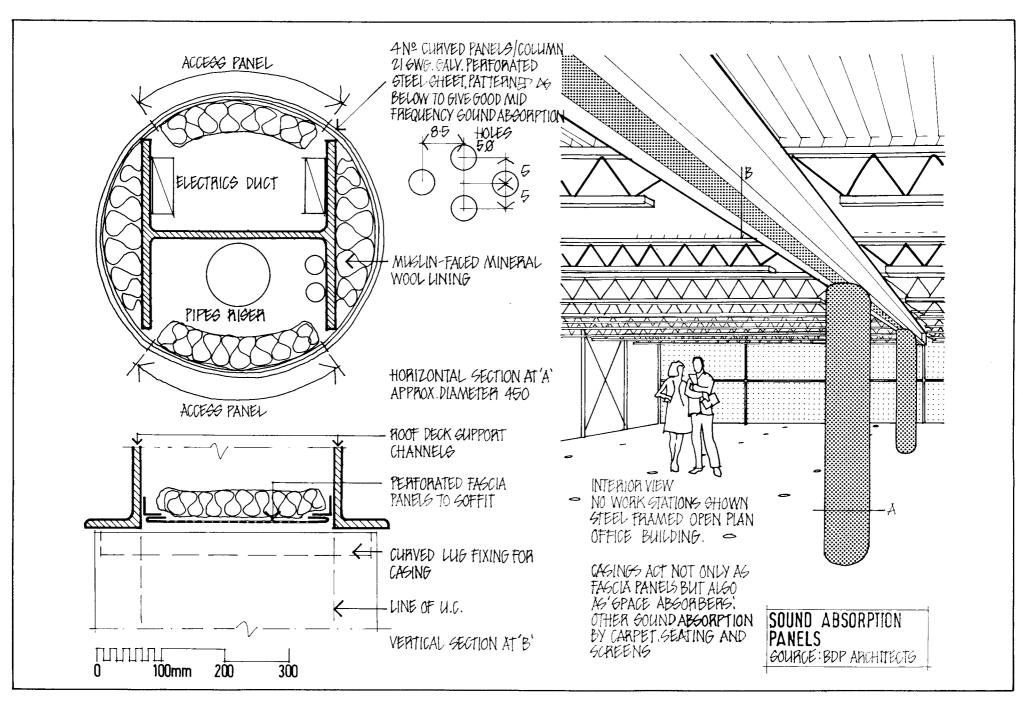
FINISHES

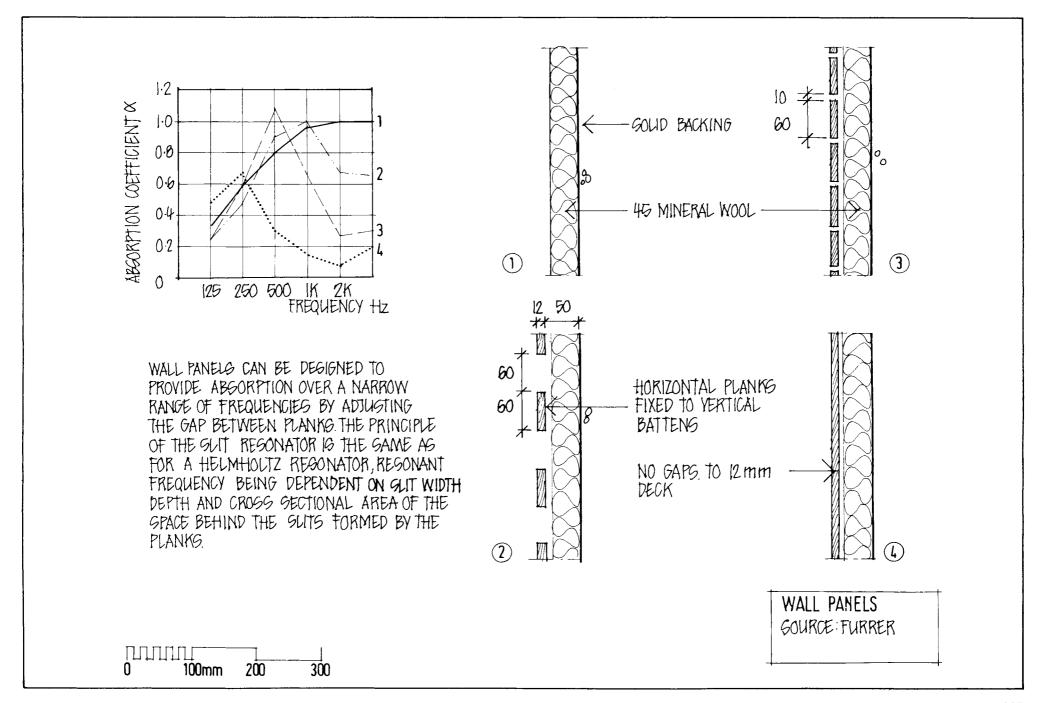


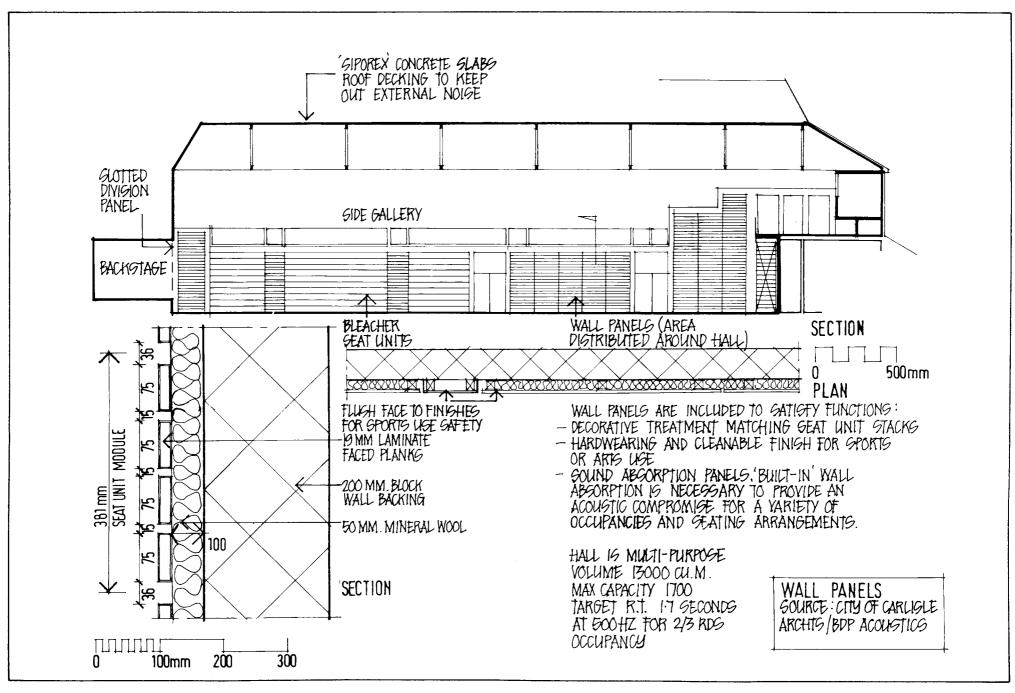


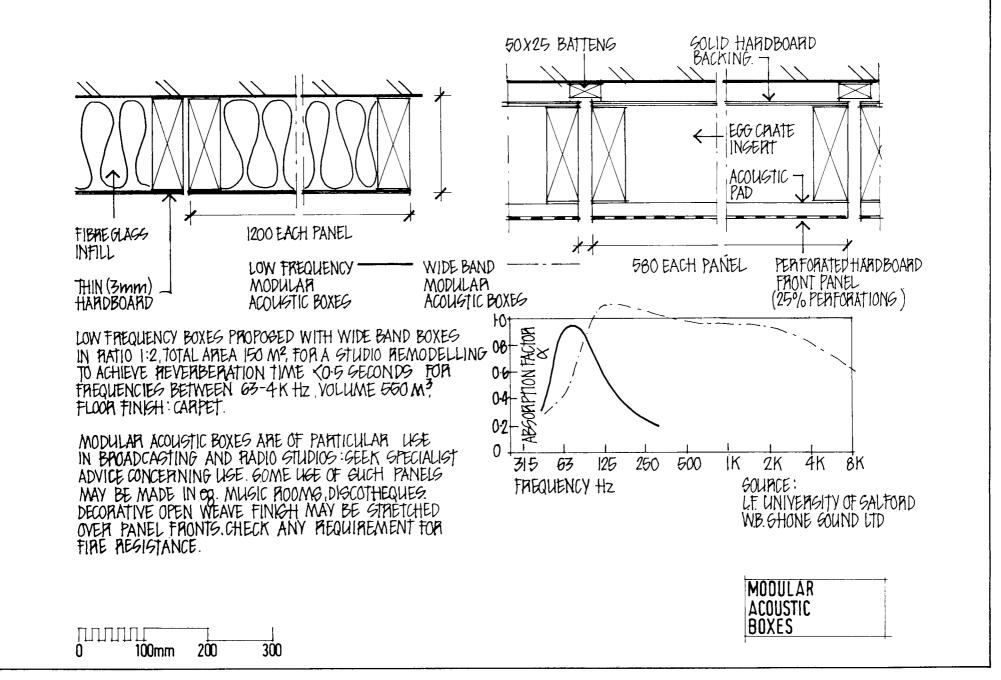


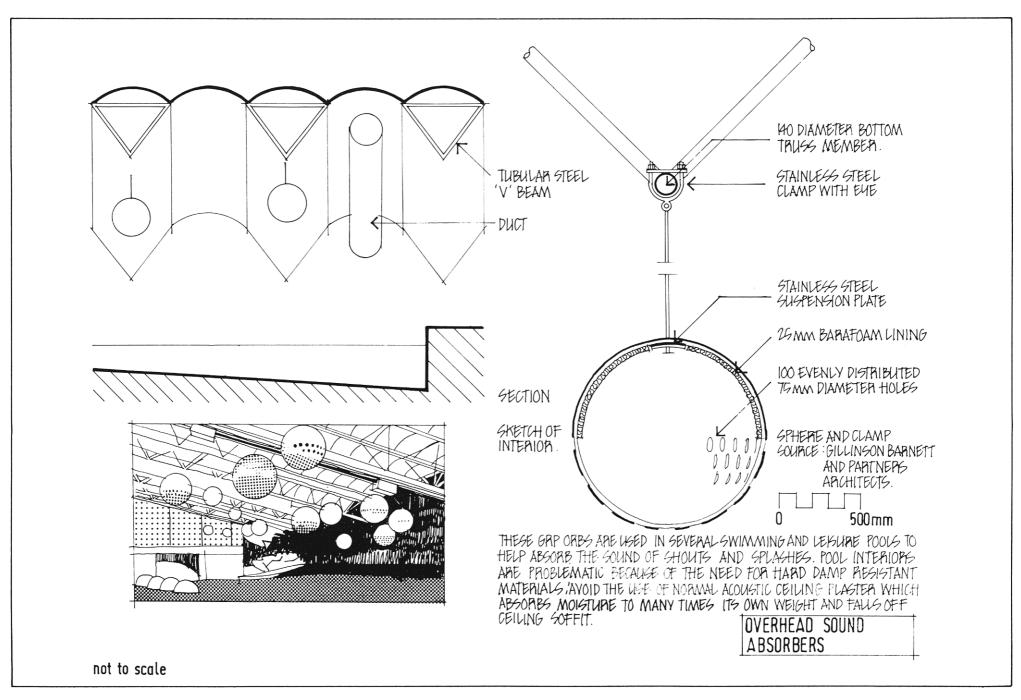




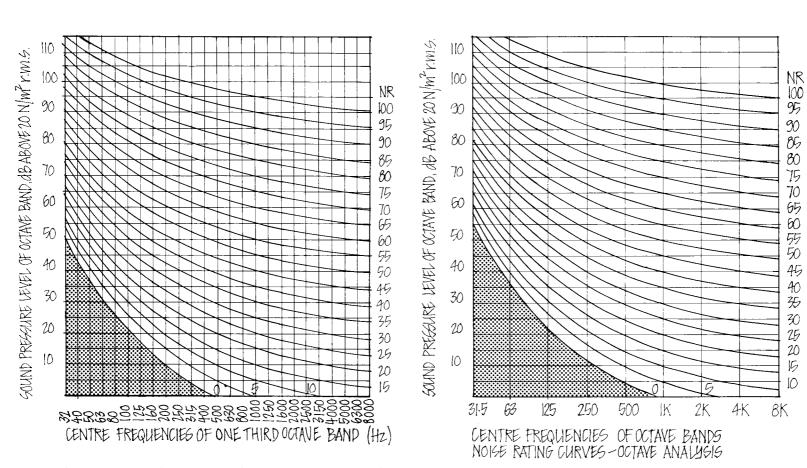






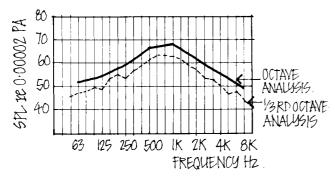


SERVICES



IT IS CONVENIENT TO SPECIFY THE LEVEL OF A PARTICULAR NOISE BY EQUAL LOUDNESS CONTOURS WHICH RECOGNISE THAT
THE SUBJECTIVE RESPONSE BY THE EAR IS TO FIND LOW-FREQUENCY NOISE LEGS NOTICEABLE THAN HIGH FREQUENCY
FOR THE SAME SOUND POWER LEVEL. THE CONTOURS ABOVE ARE NOISE RATING (NR) CURVES, ANOTHER FORM IS PNC
CURVES WHICH ARE VERY SIMILAR AT MOST FREQUENCIES. CURVES CAN BE USED TO MONITOR THAT THE AMBIENT SOUND
LEYEL IN A SPACE IS NOT AT AN UNSUITABLY HIGH LEVEL DUE TO EXTERNAL, VENTILATION, MACHINERY OR ADJACENT ROOM
NOISES. THE MAXIMUM BAND LEVEL OF THE NOISE SPECTRAL DISTRIBUTION DETERMINES ITS NR CURVE RATING.
SOUND INSULATION VALUES CAN BE USED TO CHECK SOUND PENETRATING AT EACH FREQUENCY BAND.

[AMBIENT NOISE CONTROL (1)]



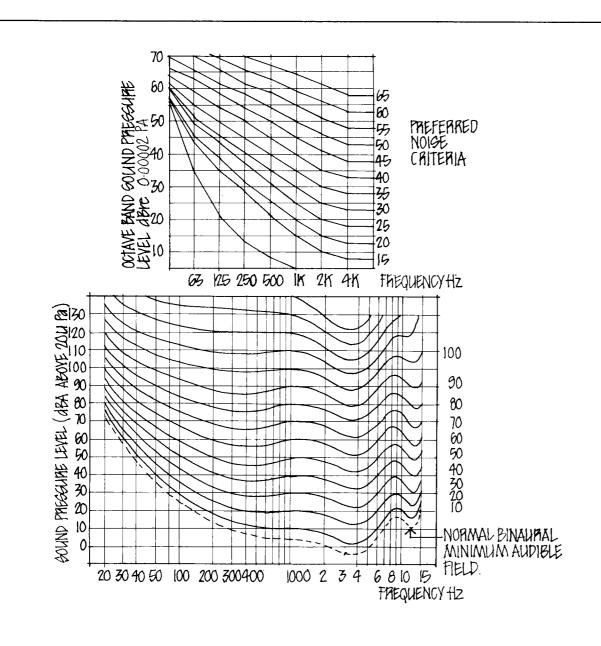
NOISE ANALYSIS IN A CANTEEN SOURCE: PARKIN, HUMPHREYS AND COWELL.

CARE SHOULD BE TAKEN THAT FIGURES USED ARE FOR OCTAVE BAND ANALYSIS AS ONE-THIRD OCTAVE BAND REQUIRES USE OF THE LHS. SET OF NR CURVES. BECAUSE OF THE REDUCED BAND-WIDTH COMPONENT INDIVIDUAL LEVELS ARE ABOUT, 5 dB DOWN AND THE 13 RD OCTAVE NR CURVES ALLOW FOR THIS. WHEN 13 RD OCTAVE BAND LEVELS ARE ADDED TOGETHER. A HIGHER FIGURE RESULTS AS THE LEVEL OVER THE WHOLE TREQUENCY RANGE.

RECOMMENDED NR. LEVELS FOR AMBIENT NOISE CONTROL TO GUIT USE	NR
STUDIOS SPACES FOR RECORDING OR BROADCAST	15
CONCERT HALLS	15-20
THEATREG, MULTI-PURPOSE HALLG CONFERENCE ROOMS, COURT ROOMS.	25
HOSPITAL WARDS, HOTEL BEDROOMS LIBRARIES	25-30
CLAGGROOMS, MEETING ROOMS FOR SMALL GROUPS, EXECUTIVE OFFICES, HOMES.	30
RESTAURANTS, OPEN PLAN AND GENERAL OFFICES	35
CAFETERIAS, CIRCULATION	40
KITCHENG, TOILETS AND WORKSHOPS	45
CAR PARKS, SHOPPING MALLS, BUS, RAIL OR AIRPORT CONCOURSES.	50
OFFICE (TYPING, WOND PROCEGS MACHINES) WORKGHOPS, INDUSTRIAL PHOCEGS	55 65

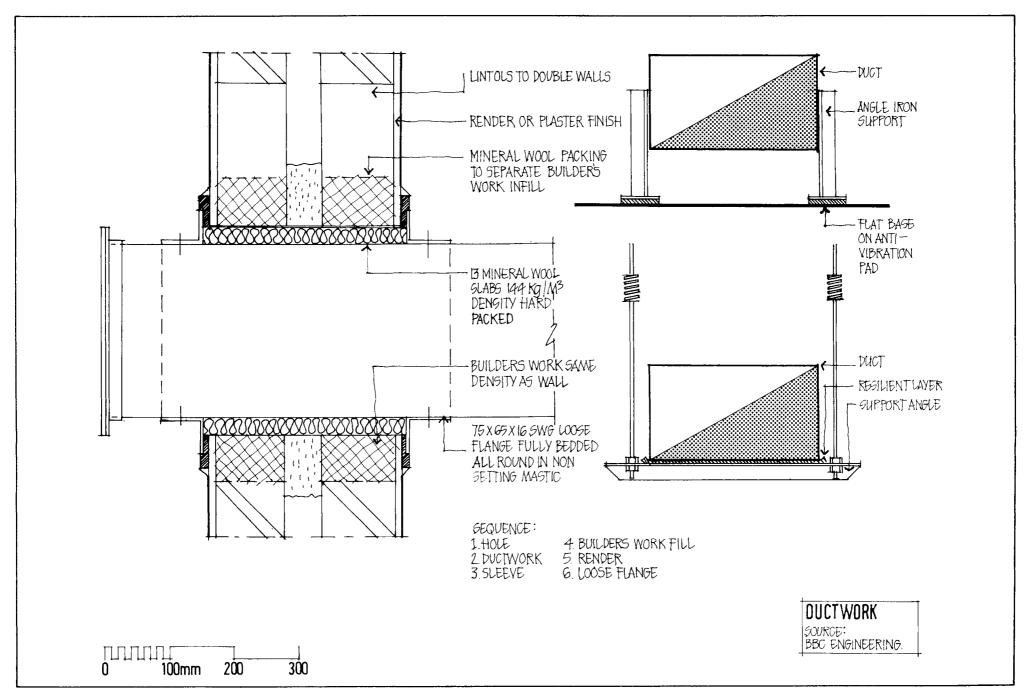
DEGINABLE AB(A) CRITERIA 5-10 ABOVE RECOMMENDED NA LEVEL

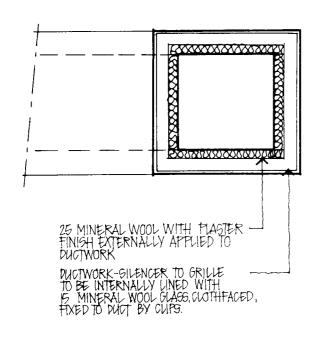
AMBIENT NOISE CONTROL (2)



NA CURVEG TEND TO BE UGED IN EUROPE, WHERE AS IN THE UGA THE 1071 PREFERRED NOISE CRITERIA (PNC) CURVEG HAVE REPLACED THE EARLIER NOISE CRITERION (NC) CURVES. THEY HAVE, HOWEVER, NOT RECEIVED UNIVERSAL ACCEPTANCE. COMPANISON WITH THE EQUAL LOUDNESS CONTOURS SHOWS THE INTENTION OF EITHER SET OF CURVES TO REFLECT THE DIFFERENT SENSITIVITY OF EAR AT DIFFERENT PARTS OF THE FREQUENCY RANGE.

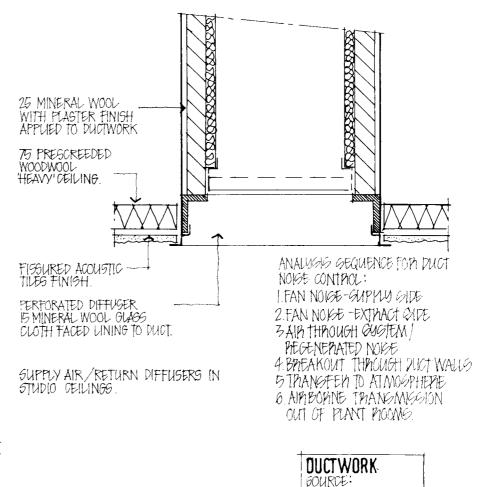
AMBIENT NOISE CONTROL (3)





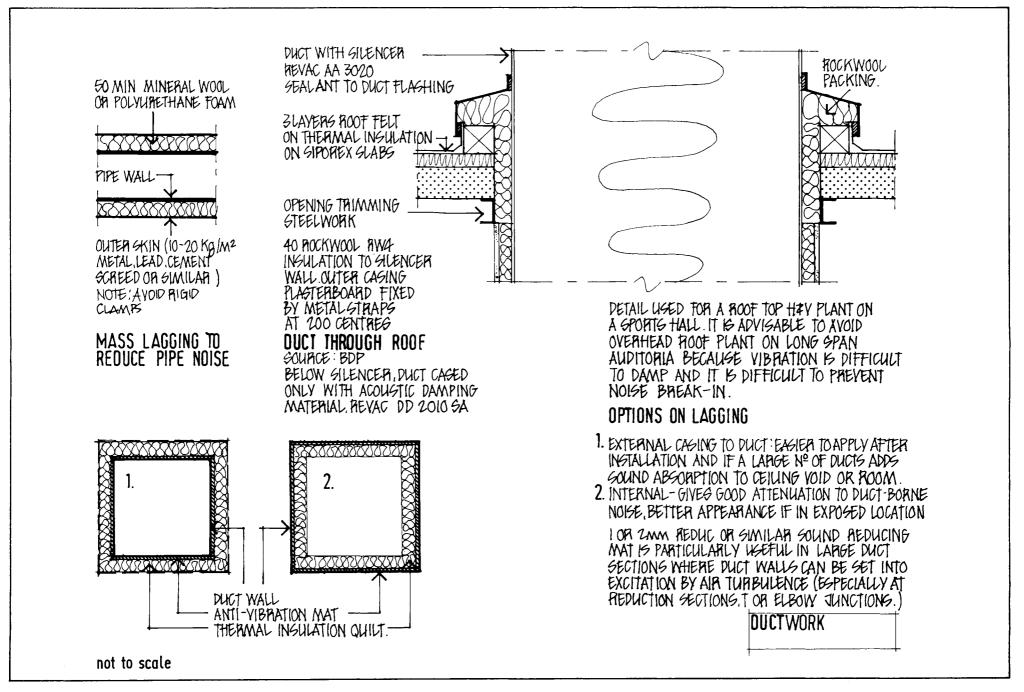
DUCT LINING.

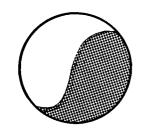
WHERE LARGE LOW AIR VELOCITY DUCTO
ARE NECESOARY TO ACHIEVE LOW AMBIENT
NOBE LEVELS, BUILDERS WORK DUCTO MAY BE
AN ECONOMIC SOLUTION FOR BOTH SUPPLY AND EXTRACT.



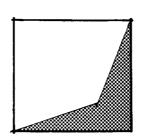
BBC ENGINEERING

not to scale



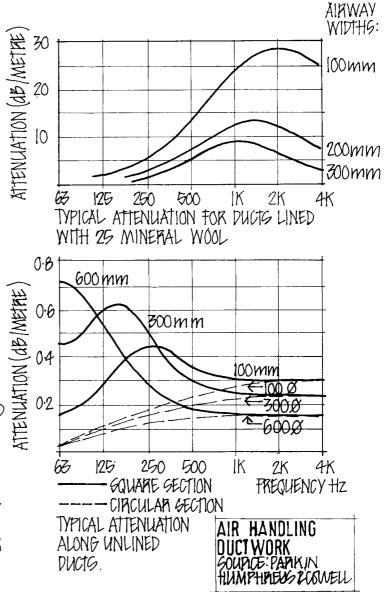


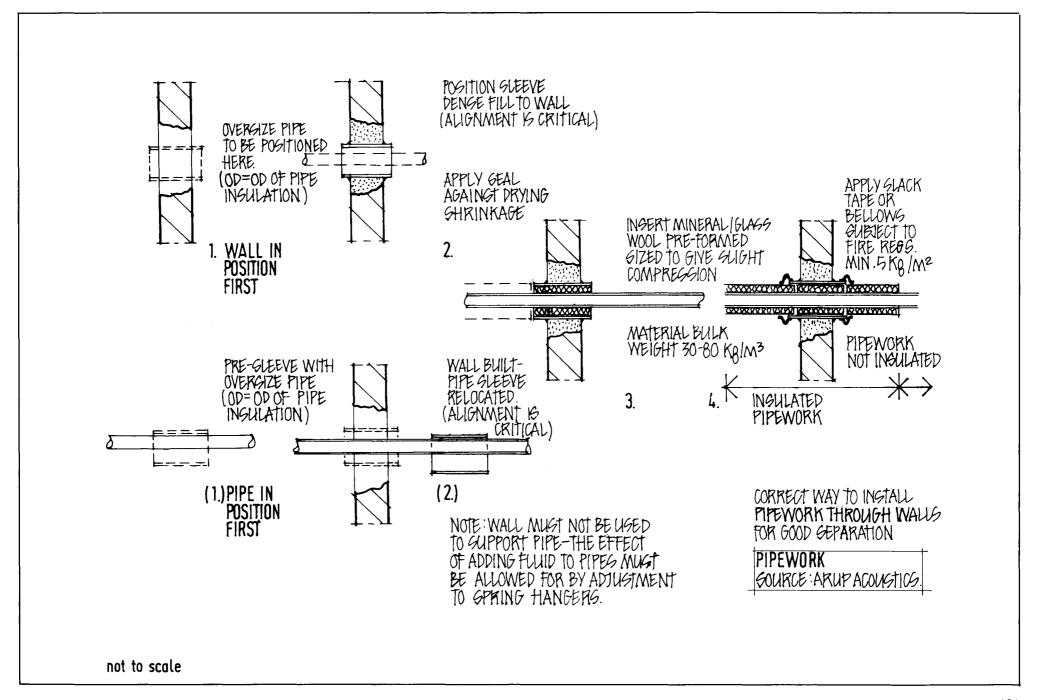
YG.

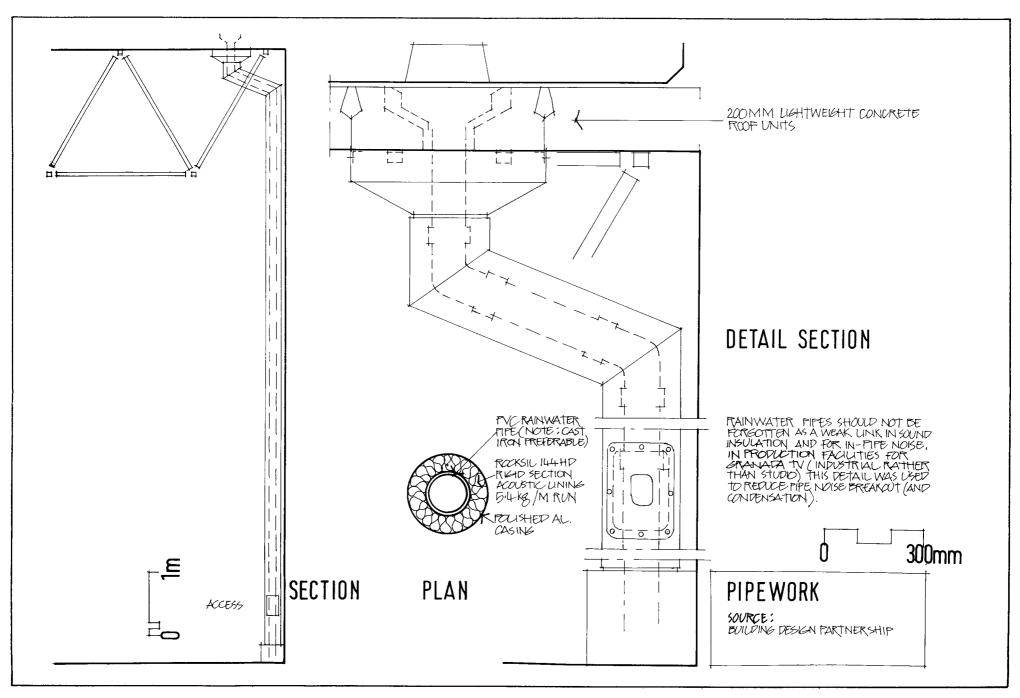


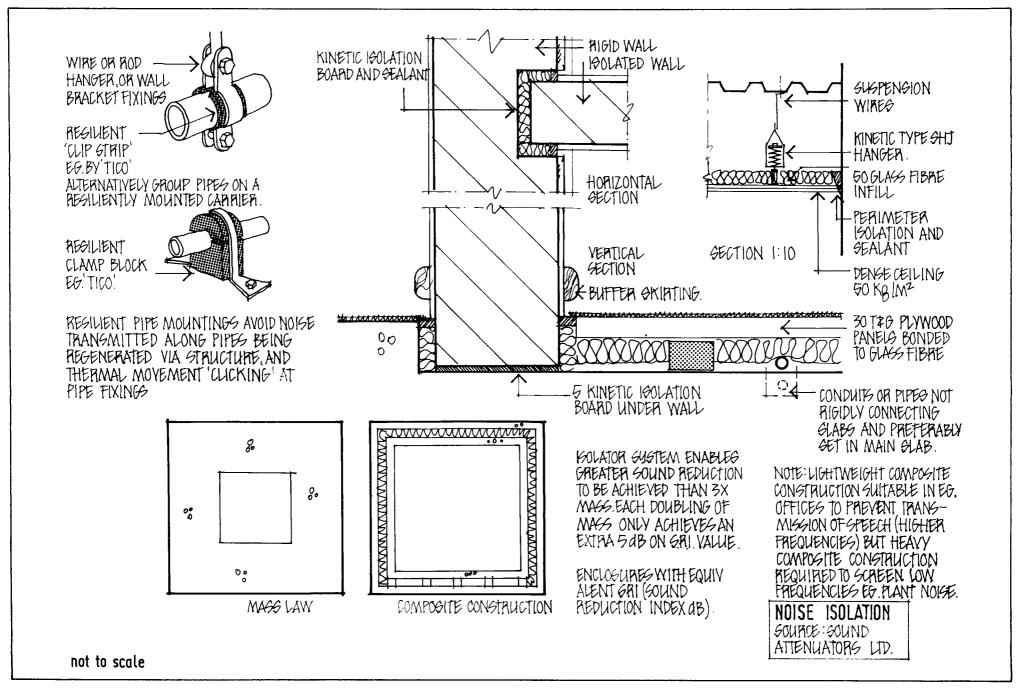
CIACULAR DUCTS ARE INHERENTLY AIGID AND OF MINIMUM PERIMETER FOR SECTIONAL APIEA: NOISE IS CONTAINED WITHIN PATHER THAN TRANGMITTED THROUGH DUCT TO SPACE. LIGE OF CIRCULAR DUCTWORK MAY THEREFORE BE PREFERABLE FOR EXPOSED INSTALLATIONS. CIRCULAR ATTENUATORS TEND TO BE LEGG EFFICIENT: OFTEN TRANSFORMATION PIECES FROM CIRCULAR PUCTWORK TO RECTANGULAR SILENCERS ARE USED IN PRACTICE.

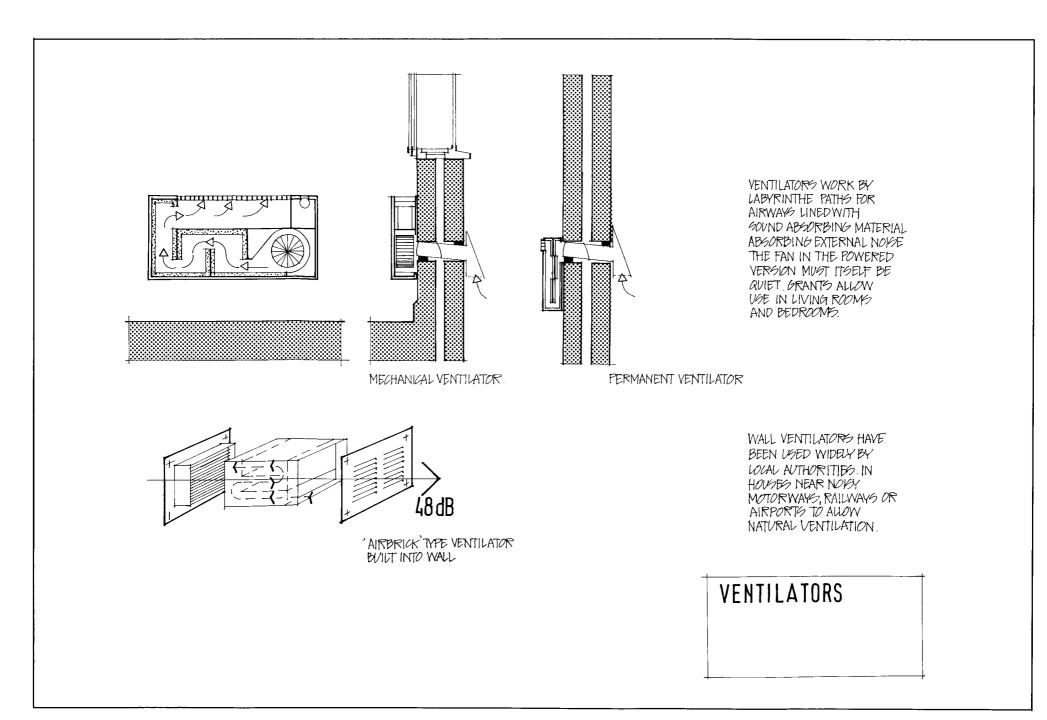
RECTANGULAR DUCTS HAVE LEGG ALGID WALLS AND NOIGE WITHIN EXCITES THE FLAT METAL SECTIONS. THIS GIVES LIBETUL LOW FREQUENCY ATTENUATION ALONG DUCTS, THERE IS ALGO A LARGER INTERNAL AREA FOR LINING WITH MINERAL WOOL: USE OF SQUARE OR RECTANGULAR DUCTWORK IS BEST FOR INSTALLATIONS MOUNTED IN CEILINGG, GUPPLYING OF EXTRACTING AIR AT A LOW NOISE LEVEL, INHERENT ATTENUATION MAY ALLOW ECONOMY OF ATTENUATORS ALONG DUCTS.LINING DUCTS IS PARTICULARLY EFFECTIVE FOR SMALL DUCTS AND FOR HIGHER FREQUENCIES.

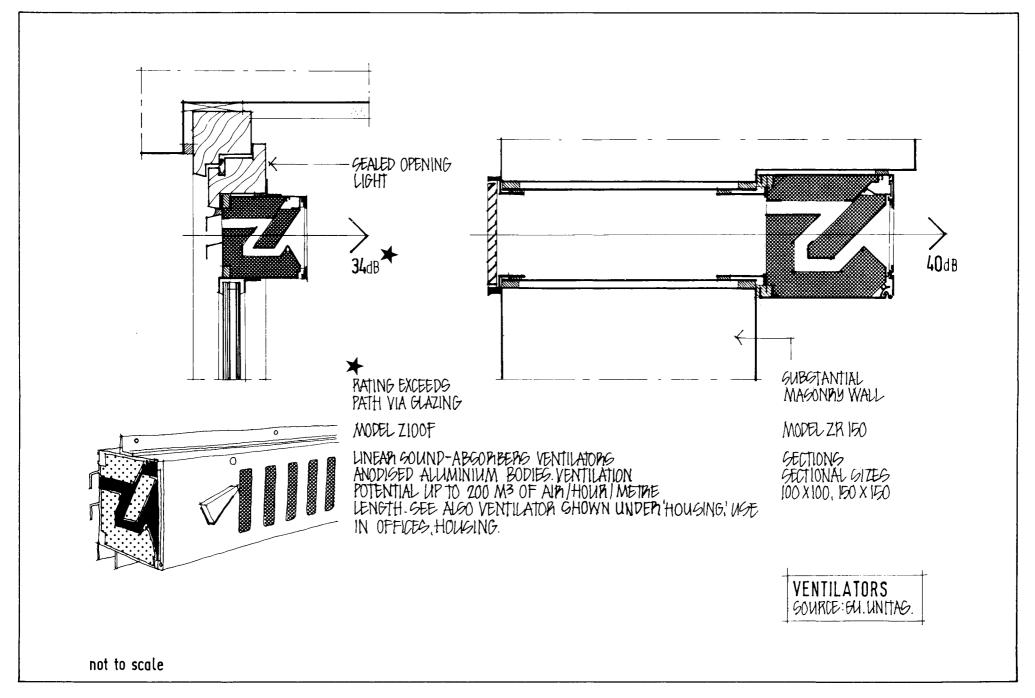




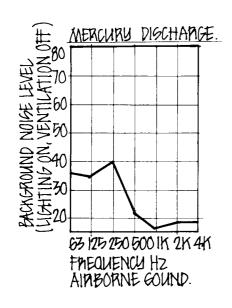








TUNGGTEN
TUNGGTEN LAWPS GIVE OFF NEGLIGIBLE NOIGE
EXCEPT WHEN ABOUT TO FAIL: THE FILAMENTS
THEN NATTLE. TUNGGTEN LIGHTING IS THENETONE
USED FOR ANECHOIC CHAMBERS AND OTHER
NOISE GENGITIVE ROOMS. DIMMER CONTROLS
ON LIGHTING MAY CAUSE SOME NOISE AT LOW
ILLUMINATION SETTING.

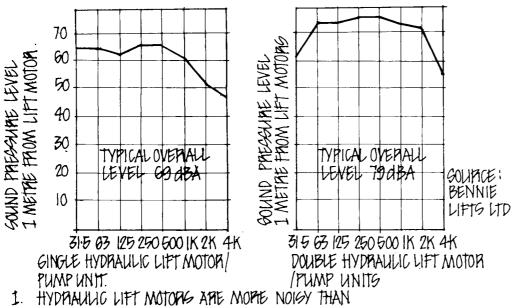


POWERFUL LIGHTING MAY CAUSE
GIGNIFICANT NOISE AT GOME
PARTICULAR FREQUENCY. THE
DISTRIBUTION AT LHS IS A
TOTAL OF 55 400 W LUMINAIRES
(TUPE HPI MBI SPECIAL SPORTS
LIGHTS) MOUNTED UNDER HIGH
LEVEL CATWALKS. IN A MULTIPURPOSE SPORTS HALL OF 11300 CU.M.
AND RT=2 SECONDS AT MID
FREQUENCY. AMBIENT GOUND LEVEL
FOR SPORTS LIGHTING ON, HOUSE
LIGHTS AND VENTILATION OFF
CORRESPONDS TO NR=30.

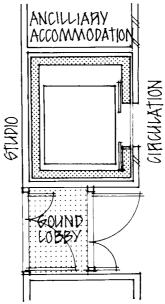
GOURCE: GANDU BROWN AGGOCIATEG.

FLUORESCENT. THERE IS A GREAT VARIATION OF NOISE FROM THE MAIN GOURCE, THE CONTROL GEAR, EVEN FOR FITTINGS OF THE GAME TYPE FROM THE SAME MANUTAGURER. THE LAMINATED IRON CORE PRODUCES NOIGE DUE TO MAGNETIGATION OF THE LAMINATIONS, YARVING ACCORDING TOTHE TYPE OF CIRCUIT AND WATTAGE RATING. THE METHOD OF MOUNTING FITTINGS AFFECTS NOISE OUTPUT: HANGING FITTINGS ARE PREFERABLE TO SOLID FIXING IN GENGITIVE APPEAG, PREMOTE CONTROL GEAR MAY HAVE TO BE CONGIDERED. INDIVIDUAL FITTINGS MAU NOT BE NOIGY. FOR INGTANCE A FITTING RECENTLY TESTED HAD A WORST CAGE SWL OF 23.3 dB AT 630 Hz. HOWEVER, 32 GUCH FITTINGS IN A PHODAL AS A TYPICAL ARRANGEMENT WERE CALCULATED TO PROPUCE A SOUND LEVEL APPROXIMATING NR=25 AT 630 Hz SOURCE: UNIVERSITY OF SALFORD

LI	GH	TIN	G	-



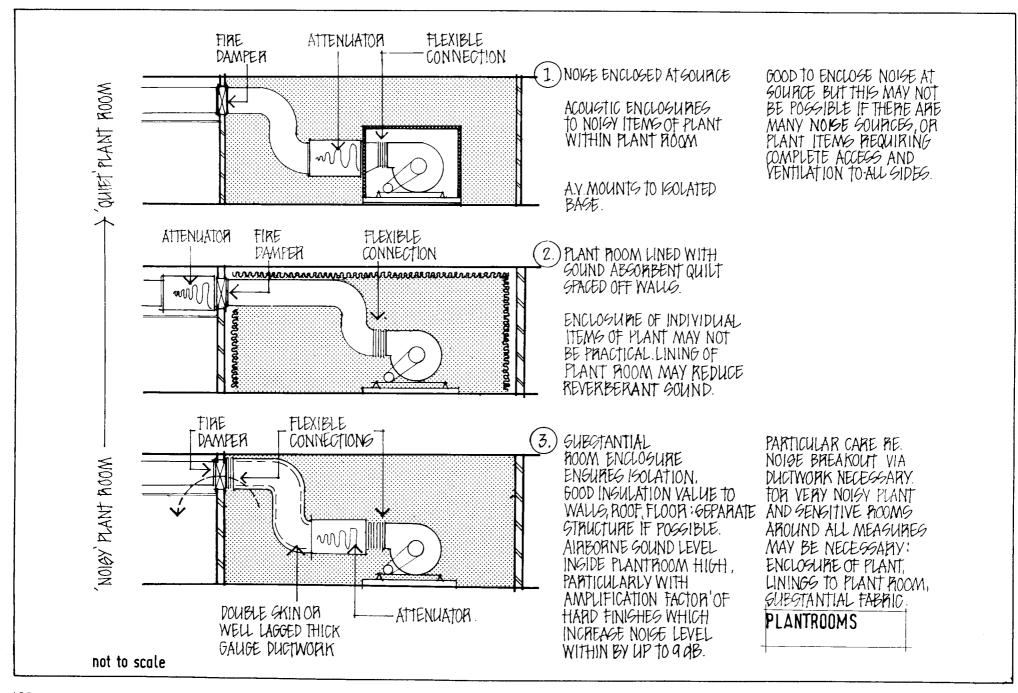
- I. HYDRAULG LIFT MOTORS ARE MORE NOISY THAN ELECTRIC MOTORS: MINIMISE BY SPECIFYING PUMP AND MOTOR TO BE SUBMERSIBLE TYPE AND TO HAVE CASINGS LINED WITH SOUND DEADENING MATERIAL.
- 2. SELECT LIFT DOORS FOR QUIET OPERATION
- 3. CHECK HIGH SPEED/HIGH RIGE LIFTS FOR WIND NOISE UPSHAFT
- 4. ALL MACHINERY TO BE ON ANTI-VIBRATION MOUNTINGS
- 5 AVOID BUILDERS WORK HOLES BETWEEN LIFT SHAFTS AND OTHER AREAS.
- 6. CHOOSE ELECTRONIC PROXIMITY SWITCHES ETC. AS A WAY OF AVOIDING 'CLICKING' WORKING PARTS IN CONTROL GEAR
- 7. ENGURE GOOD MAINTENANCE OF LIFTS.
- 8. IN REFURBISHMENT SCHEMES, CHECK NOISE FROM EXISTING LIFT INSTALLATIONS (OLDER TYPES, ESPECIALLY OPEN SHAFT, WERE FAR NOISIER.)

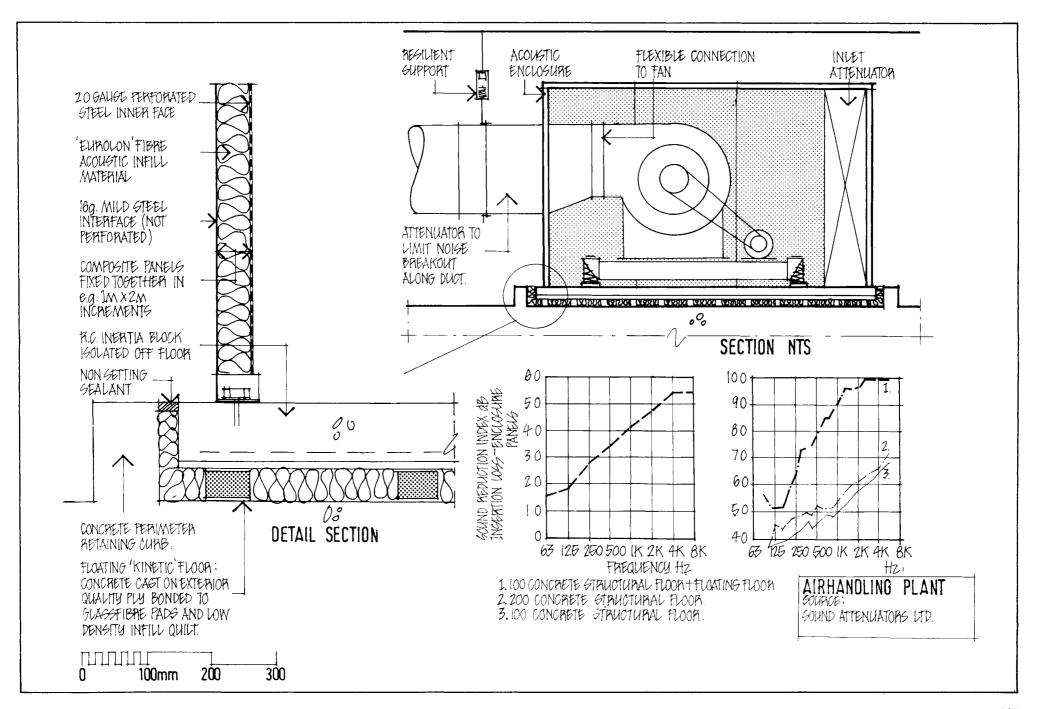


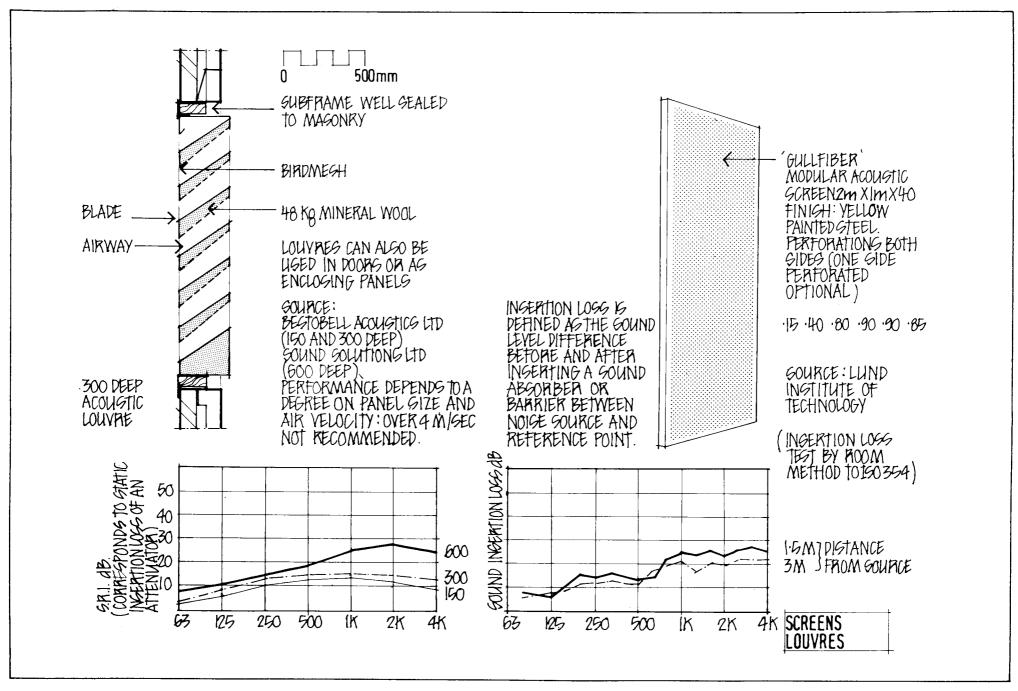
TYPICAL IGOLATED GHAFT PLAN ARRANGEMENT.

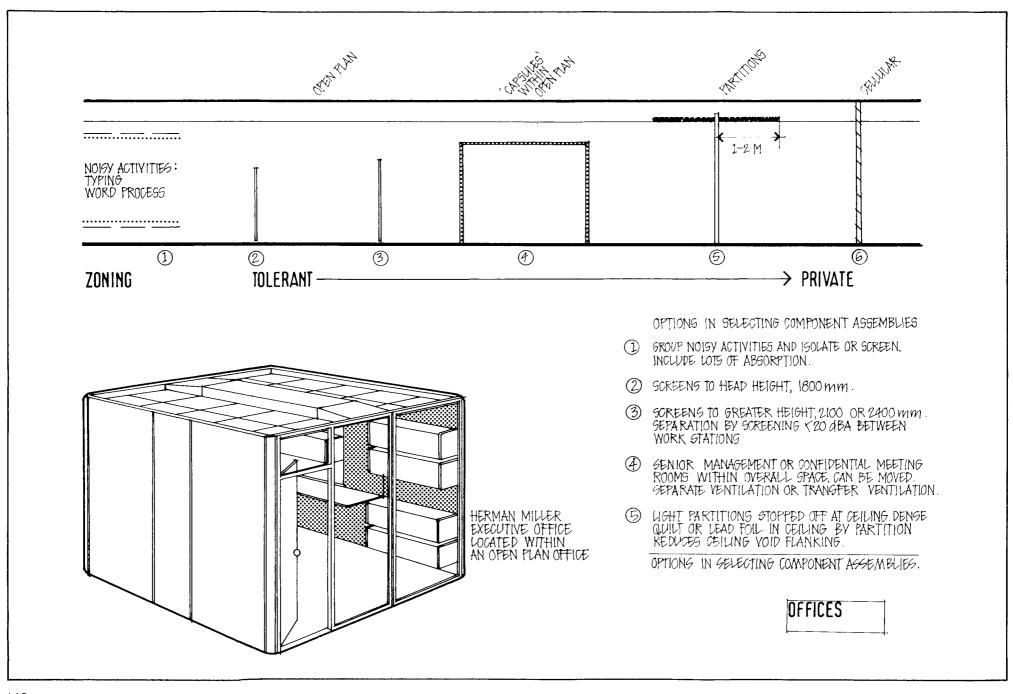
LIFT NOISE IS OF PARTICULAR CONCERN IN HOTELS OR HOSPITALS WHERE THE NOISE LEVELS FROM MACHINERY MAY NOT BE HIGH, BUT THE DISCONTINUITY OF OPERATION DRAWS ATTENTION TO THE NOISE. TYPICAL GOUND LEVELS WITHIN LIFT CAR ARE 65 dB FOR HYDRAULIC, 60 dB FOR ELECTRIC OPERATION.

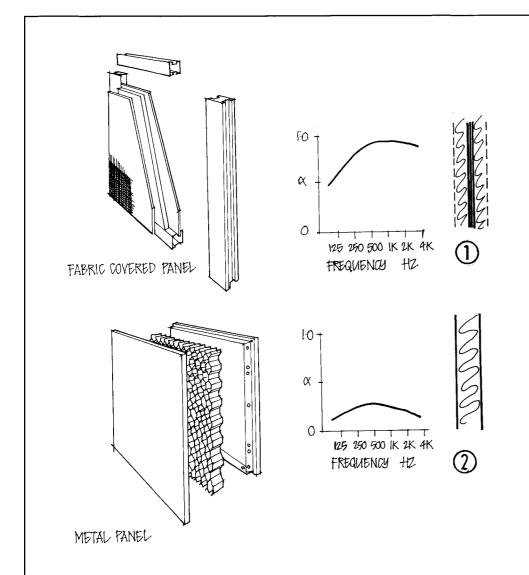
LIFTS	
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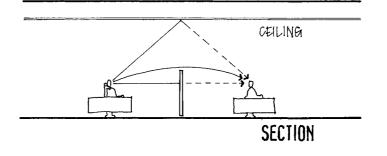


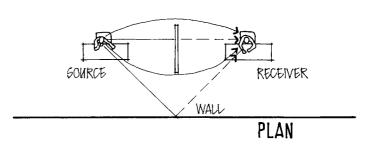








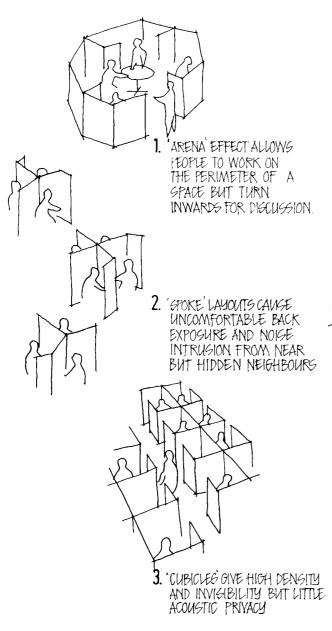




FOR A REASONABLE SPACING OF OCCUPANTS EG. 12-14 MP PERSON
SOUND ATTENUATION BETWEEN WORKPLACES ONLY 20-25 dBA MAX,
EMPIRICAL FORMULA TO CHECK ADEQUATE PRIVACY: BACKGROUND NOISE
(dBA)+ SOUND ATTENUATION > 75. BY THIS CRITERIA MANY OFFICES
HAVE AN AMBIENT LEVEL TOO LOW AND MASKING SOUND MAY BE CONGIDERED.

IN CHOOSING PARTITION SYSTEMS OR DIVIDER PANELS, LOOK FOR SANDWICH OF ABSORPTION-SOLID CORE-ABSORPTION IF A GOOD ABSORPTION RATING (OVER 0.6) IS REQUIRED. BOTH EXAMPLE 1 AND 2 ABOVE ARE EFFECTIVE AS SCREENS. GOOD ABSORPTION AT 1-2 K IMPORTANT TO MASK SPEECH.

OPEN PLAN OFFICES



<i>//</i>	

TO AVOID REFLECTED
SOUND AT PERIMETER
CURTAIN WALL: TRAP
SOUND BY ENCLOSING
ABSORPTIVE END PANELS.

LAYOUT TYPE		STAFF ATTITUDES	
FREEFLOW	12%	NATURE OF COMMON COM	PLAINTS
PLANNED TO	60%	AND REQUESTS:	
WORKFLOW AND		MORE PRIVACY	42%
RELATIONSHIPS		INTERNAL NOISE	42%
DIVISION BY	#4%	TEMPERATURE	42%
ACOUSTIC SCREENS		VENTILATION	38%
DIVIGION BY	32%	TOO MUCH DISTRACTION	25%
FURNITURE	0210	DRAUGHTS	17%
DNISION BY HALF	16%	BETTER FURNITURE	12°/0
HEIGHT PARTITIONS	10/0	BETTER LAYOUT	8%
REGULTE OF A LARGE	UK OFF	ICE LIGE, GLIRVELI	

REGULTS OF A LARGE U.K. OFFICE USE SURVEY SOURCE: SPACE PLANNING SERVICES

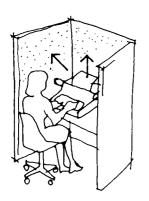
ABILITY TO CONVERGE AS A FUNCTION OF BACKGROUND NOKE

NOIGE LEVEL (NR)	CONVERSATION	FOR NORMAL M REFLECTING	Nº PEOPLE IN CONFERENCE
30	8	50	50
35	6	25	20
40	4	10	10
50	2	2	4
55	1	1	2

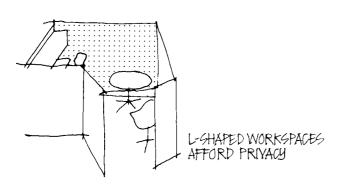
SOURCE: R.A.WALLER. APPLIED ACOUSTICS(2) 1961 PP121-130

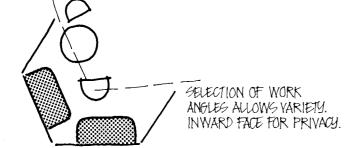
OPEN-PLAN OFFICES

SOURCE HERMAN MILLER RESEARCH CORPORATION.



ENCLOSE NOISY ACTIVITIES USE SCREENS EXTENDING TO FLOOR.

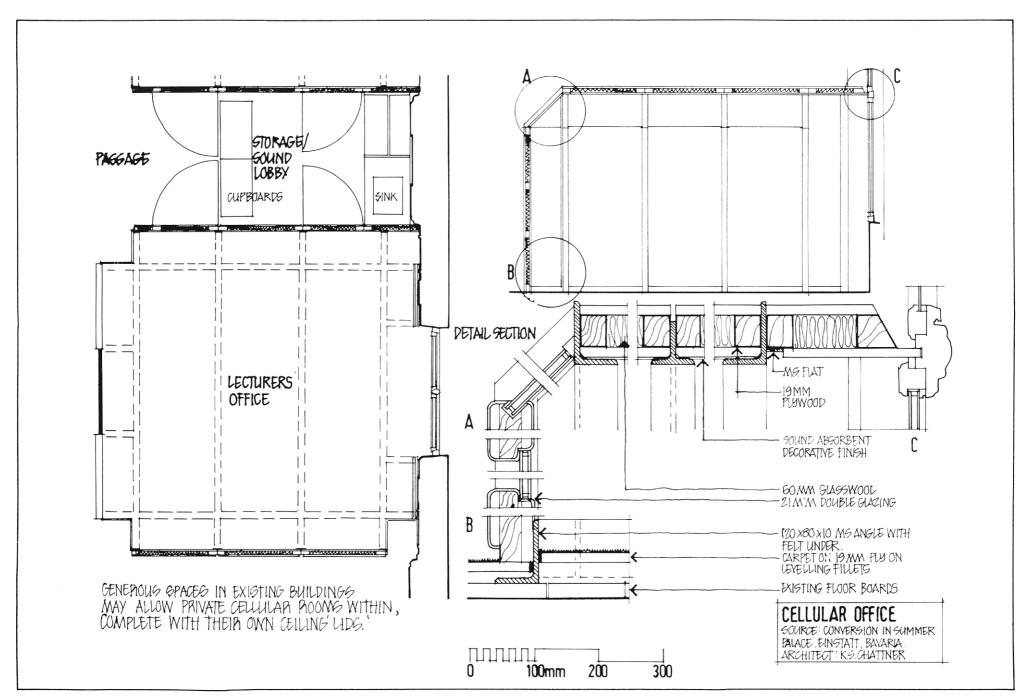


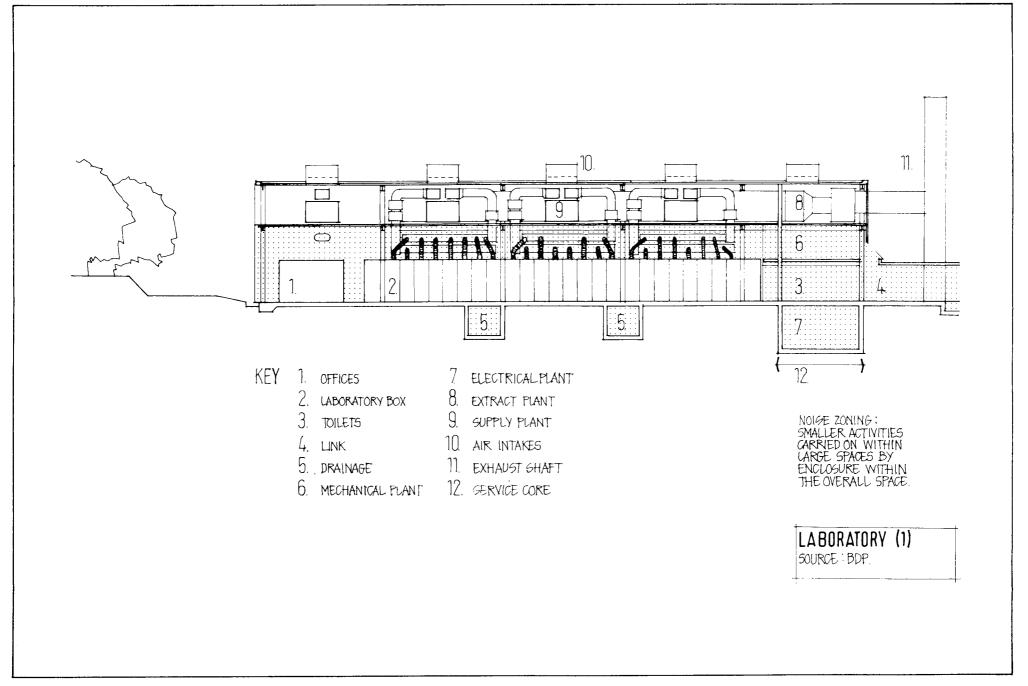


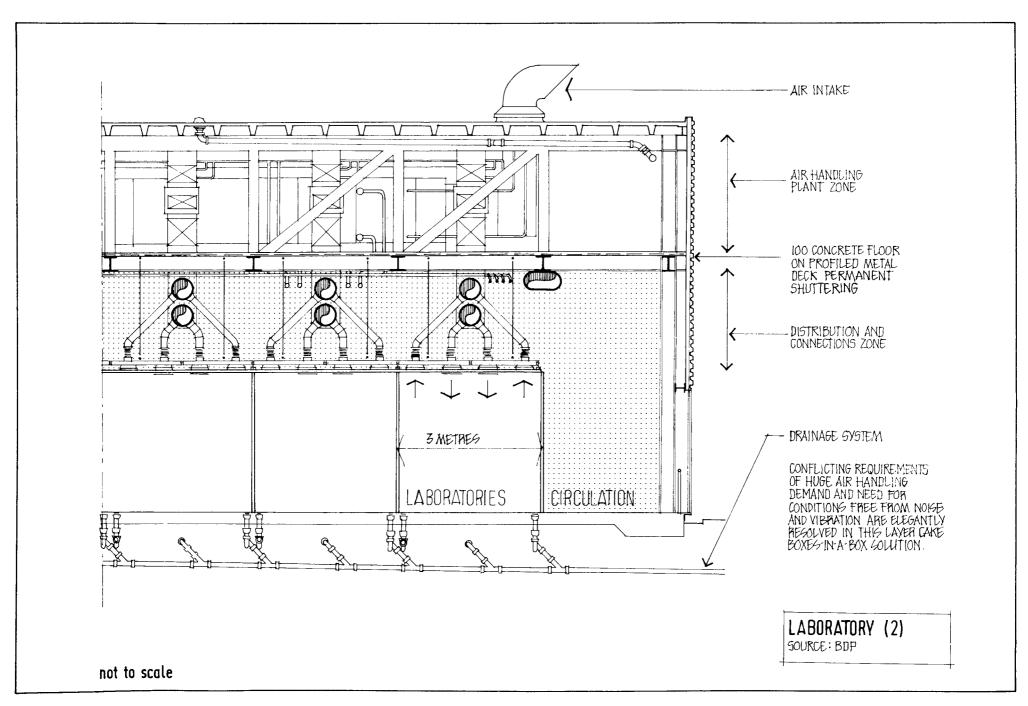
DESIGN GUIDE

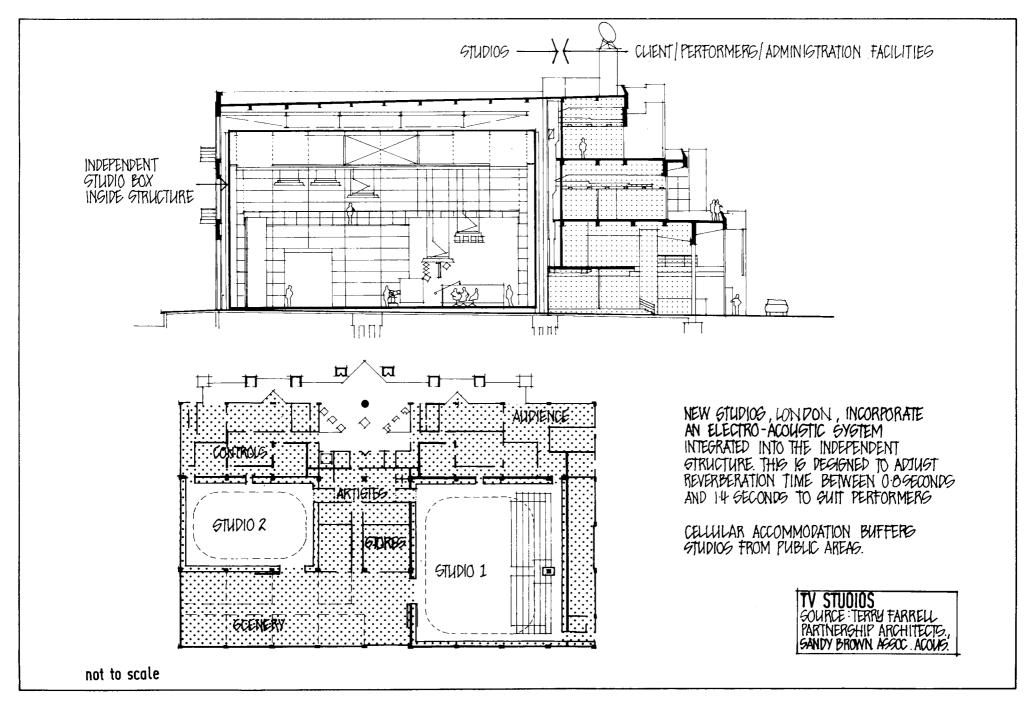
- 1. DESIGN IN A SPACE OVER 11 METRES WIDE.
- 2. PLAN 12M2/PERSON INCLUDING CIRCULATION
- 3. ZONE OFFICE MACHINES APART AND SCREEN.
- 4. DEVELOP 'ARENA' ORIENTATION LAYOUTS
- 5. CONTAIN BACKGROUND SOUND LEVEL WITHIN RANGE 40-50dBA
- $oldsymbol{6}$. DEVELOP GOOD SCREEN LAYOUTS AVOID SPOKEG AND CUBICLES.
- 7. LOCATE ACOUSTIC PANELS AROUND SOUND SOURCES TO BE CONTROLLED. WITHIN 1200.
- 8. DEGIGNATE 1/3 PANELS TO BE ACOUSTIC RATHER THAN HARD SURFACE.
- 9. CHOOSE HIGH (2100) PANELS WHERE WORKERS STAND OR CIRCULATE
- 10. CHOOSE A HIGH ABSORPTION CEILING
- 11. CHOOSE A THICK CARPET ON A DENSE UNDERLAY.
- 12. CONGIDER WHETHER MASKING BACKGROUND SOUND MAY BE NECESSARY
- 13. MINIMIGE NOIGE FROM IMPULSE OR INTERMITTENT GOURCES-TELEPHONES, TYPEWRITERS, VDUS.
- 14. CHECK FOR SPEECH PRIVACY: GOOD IF A LIGTENER SMETRES FROM A PERSON READING AT NORMAL CONVERSATIONAL LEVEL CAN ONLY UNDERSTAND 10% OF SPEECH (STANDARD SPEECH ARTICULATION TEST). INCREASE ABSORPTIVE SCREENS IF NECESSARY.
- 15. CHECK AT GENERAL OFFICE DEGINED MID TREQUENCY 0.70 GECONDS. EXECUTIVE OFFICES 0.5 GEC, OPEN PLAND 45.

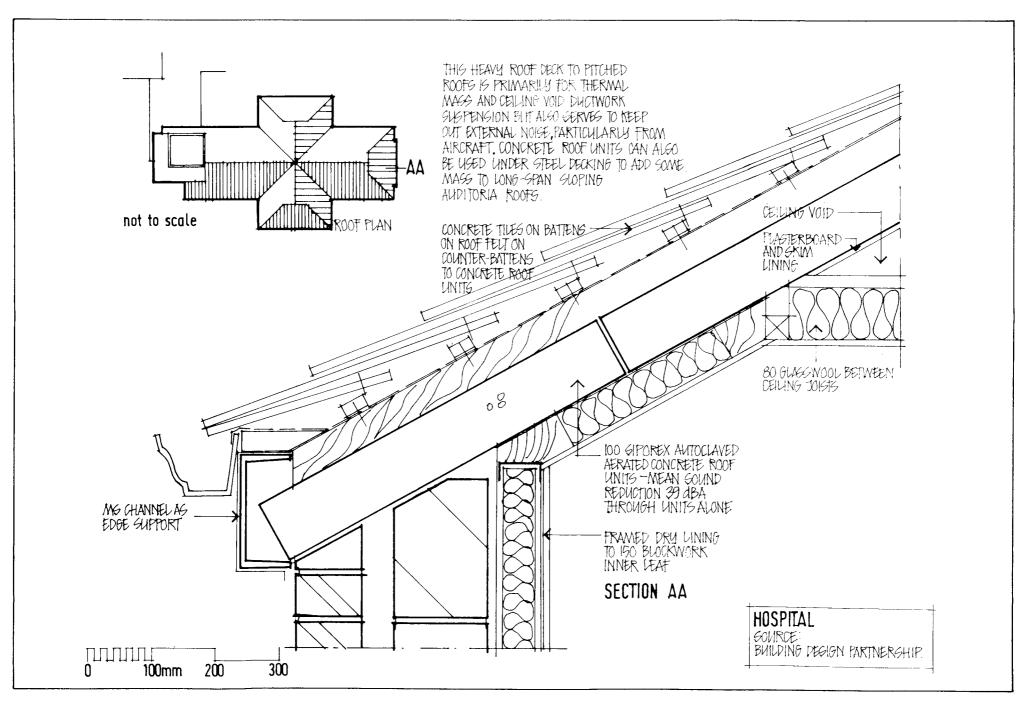
OPEN-PLAN OFFICES SOURCE: HERMAN MILLER REGEARCH CORPORATION.

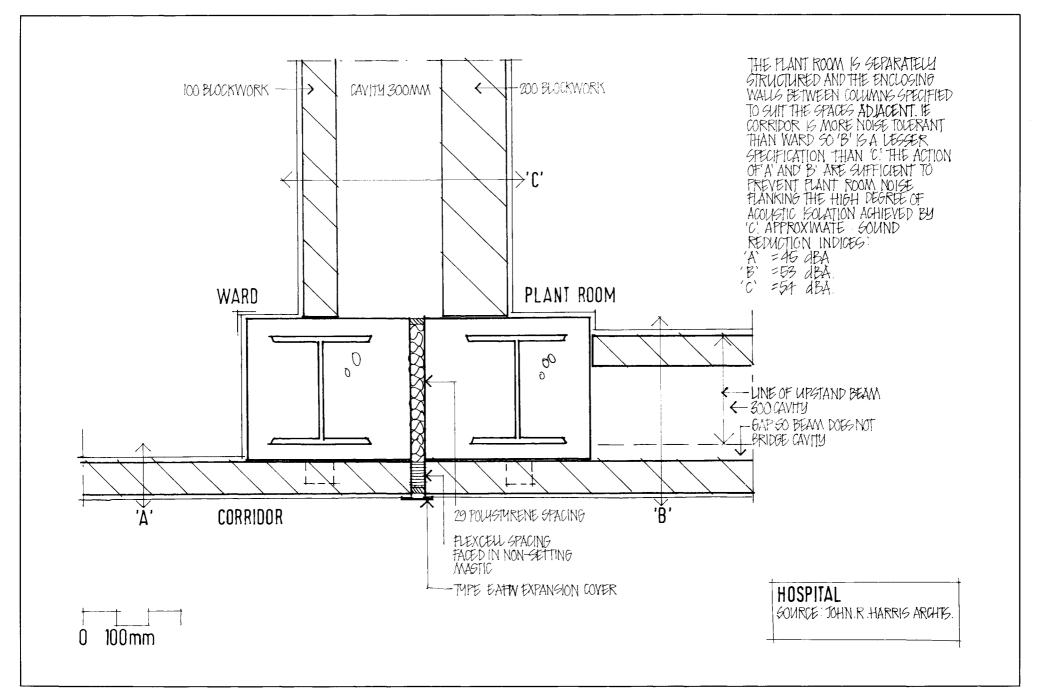


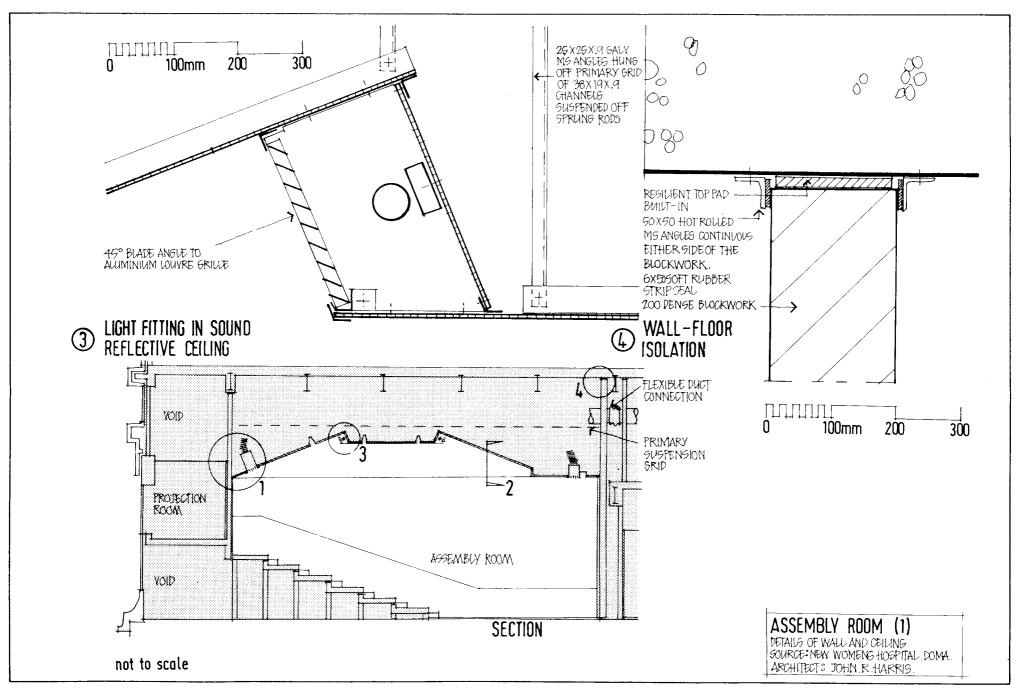


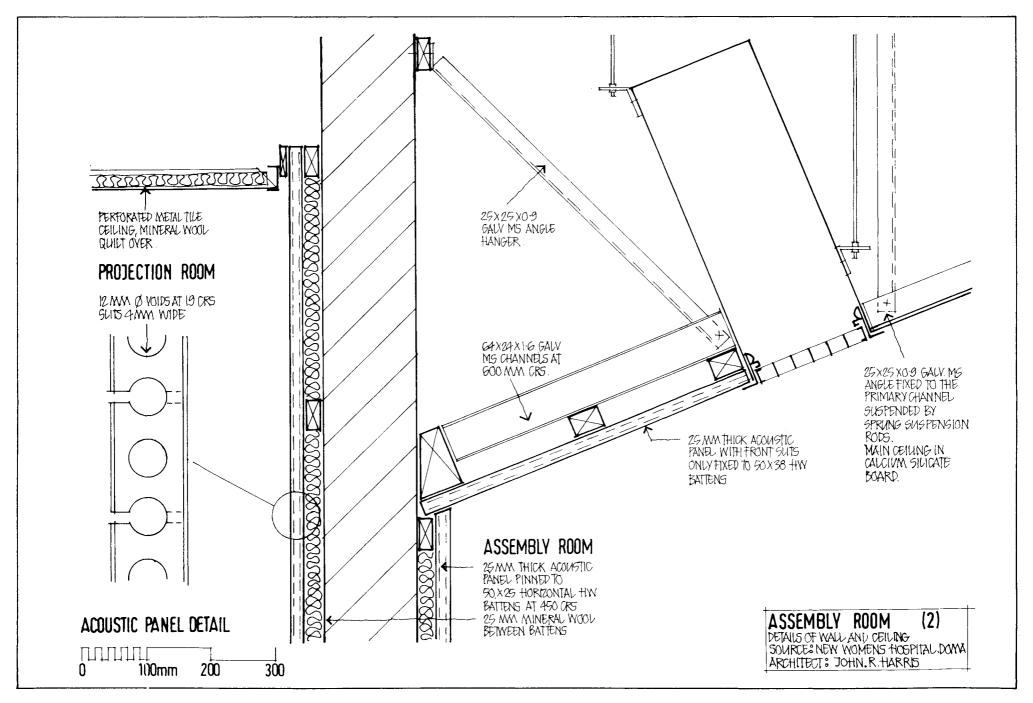


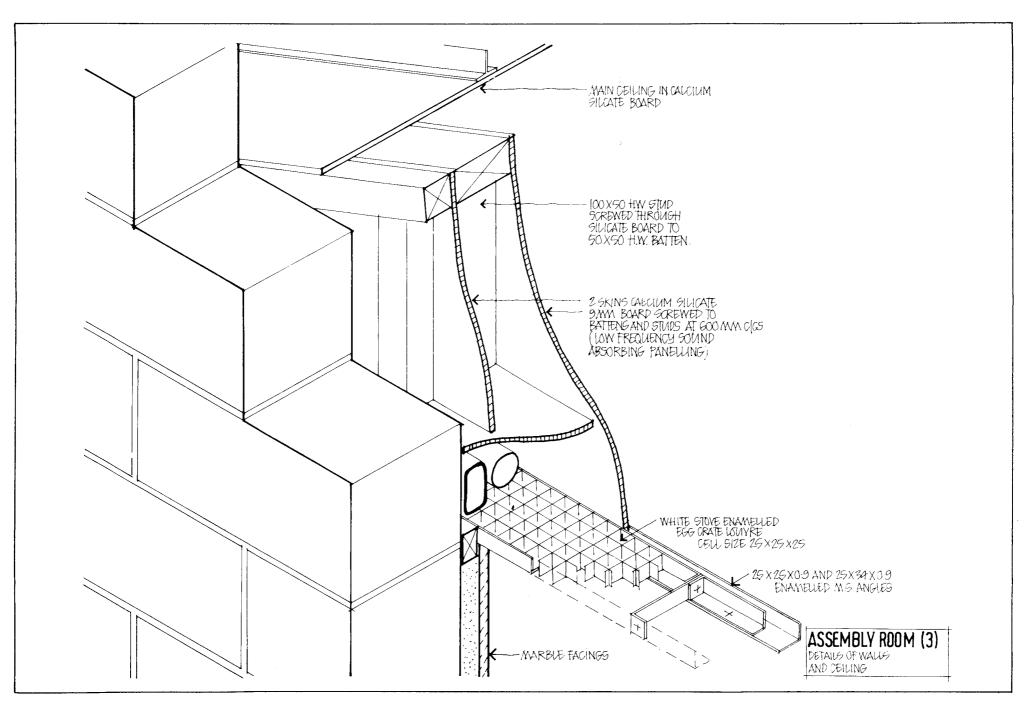


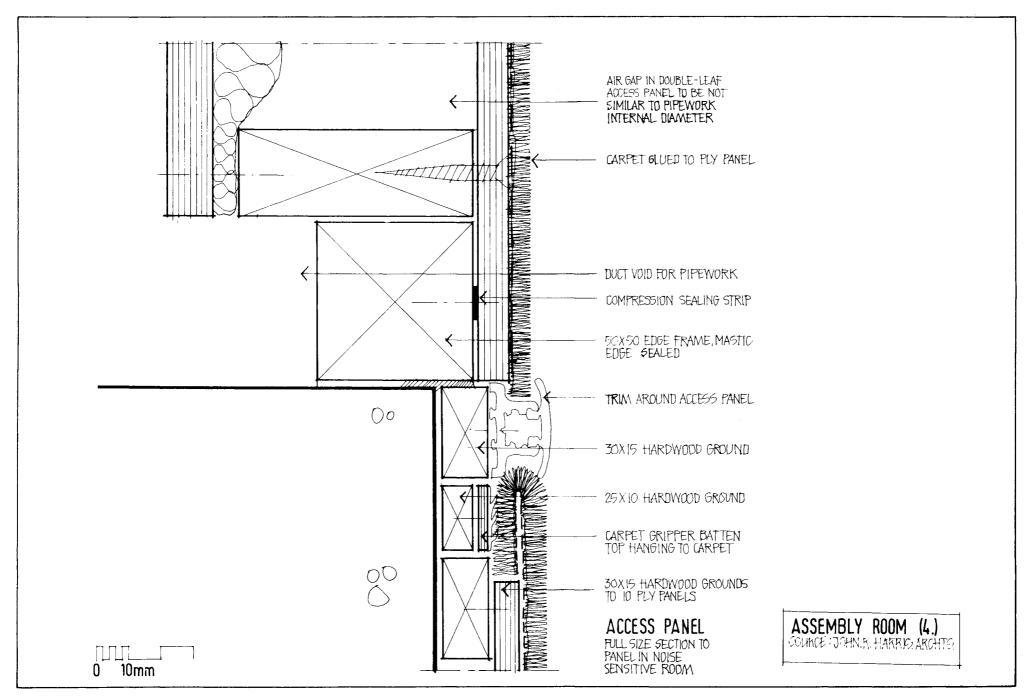


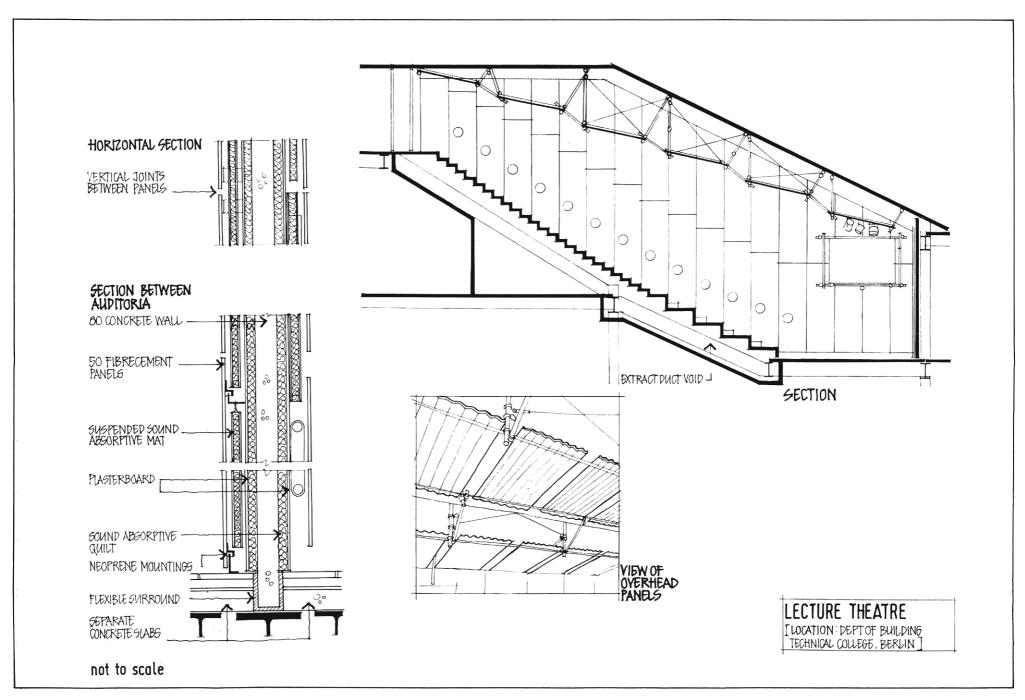


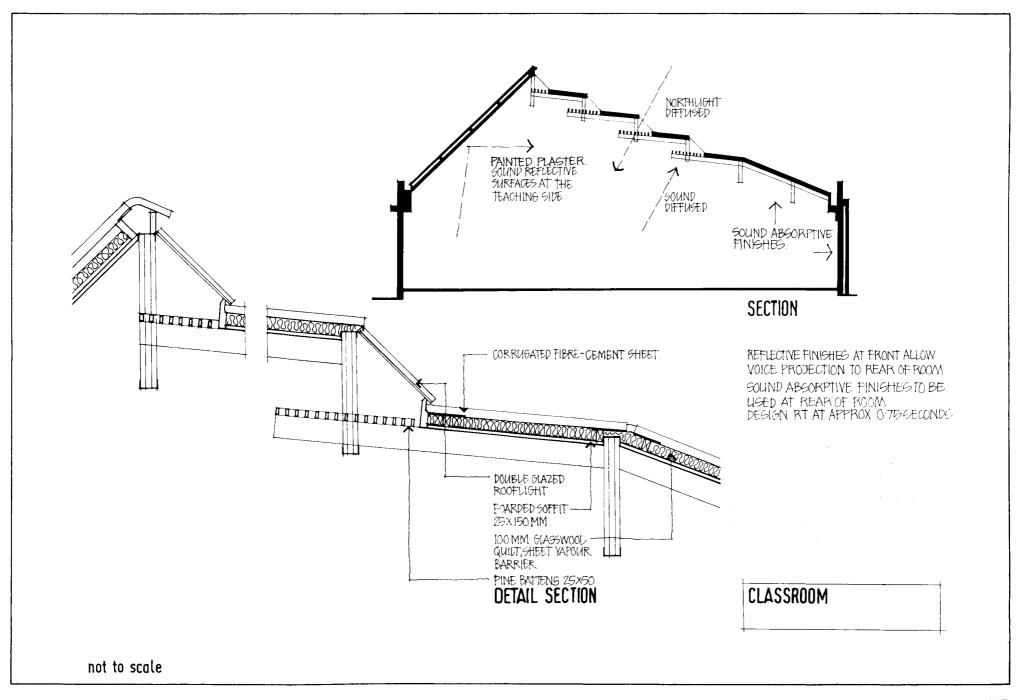


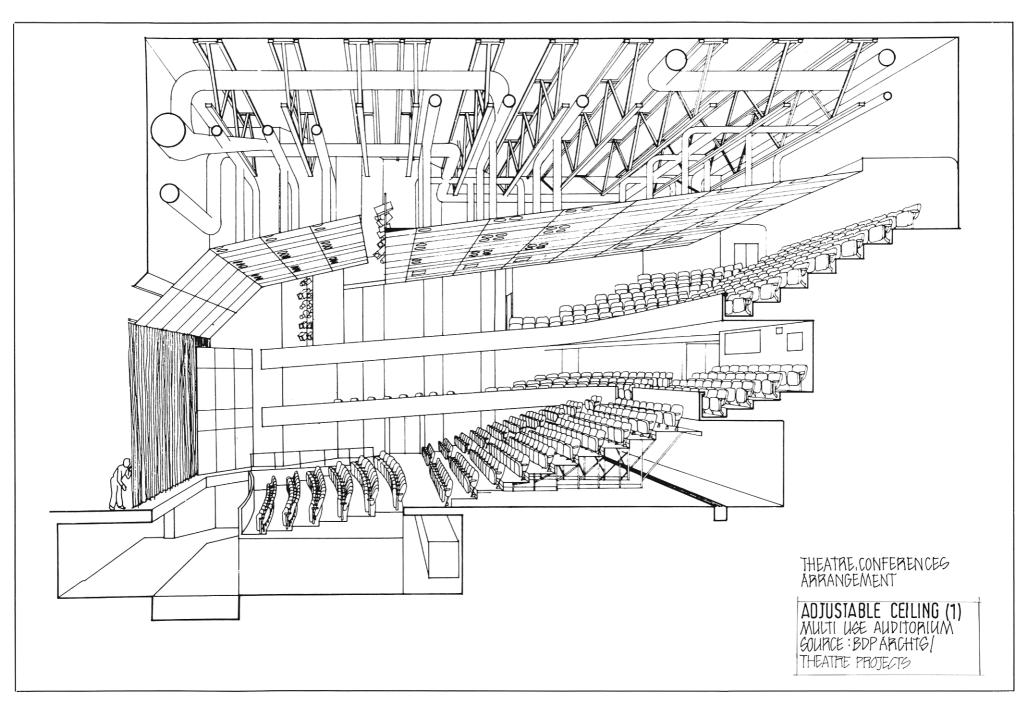


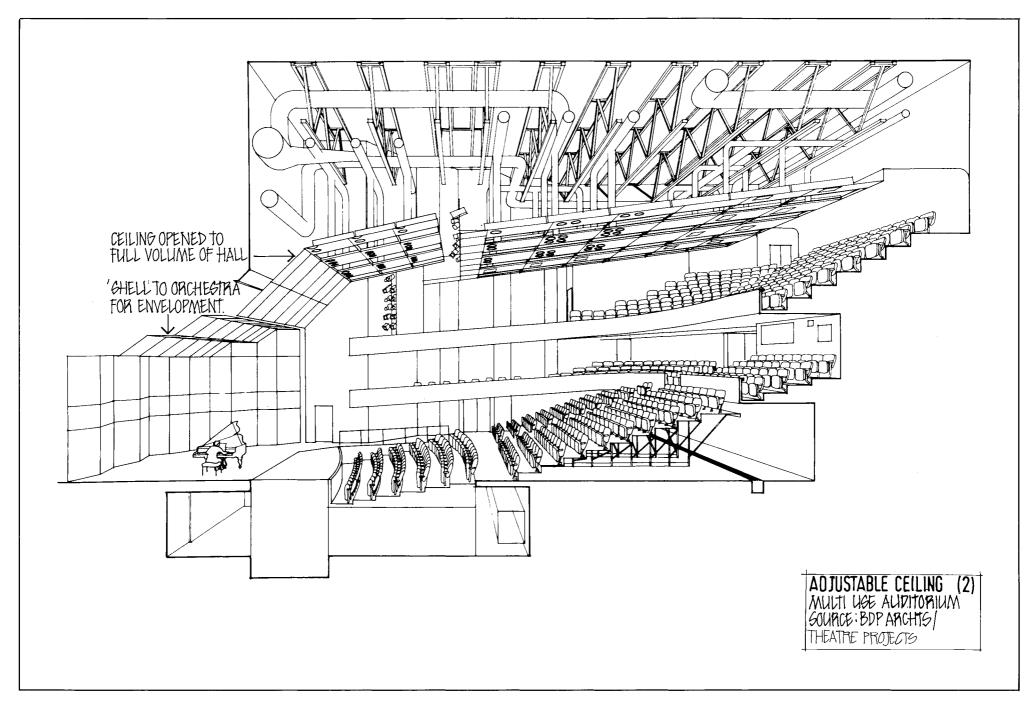


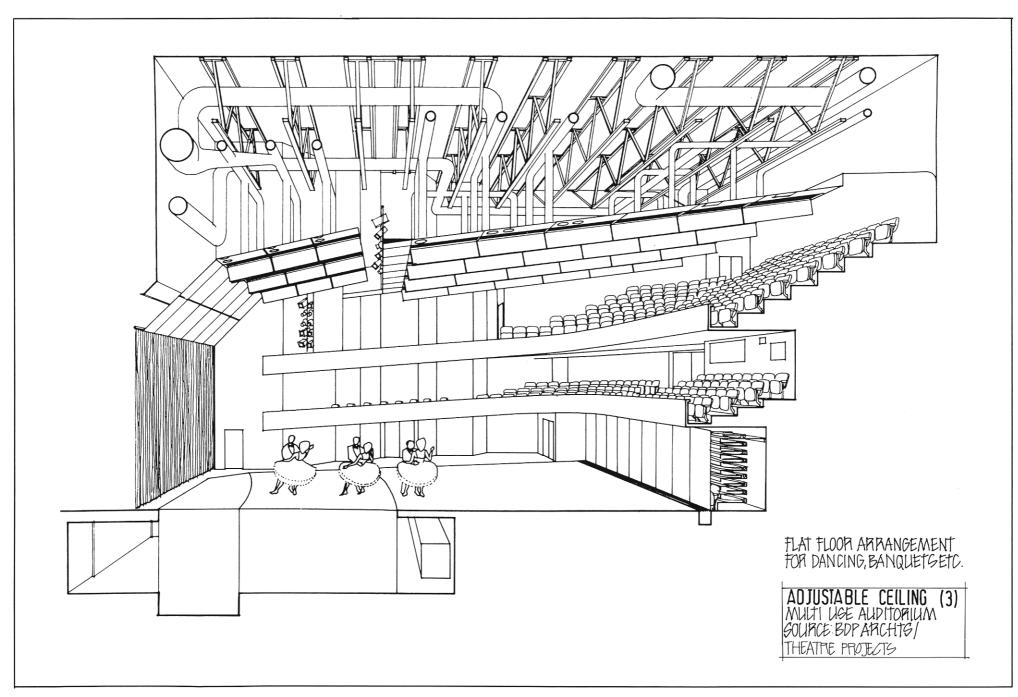


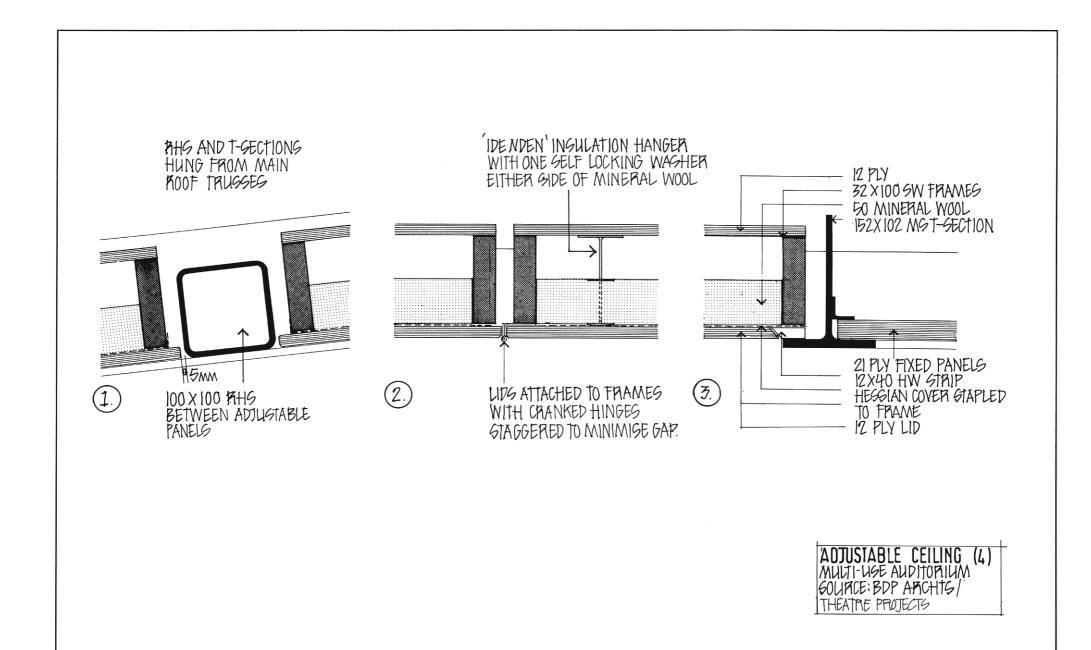


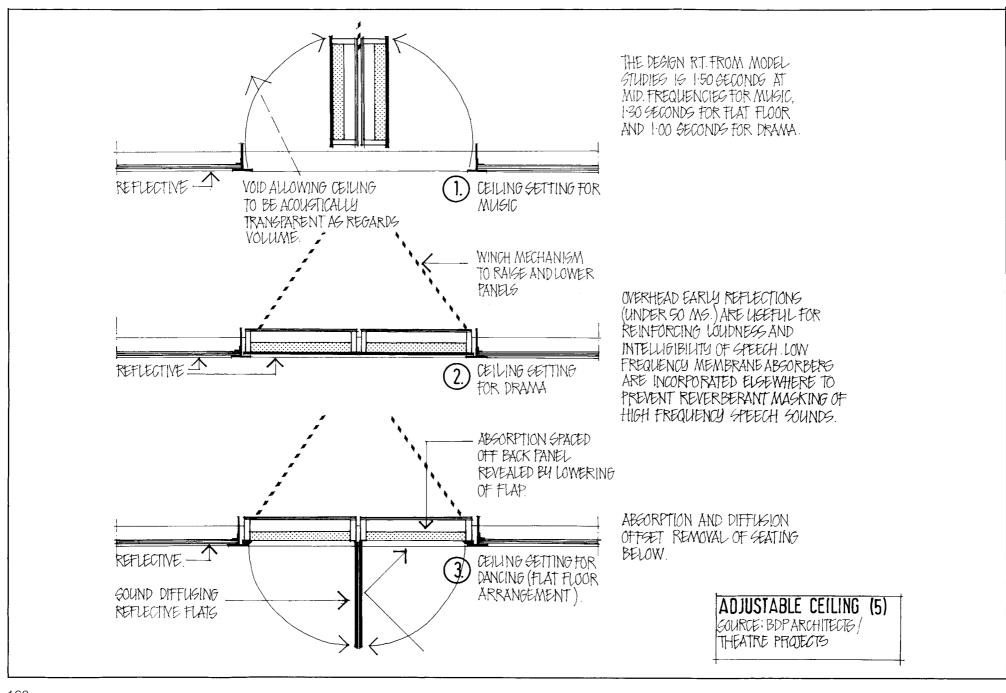


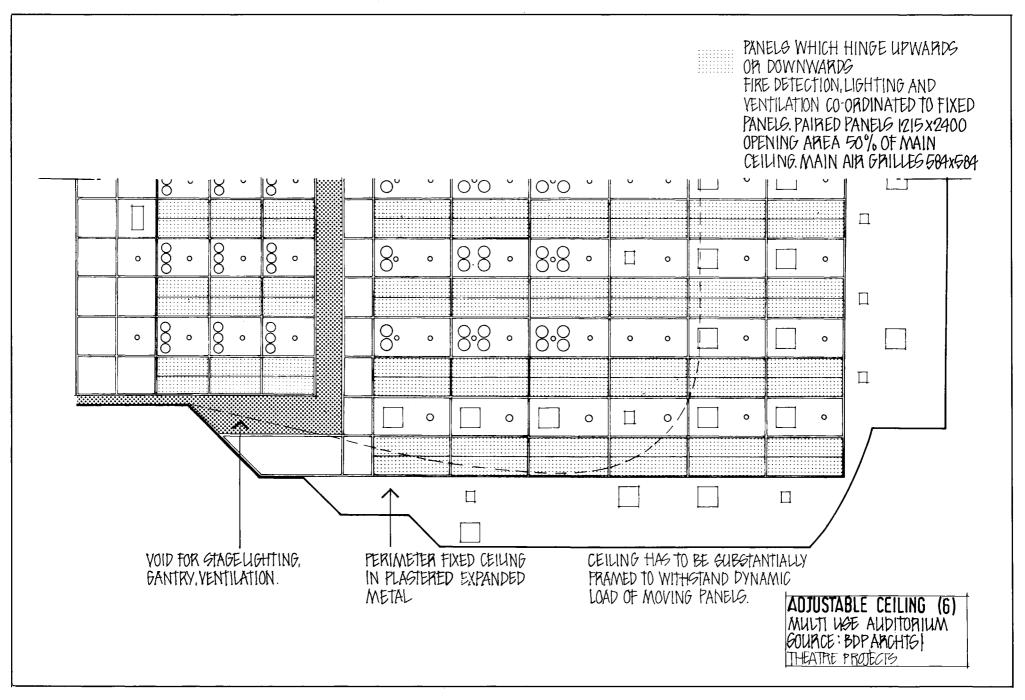


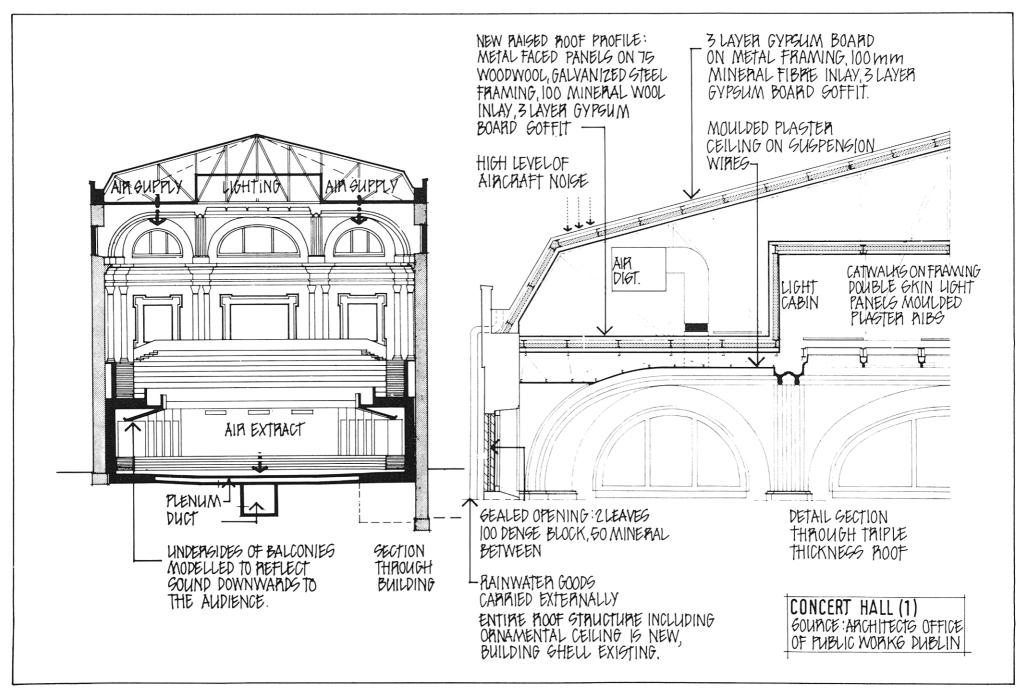


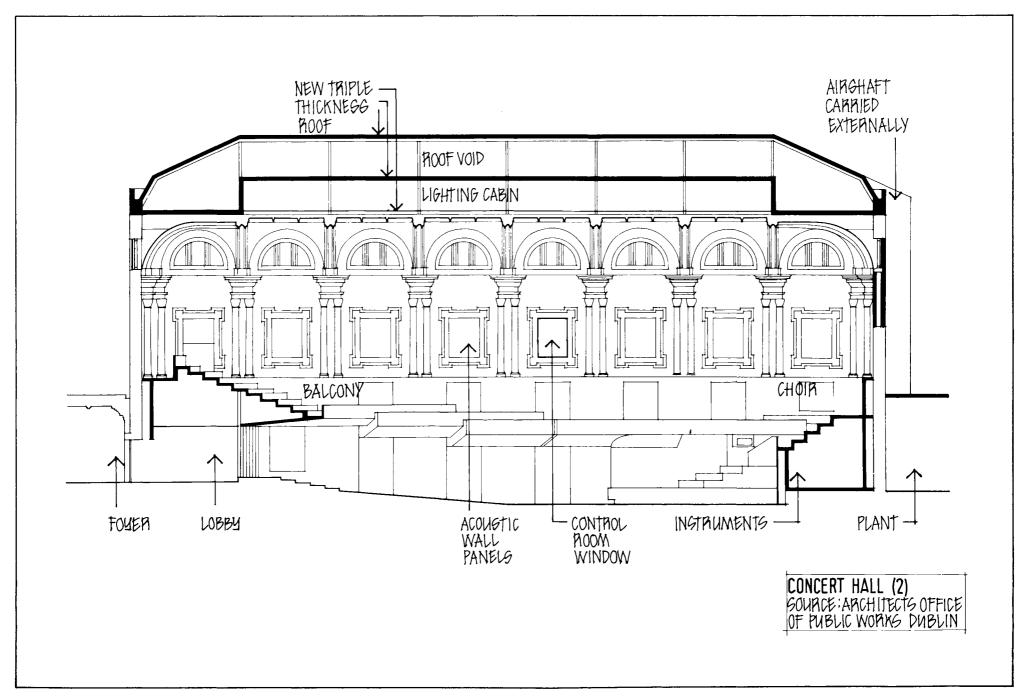


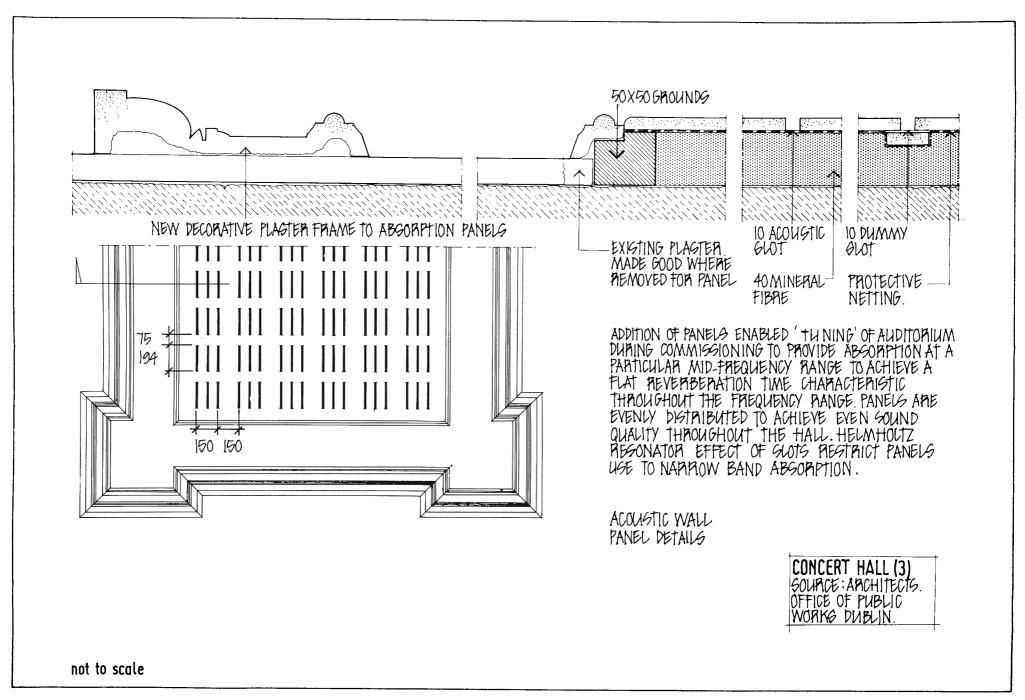


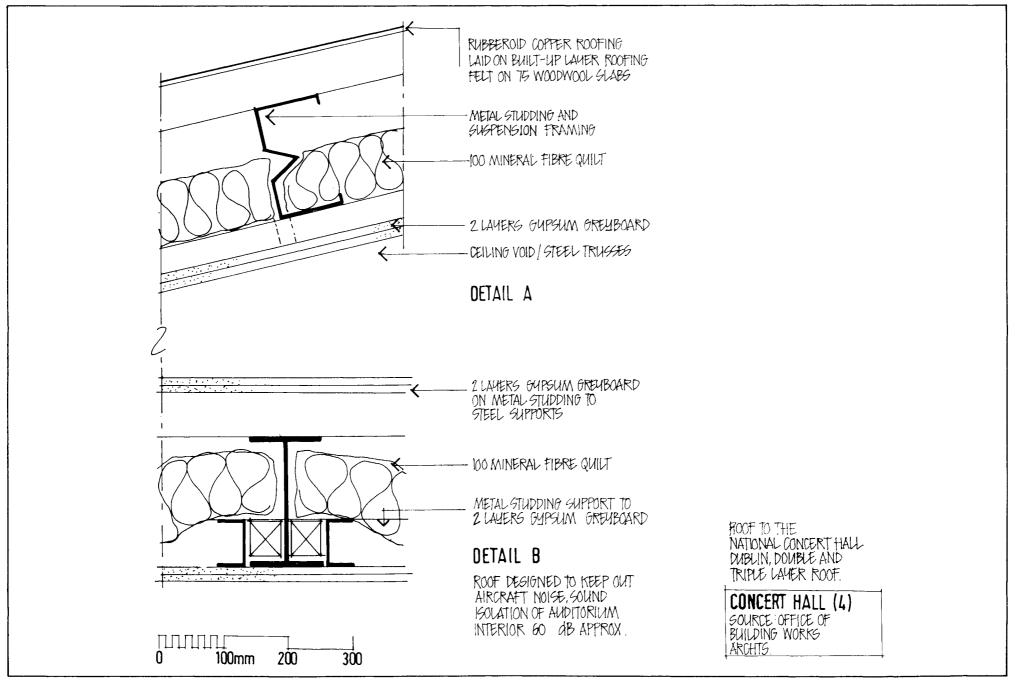


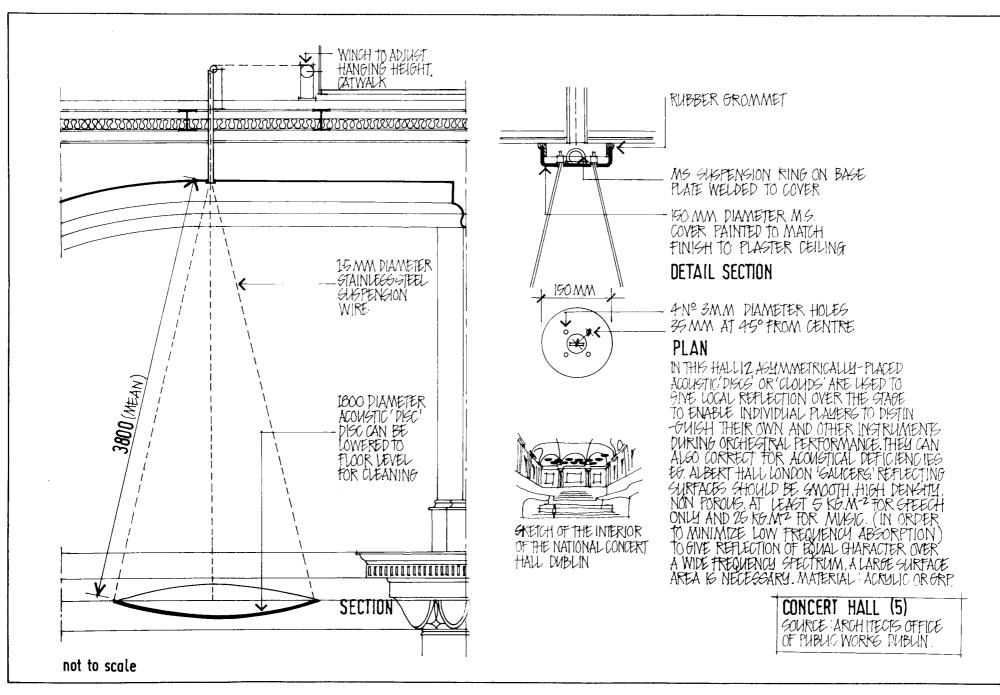


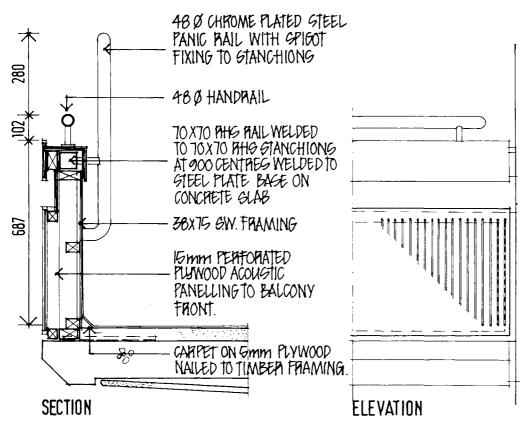


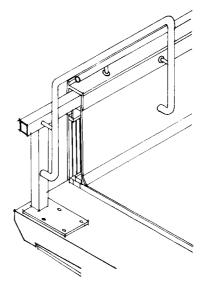












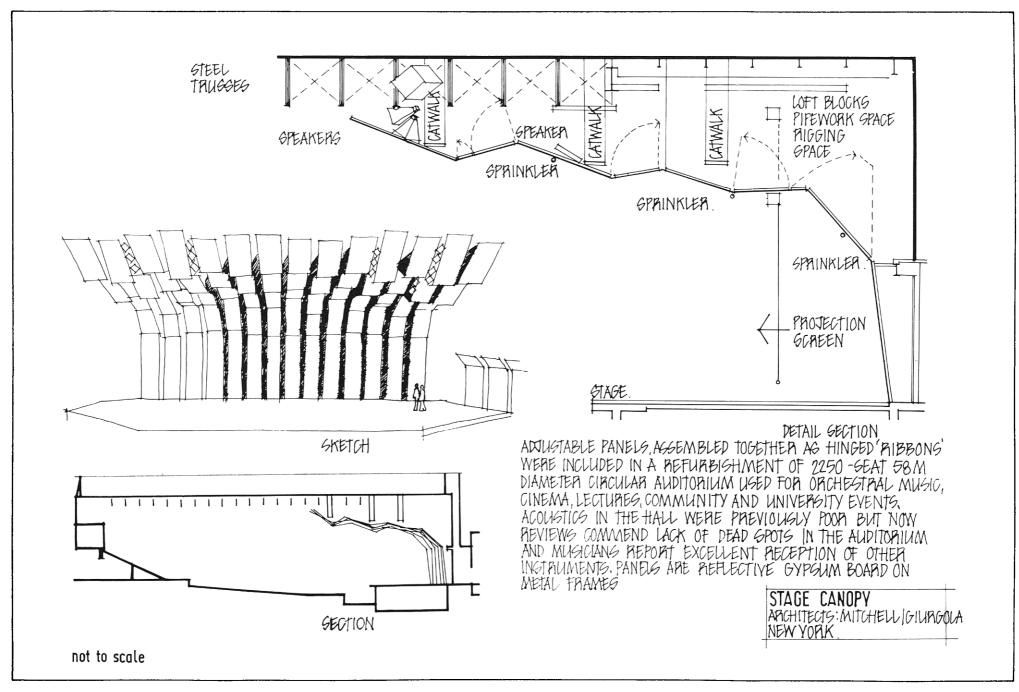
CUTAWAY AXONOMETRIC THEATRE ROYAL PLYMOUTH.

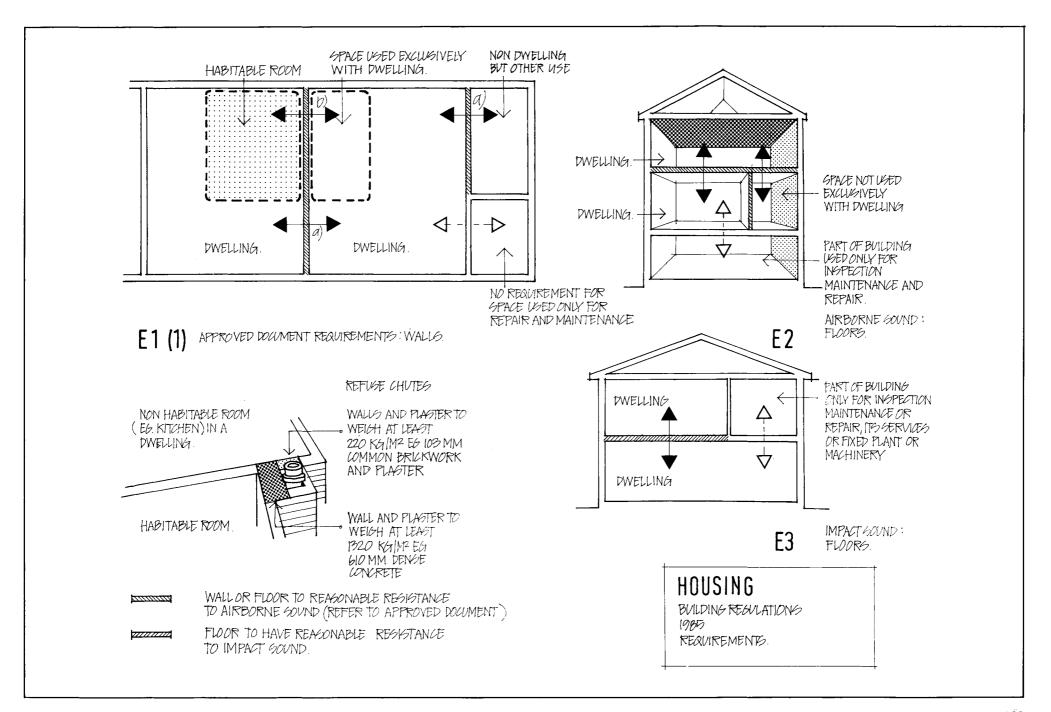
MANY AUDITORIA HAVE AS TUNING TO THE NATURAL ACOUSTICS ARISING FROM FINISHES AND SEATING SOUND ABSORBING PANELLING OR WALL LININGS, THE PANELS ABSORB SOUND WELL AT A SELECTED FREQUENCY PLANES, BY A COMBINATION OF HELMHOLTZ AND RESONATOR ACTION. WHERE ACOUSTIC PANELLING IS REQUIRED IN GRACES IT MAKES ECONOMIC GENCE FOR

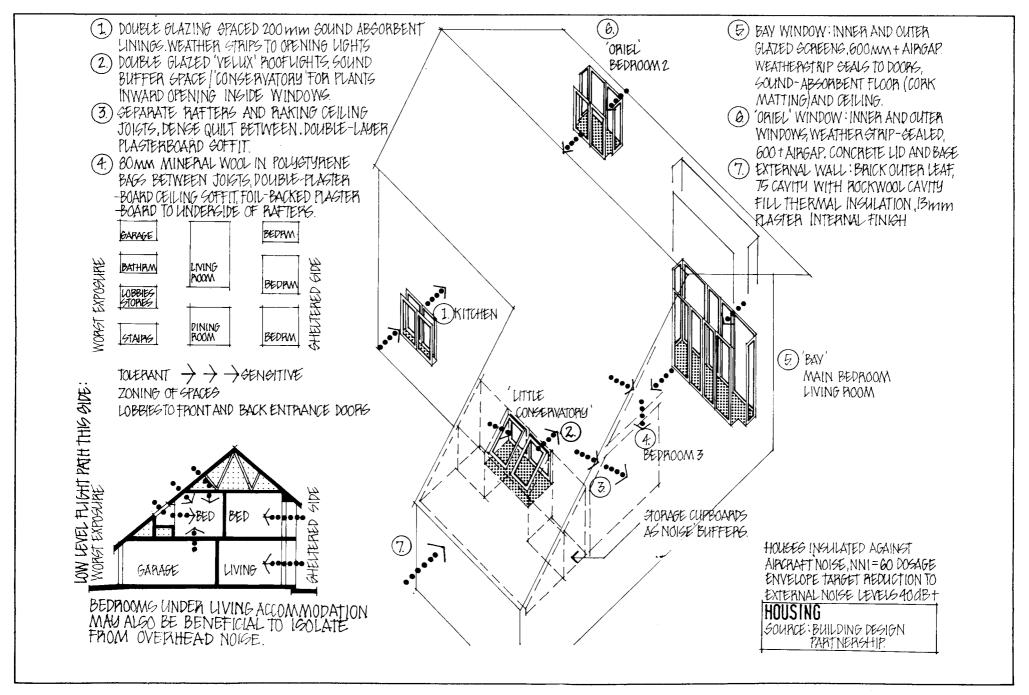
PANELLING IS REQUIRED IN GRACES IT MAKES ECONOMIC SENSE FOR IT TO BE BUILT IN AND FULFILL A USEFUL FUNCTION AS ILLUSTRATED RATHER THAN BEING HUNG ON A WALL AS AN AFTER THOUGHT.

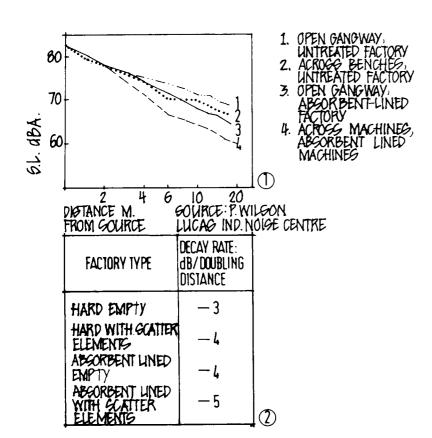
THEATRE BALCONY
GOURGE PETER MORO
PINROHIP ARCHTO

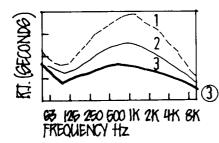
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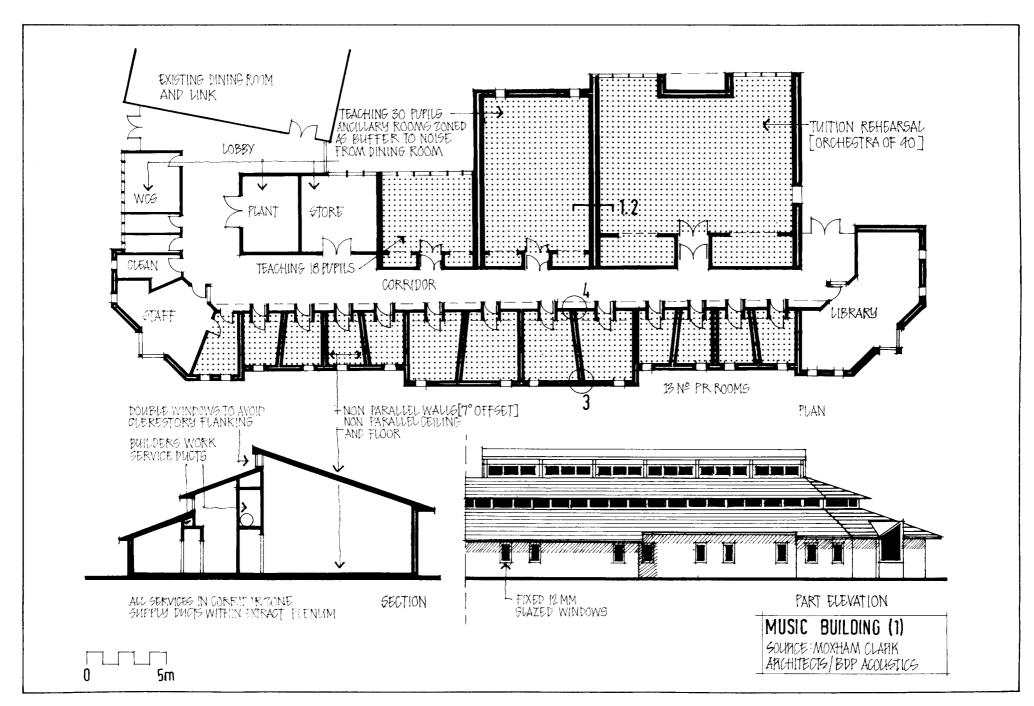


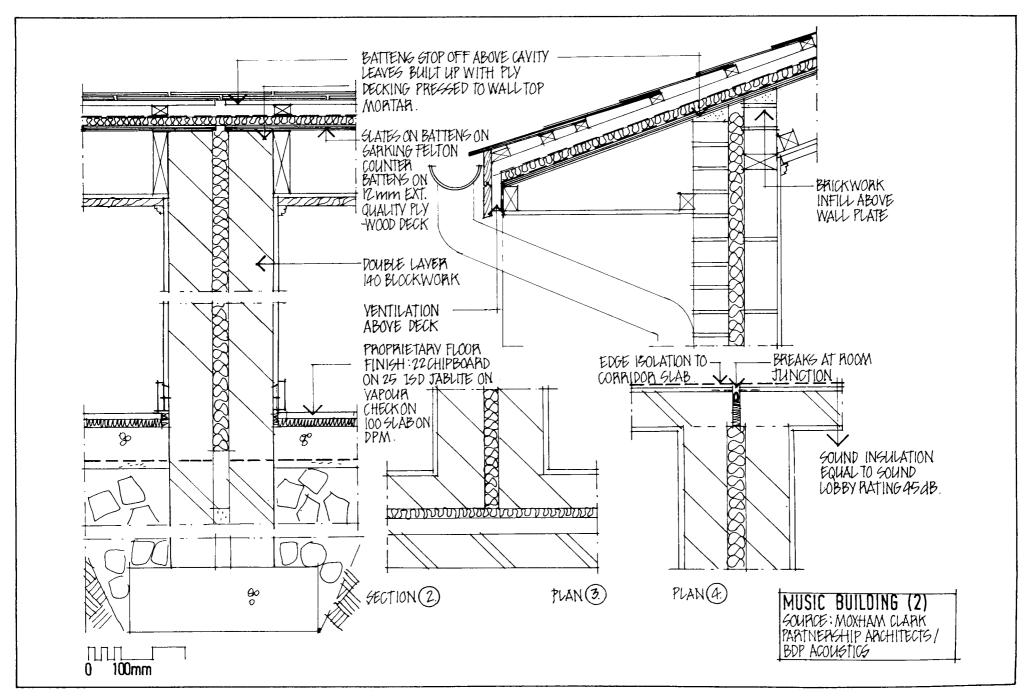
- 1. NO MACHINES 2. 25 MACHINES 3. 50 MACHINES
- FACTORY 45X43X43m HARD FINISHES BOUNCE: M.HODGSON LINNERGITY CAMBRIDGE

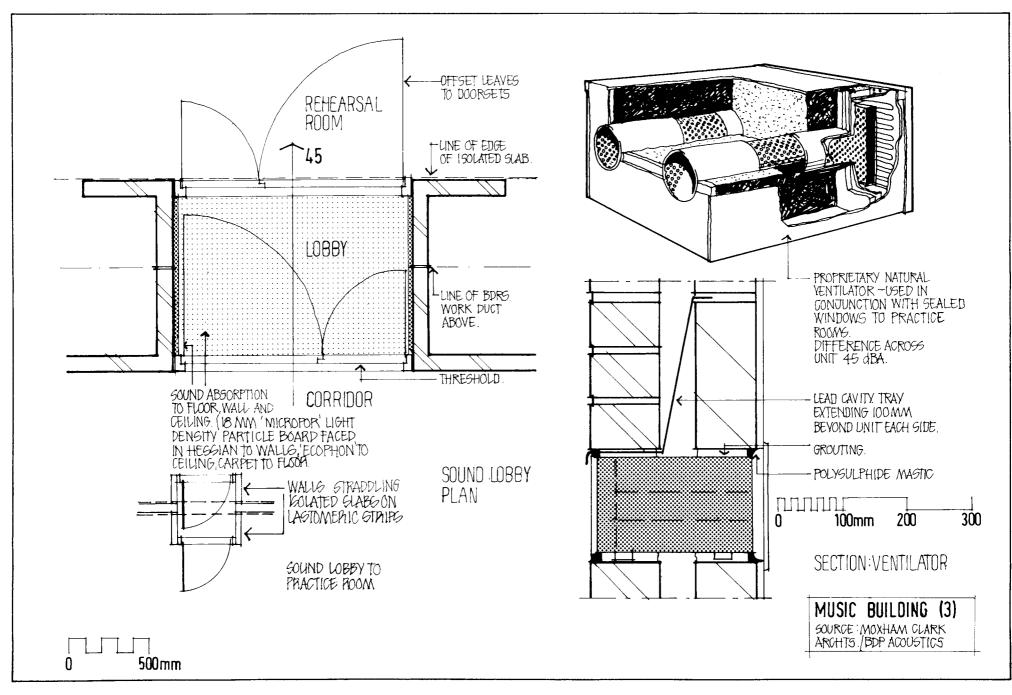
DESIGN GUIDE

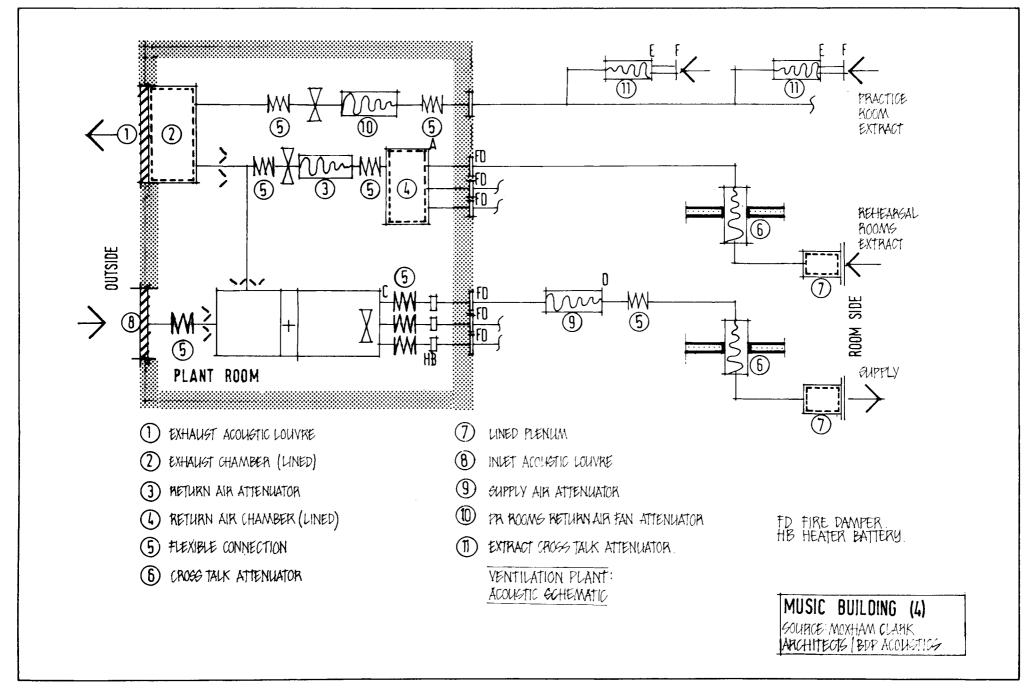
- I. WHERE EMPLOYEES EXPOSED TO) 8 HR LEQ. OF 90 dB (A), NOISE REDUCTION MEASURES TO BE TAKEN AS FAR AS REASONABLY PRACTICABLE, EAR DEFENDERS TO BE WORN.
- 2. CLASSICAL DEGCRIPTION OF SOUND IN ENCLOSURES (03. SABINE) NOT APPLICABLE. TENDENCY FOR ABBENCE OF CONSTANT REVERBERANT SOUND LEVEL OUTSIDE DIRECT SOUND FIELD OF SOURCES. THIS MEANS ABSORBENT TREATMENTS DO NOT NECESSARILY PRODUCE MARKED SOUND LEVEL REDUCTIONS IF REMOTE.
- 3. LACK OF REVERBERANT SOUND FIELD MEANS ZONING OF NOISY FROM QUIET PROCESSES AND LOCAL SCREENING ARE EFFECTIVE MEASURES
- 4. OVERHEAD GUOPENDED ABGORBERG COUPLED WITH LOCAL GCREENING ARE OFTEN THE BEST FORM OF INCORPORATING SOUND ABGORPTION.
- 5. OPERATOR EXPERIENCE OF NOISE IS NOT IMPROVED BY TREATMENT IN FACTORY GRACE—NO VARIATION IN DECAY RATE > 2 M. (1).
- 6. FOR DECAY RATE FROM AN OMNIDIRECTIONAL SOURCE IN A FACTORY SPACE, GUIDE LINES (2.) MAY BE CONGIDERED
- 7. MACHINERY AND PLANT THEMGELVES PROVIDE SIGNIFICANT SCATTER AND ABGORPTION (3.).
 - EEC PROPOSAL FOR COUNCIL DIRECTIVE (18 OCTOBER 1982): DAILY EXPOSURE MUST NOT EXCEED 85 dB(A) BUT TO TAKE ACCOUNT OF FEASIBILITY 5 YEARS ARE TO BE ALLOWED FOR IMPLEMENTATION

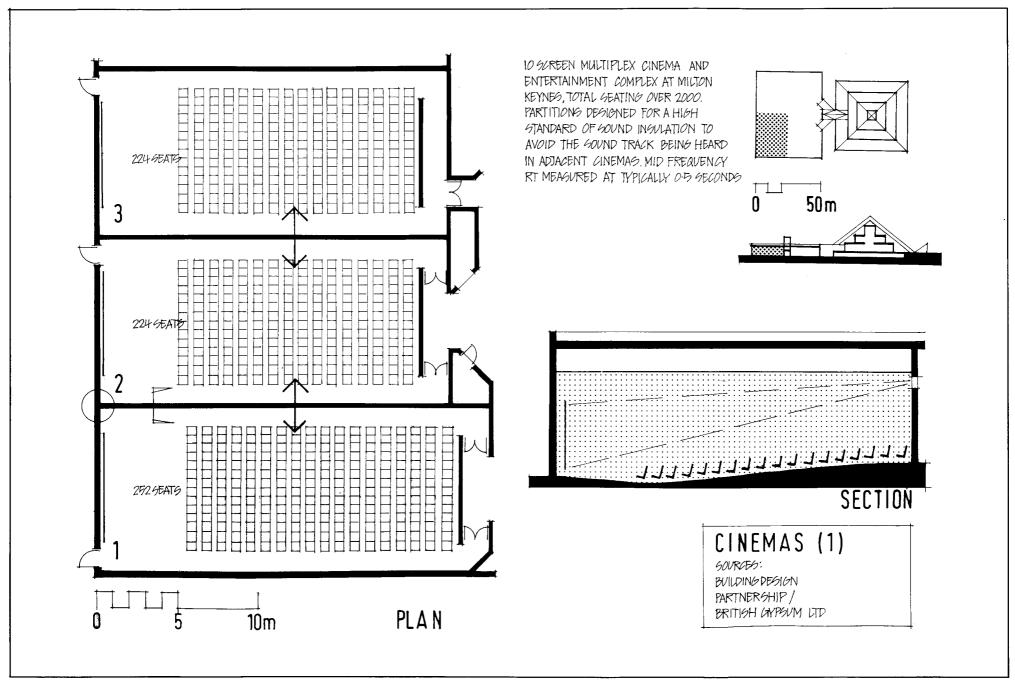
INDUSTRIAL BUILDINGS

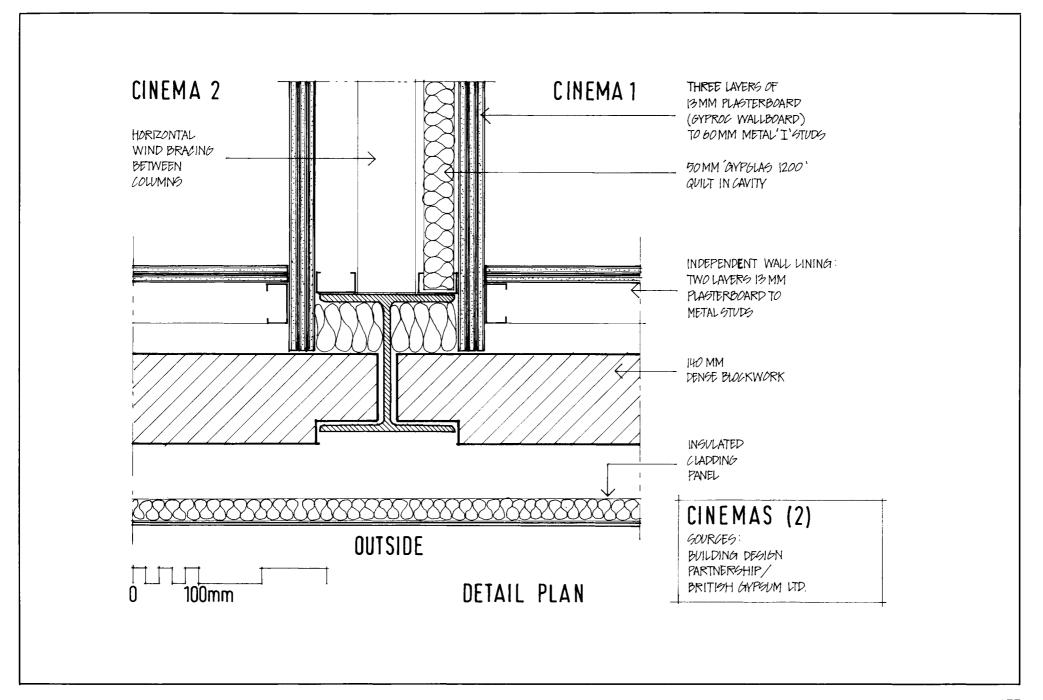


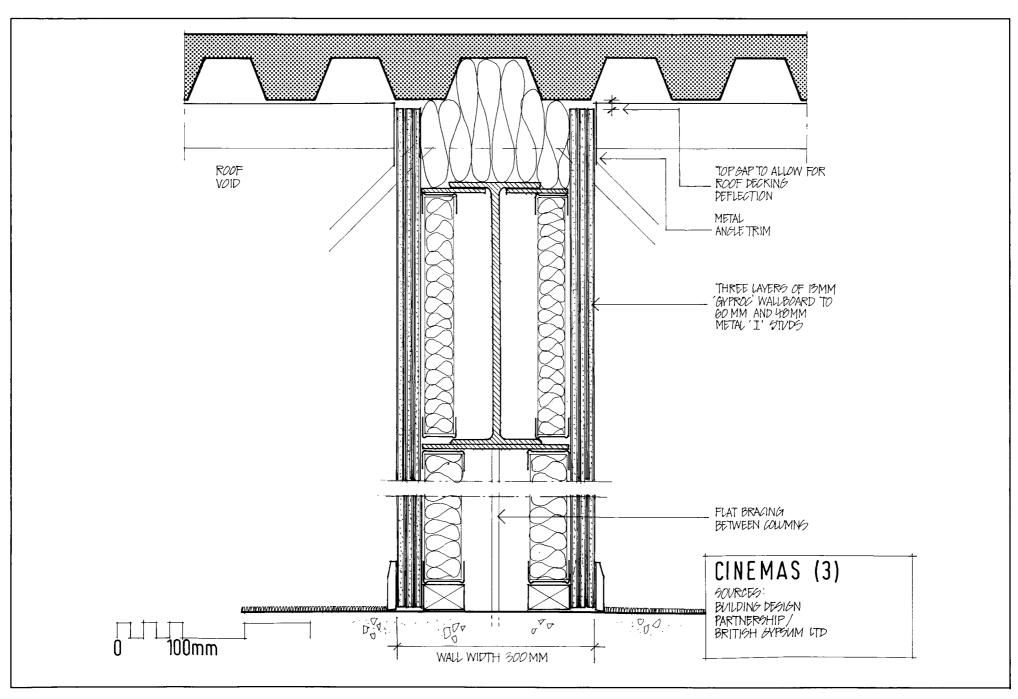


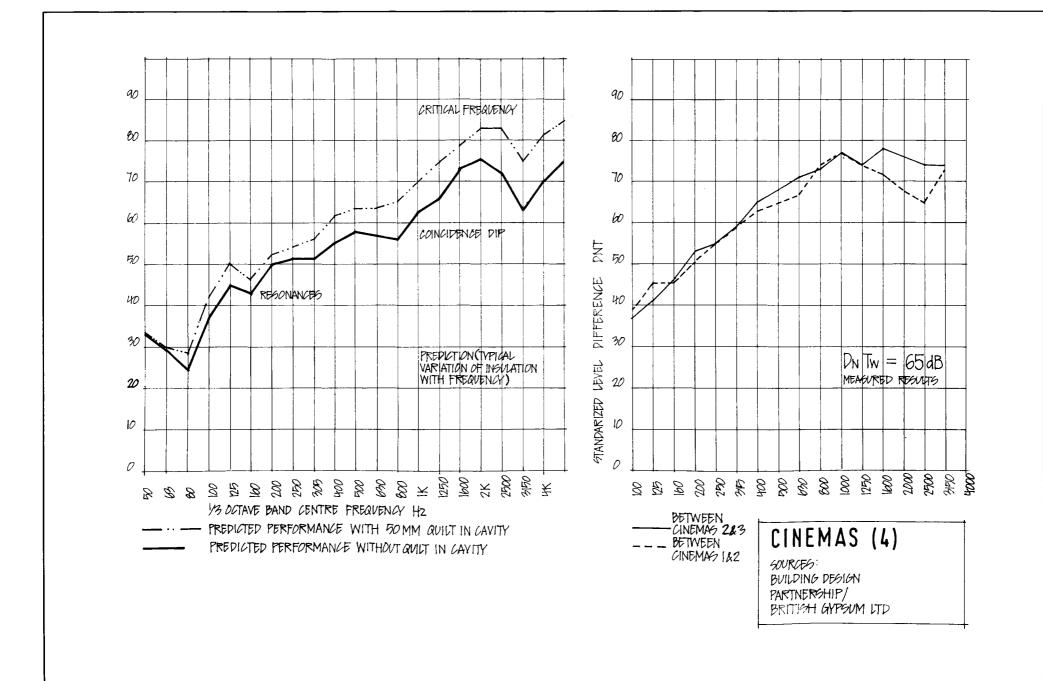


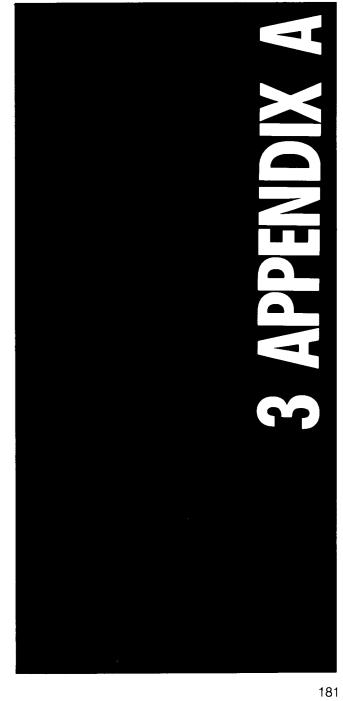




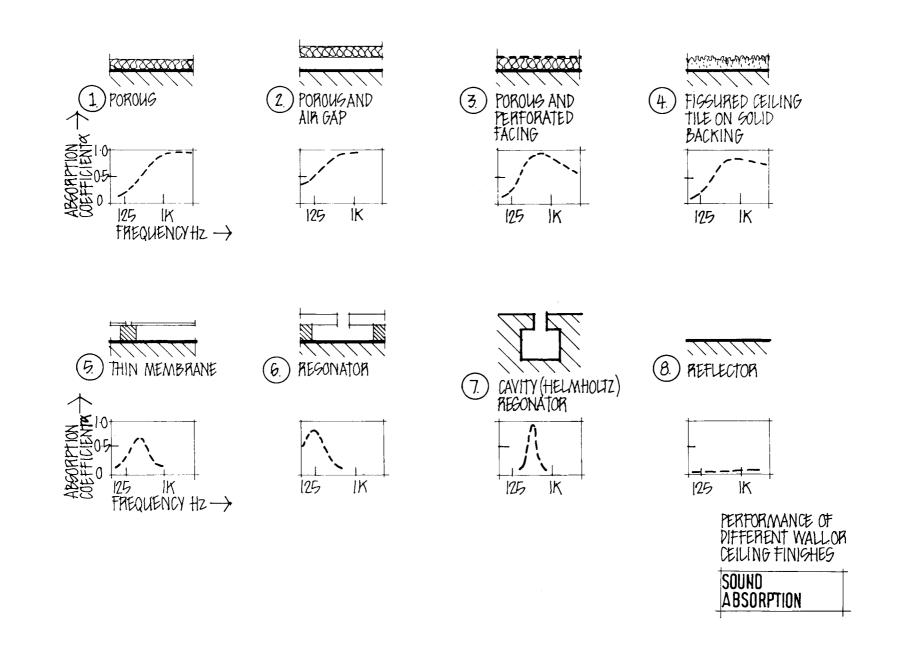


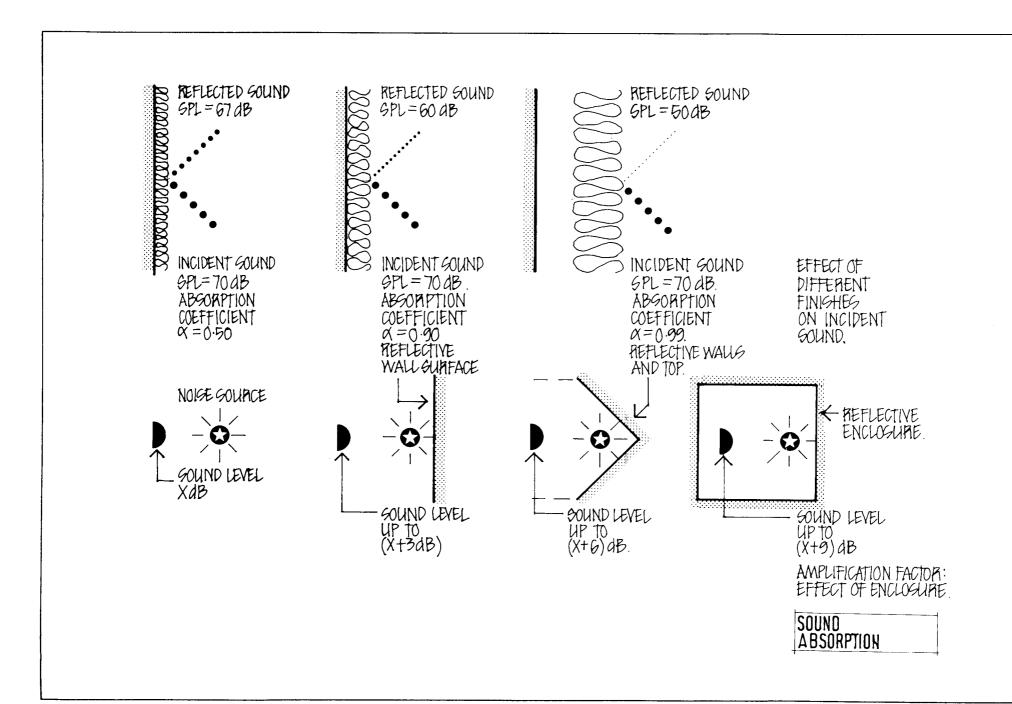




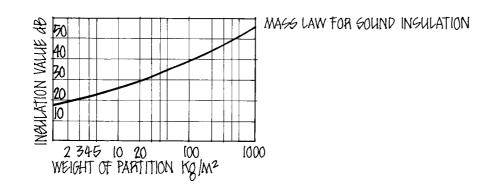


ABSORPTION SOUND

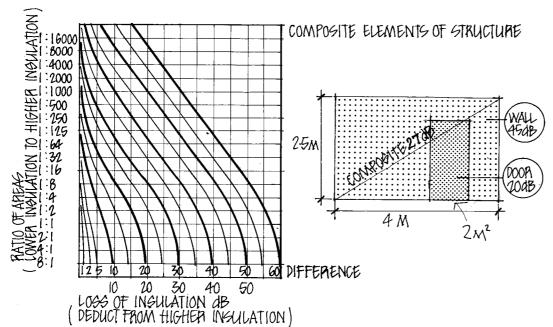




SOUND INSULATION

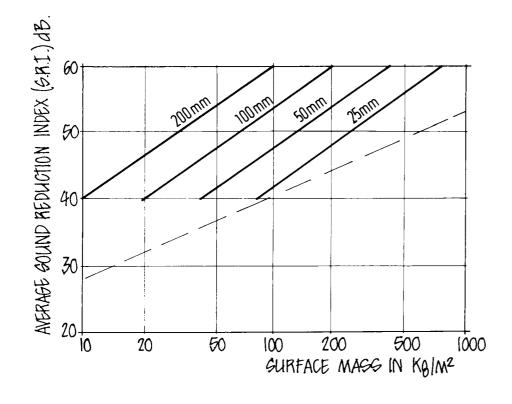


FOR SINGLE WALLS THE WEIGHT PER UNIT AREA IS AN INDICATION OF INSULATION VALUE ONLY. RESULTS BELOW MASS EXPECTATION MAY OCCUM BECAUSE OF: RESONANCE AND COINCIDENCE EFFECT; FLANKING; EDGE FIXING. COMPOSITE CONSTRUCTION OF A SEMIES OF LAYERS IMPROVES THE SOUND INSULATION ABOVE MASS LAW EXPECTATION AS DOBS. RESILIENT MOUNTING OF PANELS; DISCONTINUITY OF CONSTRUCTION; DOUBLE OR TRIPLE LAYERS WITH WIDE AIR SPACE. A HEAVY DIVIDING ELEMENT IS PARTICULARLY EFFECTIVE FOR LOW FREQUENCY SOUND.



THE COMPOSITE SOUND REDUCTION INDEX (ER.I.)
OF PARTITION BETWEEN 2 ROOMS, OR OUTSIDE
WALLS WITH WINDOWS IN A ROOM, CAN BE
OBTAINED FROM THE FIGURE AT LHS. AN EXAMPLE
OF THE EFFECT IS ALSO SHOWN AT LHS. A HOLE
IN A 10 SQ.M. 45 AB-RATED WALL OF 100 mm×100 mm
DOWN RATES THE COMPOSITE RATING TO 30 AB

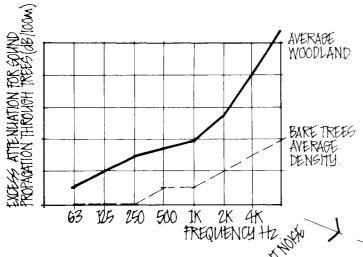
SOUND INSULATION SOURCE: PARKIN HUMPREYS AND COWELL



THE MAGG LAW FOR GINGLE WALLG HAG A CORRESPONDING EMPIRICAL RELATION OF BETWEEN GRI. AND WEIGHT PER UNIT AREA FOR DOUBLE LEAF PARTITIONS, AS WITH SINGLE WALLS, THESE CURVES ARE AN INDICATION ONLY BECAUSE THE G.R.I. WILL VARY WITH FREQUENCY.

SOUND INSULATION

EXTERNAL NOISE



PLANTING.

PLANTING IS OF SOME BENEFIT FOR HIGH FREQUENCY ATTENUATION BUT OTHERWISE OF LIMITED USE IN SCREENING, SAY, TRAFFIC NOISE COMPARED WITH MOUNDING

NOIGE LEVEL AT FRONT R1 = X

R2 = X - 6dBNOISE LEYEL AT SIDES

R3 = X-64B

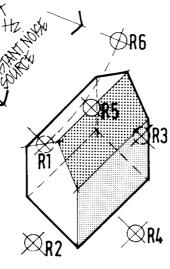
NOISE LEVEL AT REAR R4=X-10dB

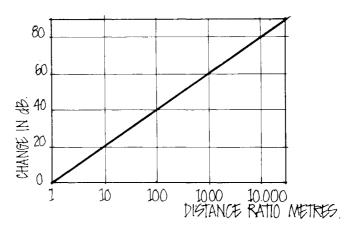
NOISE LEVEL AT ROOF

R5 = X-3 dB **R6**=X-2:5dB

NOKE LEYEL WITH NO BUILD UP RESULTING

FROM WALL BEHIND





DISTANCE

THE MAIN FACTOR AFFECTING REDUCTION OF NOISE LEVEL WITH DISTANCE IS THE SPREAD OF ENERGY, DOUBLING DISTANCE TENDS TO CAUSE A REDUCTION OF 6 dB. OTHER FACTORS AFFECT THE REDUCTION WIND FOO, SNOW AND RAIN FOR A LINEAR NOISE SOURCE LIKE TRAFFIC, THE REDUCTION WITH DISTANCE IS MUCH LESS-3 AB | DO UBLING

BUILDINGS

BUILDINGS AND WALLS AFFECT SOUND LEVELS LOCALLY, SO LOCATING ROOMS AND WINDOWS TO MORE SHELTERED ELEVATIONS WILL GIVE USEFULLY LOWER INTRUSIVE NOISE CEVELS WITHIN.

EXTERNAL NOISE

DEFINITIONS

Absorption

The ability of a material to absorb sound is measured by its 'absorption coefficient' α which is defined as the fraction of energy incident on its surface which is not reflected. The higher the decimal fraction value, the better the absorptive property of the material. This does not imply that some of the energy does not continue on through the material. The absorption A of a surface of area S is then given by:

 $A = S \alpha$ · · · ·

and if there are several absorbing surfaces of areas, S_1 , S_2 , S_3 etc. the total absorption A_T is obtained by:

 $A_T = \alpha_1 S_1 + \alpha_2 S_2 + \alpha_3 S_3$

There are different types of absorber: porous absorbers where the sound energy falling on them is dissipated by viscous losses within the pores of the material, and resonant absorbers. Resonant absorbers themselves are grouped into those on the Helmholtz resonator principle, an example of which is a perforated panel separated from a solid backing containing some porous absorbent, and membrane resonators, where a solid panel is spaced off a solid backing but by virtue of panel flexibility and its thickness (less than 20 mm) vibrates on the trapped layer of air. For Helmholtz resonators, the frequency at which maximum absorption takes place is a function of the thickness of the panel, the area of the perforations and the spacing behind the panel. For membrane resonators, the frequency at which maximum absorption occurs depends on the spacing panel to backing, the superficial weight of the panel and whether the panel-backing cavity has any porous absorbent within. Both types of resonant absorber are used for low-frequency absorption, and combination of the two types is possible.

Acoustic, Acoustical

The adjectives are almost interchangeable in use. Acoustic tends to apply in describing the basic property of the sense of hearing. Acoustical is used to describe devices or personnel in the field of acoustics.

Acoustics

The science of sound (from the Greek, akouo, to hear).

Acoustical treatment

The application of design principles in architectural acoustics to isolate noise or vibration and to correct acoustical faults in spaces by addition of absorption, reflectors or other devices.

Ambient noise

Background or general noise level-characteristic of an area, often used in comparison with a specific noise source overlay. Sound pressure level in dBA exceeded for 90% of the time (L_{90}). Ambient noise control may be by use of rating curves—see text.

Assisted resonance

An electronic method of lengthening the reverberation time of a hall by means of a series of channels each consisting of a microphone mounted in a tuned resonator in the ceiling feeding on an amplifier connected to a loudspeaker also in the ceiling.

Brilliance

.

Attribute of a hall with clear sound, prominent in treble, rich in harmonics.

Clarity (Deutlichkeit)

Defined as 10 log (energy over first 80 milliseconds expressed as a fraction of the remaining energy). The degree of clarity in sound reception depends on the strong receipt of direct rather than reverberant sound.

Coincidence

This occurs when the wavelength of the incident sound wave projected onto a partition or panel matches the bending wavelength of the partition or panel.

Critical frequency

Lowest frequency when coincidence occurs. Critical frequency is raised for thinner and less stiff surfaces in the sound path.

Decibel

Sound pressure level is the usual characteristic expressed in decibels. The scale is based on 10 times \log_{10} of the relative intensity of a sound and a

reference pressure. 'dBA' is a decibel unit with an 'A' weighting applied. This weighting has reduced response to extremes of frequency in order to simulate the response of the human ear.

Definition

Ratio of useful energy arriving within the first 50 milliseconds to total energy comprising signal; high figure means good definition.

Diffraction

Ability of a sound to pass round a screen or barrier. Lower frequency sounds can diffract around obstacles more easily because of their longer wavelength.

Diffusion

Complexity of reflecting surfaces causing an even dispersion of sound in a room, with no directionality of sound waves

Dryness

A characteristic of an auditorium which has a short reverberation time; to some extent the opposite of 'richness'.

Echo

Reflected sound discernible as separate from the initial sound, by virtue of the long reflected sound path.

Flanking

Ability of acoustic energy to by-pass a sound barrier at the edges. Good airborne sound insulation through a floor construction, for example, may be flanked by sound transmission down the walls or through ducts.

Flutter

Rapid echo pattern between parallel walls which can be discerned.

Focusing

Acoustic energy, like light energy, can be reflected from concave surfaces into a concentrated focus. This may leave 'dead spots' elsewhere.

Frequency

The number of cycles per second that a vibrating system completes. Units of frequency are cps. or more usually Hertz; both have identical value. The audibility of a sound depends on its level and also on its frequency. The human ear can detect sounds with frequencies ranging from 20 to 20,000 Hz although increasing age reduces the upper limit. The frequency, f, velocity, C, and the wavelength, λ , of the sound waves are related by the expression:

 $C = f\lambda$

Intimacy

Impression in sound quality, sometimes called 'presence', that the source is near. In an auditorium this can occur in surprisingly distant seat locations if they benefit from close reflecting surfaces.

L10

Noise level in dBA which is exceeded for 10% of the time.

L_{90}

Noise level in dBA which is exceeded for 90% of the time (background or lower limit noise condition).

L_{eq} (equivalent continuous sound level)
A-weighted energy mean averaged over the measurement period, ie the continuous steady noise level which would have the same total A-weighted acoustic energy as the real fluctuating noise measured over the same time.

Liveness

Attribute of a reverberant hall, imparting fullness of tone to music in high and mid frequencies.

Loudness

The subjective judgement of sound intensity by an individual which tends to be influenced by sound pressure and frequency. A typical response is for a three-fold change of sound pressure level to be considered a doubling of loudness.

Loudness level

The loudness level in phons of a noise is defined as

the sound pressure level in decibels of a 1000 Hz tone which sounds equal in loudness to the sound which is being rated.

Masking

The effect whereby the threshold of audibility of a sound is raised by the presence of another sound. Masking is most effective when the masking sound is of lower frequency than the sound to be masked.

Membrane absorber

A component assembly whereby a solid thin panel is spaced off a solid backing but by virtue of panel flexibility vibrates on the trapped layer of air. The frequency at which maximum absorption occurs depends on the spacing panel to backing and the superficial weight of the panel.

Noise

Sound unwanted by the recipient.

Noise reduction coefficient (NRC)

A single value to express absorption coefficients averaged over the octave bands centred on 250, 500, 1K and 2K Hz.

Normalized level difference

Difference in dB between energy levels in rooms on opposite sides of a partition corrected for a standard amount of absorption representative of normal furnished conditions in the receiving room.

Normalized level difference, $Dn = L_1 - L_2 + 10 \text{ Log}$ RT - 10 Log .5dB where RT = measured reverberation time in the receiving room during tests.

Pitch

The pitch of a sound is the frequency of an equally loud pure tone which on average is judged to occupy the same position on a musical scale.

Porous absorber

Sound-absorbing finish where the sound energy falling on it is dissipated by viscous losses within the pores of the material.

Pure tone

Sound at a finite, very narrow, frequency band and at no other.

Reflection

Sound energy returned after impact on a surface, rather than being absorbed as heat energy within the surface.

Resonance

The natural vibration of an area of material at a particular frequency as a result of excitation by a sound at that frequency.

Reverberation

The effect whereby a sound builds up in a space or at a point in a space because of multiple reflections from surrounding enclosing walls, floors and ceiling. This may enhance the sound if constant and the sound will gradually die away after the sound source ceases.

Reverberation time

The reverberation time of a room is the time taken for a steady sound when switched off to die away to inaudibility. More exactly, it is the time taken for the sound pressure level to fall by 60 dB. The reverberation time, T, is related to the volume of the room and the total absorption of the room by:

$$T = \frac{0.16V}{A} \text{ (seconds)}$$

where $V = \text{volume in } m^3$, $A = \text{absorption in } m^2 \text{ units.}$

Richness

A property of sound in an auditorium where there are many repetitions and reflections within a short period. Said to occur higher up in an auditorium because the sound is arriving up from more surfaces.

Room-to-room transmission

When a sound is transmitted from a reverberant room through a partition with sound reduction index (SRI) and Area S, into a room of absorption A, then the sound pressure level in the second room is:

$$SPL_2 = \underline{SPL_1} - SRI + 10 Log \frac{S}{A}$$
 (dB)

SPL₁ in this expression is the average sound pressure level in the first room. If the sound power level is known for the first room, then SPL₁ can be found from the equation:

$$SPL_1 = SWL - 10 Log A + 6 (dB)$$
 (6)

If instead of a second room there is just open air, then the difference in sound pressure levels between one side of the partition and the other is:

$$SPL_1 - SPL_2 = SRI + 6 (dB)$$

If SPL₁ near the inside of the wall of a building is known, then SPL₂ at some distance from the building is found from:

$$SPL_2 = SPL_1 - SRI + 10 Log S - 20 Log r - 14 (dB)$$

Sensitivity

The ear's sensitivity varies with frequency. It is much less sensitive at low rather than high frequencies, reaching a maximum at or around 1000 Hz. The sound pressure levels of sounds which are perceived as of equal loudness are referred to as equal loudness contours.

Simple sound source

A sound source radiating sound equally in all directions is called a simple source. The sound pressure level at a distance r from the source is given by:

$$SPL = SWL + 10 Log \left(\frac{1}{4 \pi r^2}\right) (dB)$$

or
$$SPL = SWL - 20 \log r - 11 (dB)$$

This is modified by different constraints which depend on the directivity of the source. As an example, if the sound source is close to the ground the sound radiates into a hemisphere and then 3 dB must be added to the SPL:

$$SPL = SWL - 20 Log r - 8 (dB)$$

6 dB would be added if the source were situated in the

angle between two walls. If the sound source is in a reverberant room rather than outdoors, the average reverberant level will be:

$$SPL = SWL - 10 Log A + 6 (dB)$$

The total sound pressure level resulting from the combination of reverberant and direct sound fields is given by:

$$SPL = SWL + 10 Log \left(\frac{1}{4 \pi r^2} + \frac{4}{A}\right) (dB) \qquad \dots$$

Sound

Sensation of hearing wave motion in an elastic medium.

Sound insulation

The fraction of incident sound energy falling per second on a partition which is transmitted through it is called the transmission coefficient τ and depends on mechanical and material properties of that partition. The performance of a partition is given in terms of an index known as the sound reduction index (SRI):

$$SRI = 10 Log \left(\frac{1}{\tau}\right) (dB) \qquad \dots$$

The SRI varies with frequency and is measured in a laboratory in either octave or one-third octave bands.

Sound power level

When a source of sound radiates sound waves in all directions, the total energy radiated in one second is called the sound power of the source and is measured in watts. The decibel range is again used to define sound power level (SWL) as follows:

$$SWL = 10 Log \left(\frac{W}{Wo}\right) (dB) \qquad \dots$$

W is the sound power of the source and Wo is the internationally recognized reference power 10⁻¹² watts.

Sound pressure level

The ear responds to the average value of pressure in the wave or root-mean-square pressure. The smallest detectable pressure is $2 \times 10^{-5} \,\mathrm{N}\,\mathrm{m}^{-2}$ or $2 \times 10^{-5} \,\mathrm{Pa}$

(Pascals) and the largest tolerable pressure is 20 Pa, referred to as the threshold of pain. The ear is approximately a logarithmic detector of pressure and so it is convenient to express sound pressure in decibels, and the sound pressure level (SPL) is defined as:

$$SPL = 20 Log \left(\frac{P}{Po}\right) (dB) \qquad \dots$$

Po is $2 \times 10^{-5} \, \text{Nm}^{-2}$ and P is the sound pressure of interest.

Sound reduction index

Difference in dB measured between the amount of energy flowing towards the wall in the source room and the total amount of energy entering the receiving room (usual range 100–3150 Hz).

$$SRI = L_1 - L_2 + 10 \text{ Log S} - 10 \text{ Log A (dB) (for negligible flanking)}$$

Where $S = \text{common area of partition in } m^2$, or more conveniently:

$$SRI = L_1 - L_2 + 10 Log \frac{ST}{0.16V} (dB)$$

Sound spectrum

Sounds can be analysed to reveal their frequency content. This can be achieved by dividing the frequencies into octave or one-third octave bands and the sound pressure levels measured in those bands.

Sound transmission class (STC)

Single-figure rating used mainly in the USA for comparing partitions for general building design purposes. Sound transmission losses in sixteen test bands from 125 to 4K Hz are compared with a reference contour as defined in ASTM E 413-73.

Sound waves

Sound waves are longitudinal pressure waves usually propagated through the air but also through solid material. In air they travel with a speed of 343 ms⁻¹ at 20°C.

Standardised level difference, DnT.

Difference (1S0 140) is given by DnT =
$$10 \log_{10} \frac{T}{T_0} dB$$

Where D is level difference

T is receiving room RT, seconds To is reference RT, 0.5 seconds.

Single figure value given as weighted standardised level difference, DnTW.

Standardised impact sound pressure level, L'nt The standardised impact sound pressure level in dB, is given by

$$L'nT = L_i + 10 \log \frac{To}{T}$$

where L_i is average sound pressure level
To is reference RT, 0.5 seconds
T is receiving roan RT, seconds.
Single-figure value is given as weighted standardised impact sound pressure level L'ntW.

Structure-borne sound

Sound energy that has passed through the solid elements of the building structure.

Warmth

Fullness of bass tone relative to mid-frequency response.



TABLES

C1 Typical sound reduction index values for elements of structure (20–50 m² size), in dB

	Average	verage Octave band centre free				juency (Hz) 2K 4K		
Sheet materials								
3 mm sheet lead	34	30	31	27	38	44	33	
6 mm steel plate	38	27	35	41	39	39	46	
20 sw profiled steel sheet	18	8	14	29	26	32	36	
Floors								
T & G Boards (or chipboard) to joists, plasterboard								
and skim soffit	35	18	29	37	49	44	46	
As above with fibreglass under chipboard, 50 mm								
sound pugging on mesh-backed plasterboard	51	37	42	47	52	60	64	
50 mm screed on 125 mm reinforced concrete	47	35	37	42	49	58	63	
As above with 13 mm fibreglass under screed	51	38	43	48	54	60	64	
50 mm screed on 200 mm reinforced concrete	51	38	45	47	52	60	64	
Doors								
Flush hollow doors, normal edge gaps	16	12	13	14	16	18	24	
Solid door, normal edge cracks	26	17	21	26	29	31	34	
Acoustic metal doorset, double seals	47	36	39	44	49	54	57	
Folding steel door	25	16	23	26	27	28	27	
Walls and partitions								
Single leaf fairfaced brick 102 mm	45	36	37	40	46	54	56	
Single leaf brickwork plastered on both sides								
13/102/13	47	34	36	41	51	58	60	
Double leaf brickwork plastered on both sides								
13/214/13	51	41	45	48	56	58	60	
Cavity brickwork with ties 102/50/102 plastered on	50	0.4	0.4	40	50	70	7.0	
both sides	52	34	34	40	56	73	76	
Fairfaced 115 mm lightweight concrete blockwork	38	32	32	33	41	49	57	
Fairfaced 115 mm light concrete blockwork	41	20	24	37	ΛE	ΕO	57	
+ 13 mm plaster on both sides	41	32	34	37	45	52	57	
Fairfaced 115 mm light concrete blockwork + 12.7 mm plasterboard on plaster dabs on both								
sides	44	28	34	45	53	55	52	
Fairfaced 215 mm light concrete blockwork	44	35	38	43	49	54	58	
Fairfaced 215 mm light concrete blockwork	44	30	30	40	43	54	50	
+ 13 mm plaster on both sides	47	37	39	46	53	57	61	
Fairfaced 215 mm light concrete blockwork	77	0,	00	70	00	0,	01	
+ 12.7 mm plasterboard on dabs on both sides	47	33	39	50	55	56	50	
Double wall of two 100 mm dense concrete blocks	, ,	00	00	00	00	,00	00	
with 50 mm cavity + 13 mm plaster on both sides	52	35	41	49	58	67	75	
man da min davity i To min places on both blace	32			.0	00	٥,	, 5	

	Average	Octave band centre frequency (F					
	Atolage	125	250	500	1K	2K	4K
Double partition of two 12.5 mm plasterboard skins with 50 mm cavity completely filled with glass							
fibre quilt Double partition of two 12.5 mm plasterboard skins	40	21	35	45	47	47	43
with 75 mm cavity – glass fibre blanket suspended within Double partition of two 12.5 mm plasterboard	39	24	37	44	42	43	44
sheets on each side of 50 mm cavity completely filled with glass fibre quilt	47	33	45	51	52	52	52
Double partition two 12.5 mm plasterboard skins on 75 × 50 mm staggered timber studding 50 mm woodwool cement slabs sealed on one side	37	24	28	37	46	46	38
only Sealed on both sides	30 33	26 25	28 31	30 36	32 35	33 35	36 37
100 mm woodwool cement slabs sealed on one side only	31	28	28	32	34	33	38
Sealed on both sides 50 mm woodwool cement slabs with 100 mm concrete on one face	35 42	29 36	30 36	32 42	36 44	39 46	46 53
50 mm standard woodwool cement/200 mm airspace/2 × 9.7 mm plasterboard attached to	42		30	42	44	40	55
legs of units 150 mm concrete supporting on resilient mounts	51	34	44	51	57	61	60
100 mm prescreeded woodwool cement slabs – large airspace 38 mm × 22 SWG profiled steel cladding sheet/	71	60	66	77	83 n	urable	
60mm glass fibre/9.5 mm plasterboard. Mounted on $50\times50\text{mm}$ timber spacers	39	18	30	41	46	49	50
38 mm × 22 SWG profiled steel cladding sheet/ 146 mm space containing 60 mm glass fibre/ 2 × 12.7 mm plasterboard. Mounted on 146 mm							
steel studs at 600 mm centres	47	32	41	47	49	53	58
Glazing Single – non-openable							
4 mm 6 mm 6.4 mm laminated	28 29 30 34	20 18 22 28	22 26 24 31	28 31 30 35	34 36 36 34	34 30 33 39	29 38 38 37
12 mm 4 mm glass in aluminium frame 100 mm opening	34 11	28 10	10	11	12	39 12	13
Sealed units – non-openable 4/12/4 mm	29	22	17	24	38	42	38
6/12/6 mm	30	20	20	29	30	36	46

	Average	0 125	ctave ba	and cent	re frequ 1K	iency (H 2K	lz) 4K
4/12/10 mm	34	25	22	33	41	44	44
4/12/10 mm + SP6	36	22	19	43	44	47	47
6/12/10 mm	34	26	27	35	41	39	47
6/150/4 mm	44	29	35	45	56	52	51
Sealed units – openable 3/6/3 mm Weather stripped	26	25	22	25	28	27	31
Dual units – non-openable 4/200/4 mm with absorbent reveals and separate heavy frames 6/200/6 mm with absorbent reveals in separate	42	37	37	44	53	47	36
heavy frames	46	37	41	48	54	47	47
Openable 4/200/4 mm with absorbent reveals in aluminium frames 4/200/4 mm with absorbent reveals in aluminium	39	27	33	39	42	46	44
frames – opposite ends open 25 mm Opposite ends open 100 mm	27 22	15 10	23 16	34 27	32 25	28 27	32 27

These are typical values measured in the laboratory. Field tests may give lower values.

C2 Typical coefficients of sound absorption

	Octave band centre frequency (Hz)						
	125	250	500	1K	2K `	4K	
Ceiling							
Overhead sound absorbers, one 1200 × 450							
× 50 mm panel every sq m, parallel pattern	.28	.58	.96	.91	.86	.81	
Fissured mineral tiles, 300 mm ceiling void	.3	.35	.4	.55	.8	.7	
Metal tiles (5% perforated), 20 mm fibreglass quilt,							
ceiling void	.13	.27	.55	.79	.9	1.0	
Metal planks, slots between planks (14% free area)	.5	.7	.8	1.0	1.0	1.0	
13 mm plasterboard ceiling over large air space	.2	.2	.2	.1	.05	.05	
13 mm acoustic plaster on metal lathing	.05	.2	.5	.8	.8	.8	
Profiled metal deck	.1	.3	.3	.1	.1	.2	
Walls and linings							
Brickwork – fairfaced	.02	.02	.02	.03	.04	.05	
painted	.01	.01	.01	.02	.02	.02	
plastered	.02	.02	.03	.03	.04	.05	
Blockwork – fairfaced	.2	.5	.5	.4	.5	.4	
Concrete – textured finish	.01	.02	.04	.06	.08	.1	
9 mm acoustic plaster on solid wall	.02	.08	.3	.6	.8	.9	
Woodwool slabs on solid backing							
– 50 mm thick	.2	.2	.6	.8	.7	.9	
– 100 mm thick	.3	.8	.9	.7	.7	.8	
Prescreed woodwool slabs on 600 mm air gap	.4	.4	.7	.7	.7	.8	
9 mm plasterboard on 18 mm air space filled with							
fibreglass to solid backing	.3	.2	.2	.05	.05	.05	
12 mm plywood on 30 mm airspace filled with		_	_				
fibreglass, to solid backing	.4	.2	.2	.1	.1	.05	
6 mm glass, large panes	.3	.3	.2	.1	.05	.05	
Stretched, lightweight fabric wall hanging	.04	.1	.2	.5	.6	.5	
Heavy curtain material hung in folds	.06	.16	.3	.55	.65	.65	
Fibreglass quilt to solid backing	4	4	0	7	0	0	
25 mm thick	.1	.4	.6	.7	.8	.8	
50 mm thick	.3	.6 .8	.8	.9	.8	.8	
100 mm thick	.5 .5	.8 1.0	.8 .9	.9	.9	.9	
Fibreglass 100/100 mm airspace Mineral wool to solid backing	.5	1.0	.9	.8	.6	.4	
– 25 mm thick	.01	.3	.7	1.0	1.0	1.0	
– 50 mm thick	.01	.s .8	1.0	1.0	1.0 1.0	1.0 1.0	
Mineral wool 25/25 mm airspace	.s .1	.4	.7	1.0	1.0	1.0	
50/50 mm airspace	.5	.7	.7	.9	.9	.8	
·	U.	. 1	.9	.9	.5	.0	
Floors This contract corner on called floor	0.1	0.4	0.5	10	^	^	
Thin contract carpet on solid floor	.01	.04	.05	.18	.3	.2	

	Octave band centre frequency (Hz)					
	125	250	500	1K	2K`	
Thick carpet on underlay	.07	.23	.69	1.0	1.0	1.0
Rubber flooring, vinyl sheet	.02	.04	.05	.05	.05	.05
Marble, ceramic tiles	.05	.05	.05	.05	.05	.05
Reinforced concrete, grano	.02	.02	.02	.04	.05	.05
Water (swimming pool), ice (rink)	.01	.01	.01	.02	.02	.03
Other						
Seated audience, per person*	.33	.4	.44	.45	.45	.45
Standing adults, per person*	.15	.38	.42	.43	.45	.45
Wooden seats*	.1	.2	.3	.3	.3	.35
Upholstered seats*	.24	.26	.27	.31	.37	.38
Shading reduction factors (for floor finishes						
absorption under seating)	-20%	-30%	-40%	-50%	-60%	-80%

^{*}These figures are the total absorption in m².

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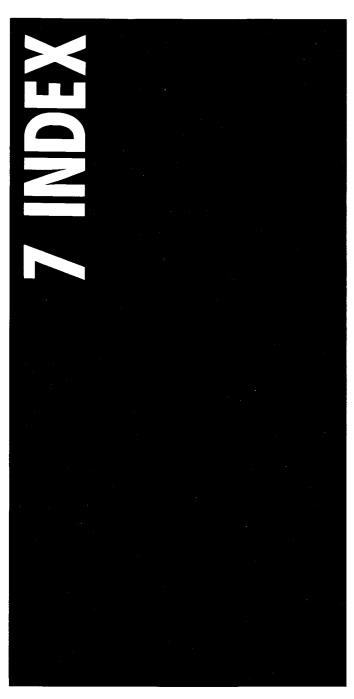
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